



BLUELINE

City Heights Phase I (Pods B7 and C) Cle Elum, Washington

Date: June 17, 2020



6/17/20

Preliminary Storm Drainage Report

Prepared for
City Heights Holdings, LLC
116 1/2 S. Washington Street
Seattle, WA 98104

Blueline Job No. 19-349
Prepared by: Michelle Roberge, PE
Reviewed by: Lyndsey Fedak, PE
Approved by: Brett Pudists, PE

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APPENDIX

- Crystal Creek 3 (Pond B7-A) Hydraflow Output
- Crystal Creek 5 (Vault C) Hydraflow Output



Section 1 Project Overview

Project Name:	City Heights
Project Parcels:	493935, 956732, 956734, 956736 (Phase 1)
Project Engineer:	The Blueline Group Brett Pudists, PE (425) 250-7247
Project Applicant:	City Heights Holdings, LLC Sean Northrop (206) 388-3121
Project Development Area:	33.11 acres (Phase 1) Total Disturbed: 15.86 acres
Number of Lots:	68

1.1 SITE INFORMATION

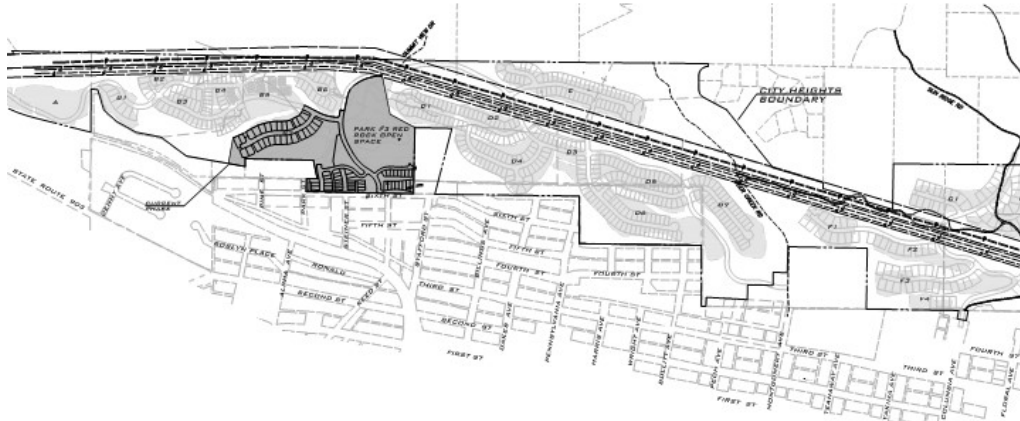
SITE INFORMATION	
Project location	City of Cle Elum
Zoning	Planned Mixed Use Development (PMU)
Climate Region (Figure 4.1 of 2019 SWMMEW)	Region I (East Slope Cascades)
Average Annual Precipitation (Figure 4.1 of 2019 SWMMEW)	25 in/yr
P2year,24hour (Figure 4.7 of 2019 SWMMEW)*	2 in
P10year,24hour (Figure 4.9 of 2019 SWMMEW)*	3.25 in
P25year,24hour (Figure 4.10 of 2019 SWMMEW)*	3.5 in
P100year,24hour (Figure 4.12 of 2019 SWMMEW)*	4.75 in
Type of Soil per Geotech report	Weathered siltstone/sandstone with areas of fill soils east of Summit View Road and silty sand/gravel/silt with areas fill soils containing coal waste west of Summit View Road
Design Infiltration Rate per Geotech report	N/A, deemed infeasible

*Precipitation depth adjusted for rain-on-snow and snowmelt considerations, refer to Section 6.3 for adjusted precipitation depths.



1.2 EXECUTIVE SUMMARY

This Preliminary Storm Drainage Report is for the construction of Phase 1 of City Heights (Pods B7 & C), a Planned Mixed Use (PMU) development. More generally the property is located within the NE ¼ of Section 27, Township 20 N, Range 15 East, W.M. See vicinity map below.



Vicinity Map, Not to Scale

The overall City Heights project is approximately 358 acres; however, this report will limit discussion to Phase 1, which is approximately 33.11 acres. The site is mostly forested and consists of existing bike trails and an asphalt road, Summit View Rd, that heads north. There are also wetlands and a stream identified in the report prepared by Sewall Wetland Consulting, Inc. dated October 26, 2009. The site is underlain with weathered siltstone/, sandstone, silt/silty sand/gravel, and fill soils containing coal waste generally consistent with the report prepared by Terra Associates, Inc dated June 9, 2020. A Web Soil Survey Map is included in Section 4. The site contains moderate to steep slopes 2% to greater than 25%.

In the existing condition, runoff is generated from two drainage basins dictated by a stream bisecting the site, creating the Crystal Creek 3 basin, tributary to Stream C (ultimately tributary to Crystal Creek) and the Crystal Creek 5, tributary to an existing roadside ditch (ultimately tributary to Crystal Creek). Runoff from Crystal Creek 3 generally sheet flows southeast before entering an existing onsite stream (Stream C), which is tributary to Crystal Creek. Runoff from Crystal Creek 5 generally sheet flows south before entering an existing ditch along 6th Street, which is tributary to an existing roadside ditch. Please refer to the Existing Conditions Exhibit included at the end of this section and the Downstream Drainage Exhibit included in Section 3.

In the proposed condition, Crystal Creek 5 (Vault C) will consist of 40 lots (32 single-family and 4 duplexes), proposed roads/alleys, a relocated portion of Summit View Road, a future amenity area (Outfitter) and parking area, a biofiltration swale for water quality, and a detention vault (Vault C) for flow control. Crystal Creek 3 (Pond B7-A) will consist of 28 single family lots, proposed roads/alleys, a biofiltration swale for water quality, and a detention pond (Pond B7-A) for flow control.

The Crystal Creek 4 basin will be developed as part of a future phase. Tract K, proposed with this application, is set aside in an open space/stormwater tract and is reserved for the future detention pond (Pond B7-B) that will be sized to accommodate the future development of Pods B2-B6. Please note Pond B7-B and its associated future



development (Pod B2-B6) will be submitted under a separate permit. Refer to the Proposed Conditions Exhibit included at the end of this section and the Downstream Drainage Exhibit included in Section 3.

The project has been designed using the guidelines and requirements established in the 2019 Department of Ecology (DOE) Stormwater Management Manual for Eastern Washington (SWMMEW) and the City Heights Annexation and Development Agreement (DA), dated November 8, 2011.

The project will implement flow control BMPs per Chapter 6 of the 2019 SWMMEW. Per Section 4.3.9 of the 2019 SWMMEW, including rain-on-snow and snowmelt design, is optional guidance for detention and water quality design. However, rain-on-snow and snowmelt design requirements are applied for this project. For more information, refer to Section 6 of this report. Per the Geotechnical report provided by Terra Associates, Inc dated June 9, 2020, infiltration is infeasible.

A detention pond (Pond B7-A) and a vault (Vault C) are proposed as flow control facilities for the site per BMP F6.10 and BMP F6.12 to match the developed peak flows with existing peak flows for 50% of the 2-year storm event and the full 25-year storm event. Additionally, per the DA, while the manual stipulates that the design needs to assume a 25-year flood event, the City has requested, and the Ridge Entities have agreed, to design the stormwater system for City Heights assuming a 100-year flood event, thereby increasing the capacity of the system beyond what is required by current regulations. The project will not be required to remedy any already existing deficiencies in the existing system.

The project proposes more than 5,000 SF of pollution generating hard surface (PGHS), is not a commercial or industrial site, and does not discharge to a wetland or phosphorous sensitive receiving waters. Per Figure 2.3 of the 2019 SWMMEW, basic water quality treatment is required. Refer to the flow charts for determining stormwater requirements in accordance with the 2019 SWMMEW on the following pages.



Figure 2.1: Flow Chart for Determining Applicable Core Elements for New Development Projects

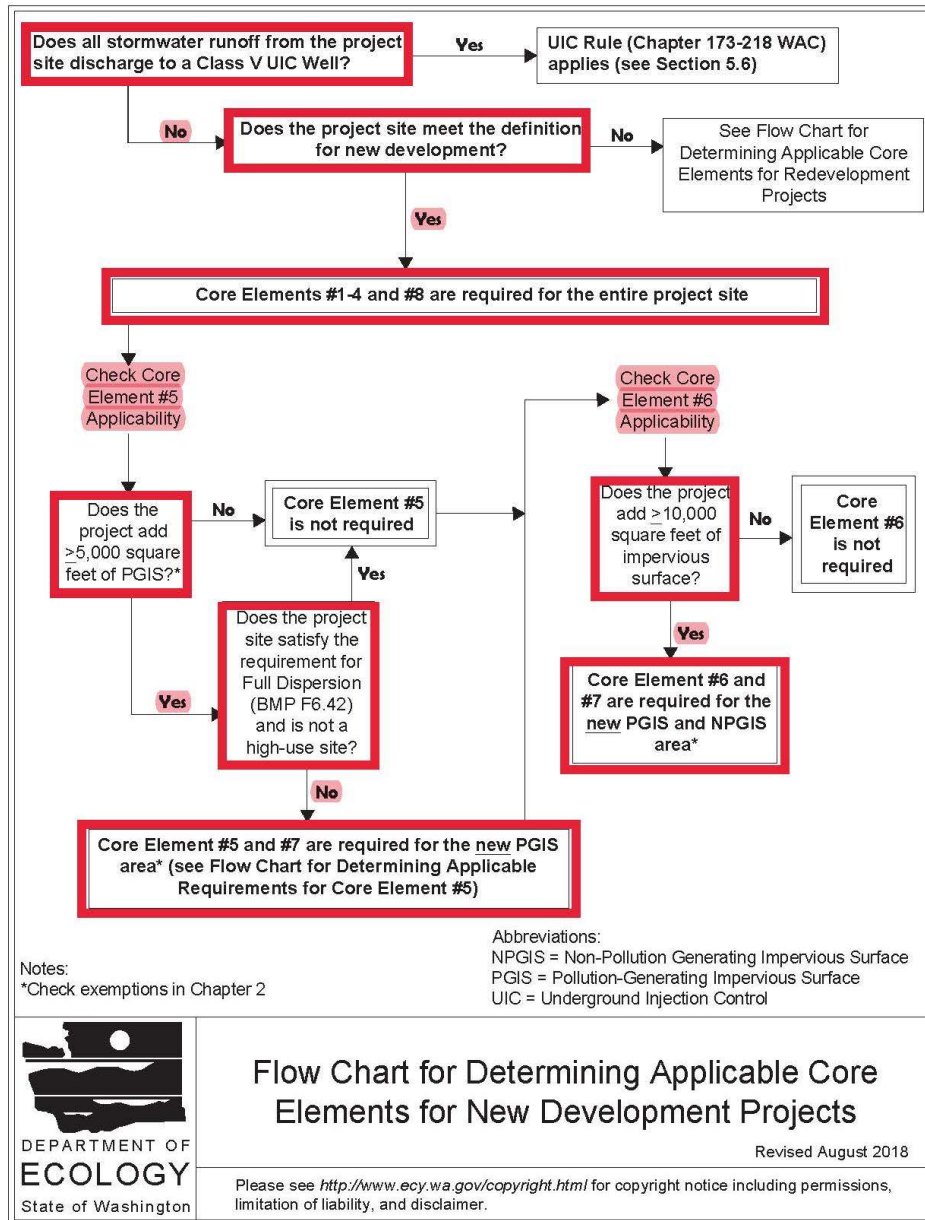
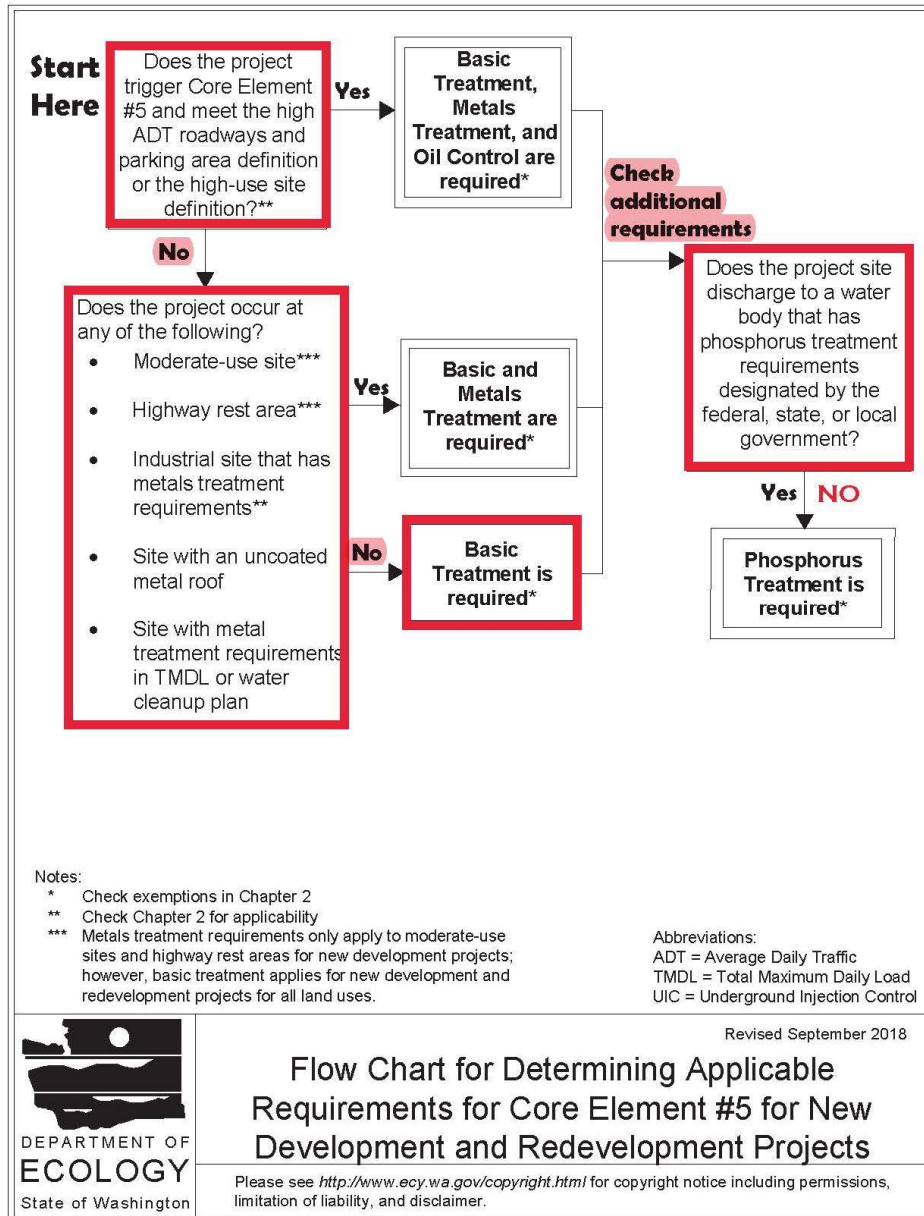


Figure 2.3: Flow Chart for Determining Applicable Requirements for Core Element #5 for New Development and Redevelopment Projects



Section 2 Existing Conditions

The City Heights project is located in Cle Elum, Washington. The Site generally consists of topographic conditions ranging from nearly flat/gently sloping to relatively steeply sloped ground with multiple topographic drainage features. Per the Geotechnical Engineering Report prepared by Terra Associates, Inc dated June 9, 2020 onsite soils consist of weathered siltstone/sandstone with areas of fill soils east of Summit View Road. West of Summit view consists of silty sand/ gravel/silt with areas fill soils containing coal waste. See Geotechnical Report submitted under separate cover for more information.

The majority of the site is a forested, undeveloped land with existing bike trails within and near the proposed project site – Phase 1. Summit View Road is an existing road that serves as an access road to existing residential lots north of the City Heights development. Runoff generally sheets flow southwest to an existing onsite stream (Stream C) and the remainder of the Phase 1 areas sheet flow southeast towards a ditch along 6th Street. There are existing culverts located within the project site.

The existing site contains two drainage basins: Crystal Creek 5, tributary to an existing roadside ditch and Crystal Creek 3, tributary to Stream C. There is an existing gully created by a seasonal stream that crosses Summit View Road. Stream C acts as the natural basin divide. Phase 1 areas that drain to Stream C are associated with Crystal Creek 3. Remaining Phase 1 areas are associated with Crystal Creek 5.

An upstream area of 3.89 acres sheets flows towards Crystal Creek 5. This area will remain undeveloped and undetained. In the developed condition, this area will be collected via shallow swale and will bypass the detention/water quality facilities and, as such, are not included in the analysis. An upstream area of 2.17 acres sheets flows towards Crystal Creek 3. This area will remain undeveloped. This area will be routed through the detention/water quality facilities and, as such, is included in the analysis.

Crystal Creek 4 represents the area north of Crystal Creek 3 that will be developed as part of a future phase. These areas will be routed away from the detention/water quality facilities associated with Phase 1 and, as such, are not included in the analysis. Please note Pond B7-B and its associated future development (Pod B2-B6) will be submitted under a separate permit.



Section 3 Developed Conditions

The proposed development includes the creation of 68 residential lots (60 single-family detached lots and 8 lots to accommodate single-family attached duplexes) with associated utilities, stormwater detention and water quality facilities, access roadways and supporting utilities/infrastructure. Water quality and flow control improvements are described in Section 6 of this report.

Crystal Creek 5 (Vault C)

Crystal Creek 5 is the portion of Phase 1 development located north of 6th Street. A detention vault (Vault C) is proposed to serve 40 lots (32 single-family and 4 duplexes). Stormwater within Crystal Creek 5 will be collected by catch basins and area drains and conveyed via tightline conveyance to Vault C. Vault C is sized to maintain the stream protection flows as defined by the 2019 SWMM EW. Stormwater will discharge from the detention vault and be conveyed eastward to a proposed public tightline system along the 6th Street before outletting to an existing roadside ditch.

Onsite stormwater will be treated using a biofiltration swale, which is sized to treat the full water quality volume as calculated by Hydraflow software. Please refer to Section 6 for the detention sizing and the water quality selection for the project.

An upstream area of 3.89 acres sheets flows towards Crystal Creek 5. This area will remain undeveloped and undetained. In the developed condition, this area will be collected via shallow swale and will bypass the detention/water quality facilities and, as such, are not included in the analysis.

Crystal Creek 3 (Pond B7-A)

Crystal Creek 3 is the portion of Phase 1 development tributary to Stream C. A detention pond (Pond B7-A) is proposed to serve 28 single-family lots. Stormwater within Crystal Creek 3 will be collected by catch basins and area drains and conveyed via biofiltration swale and tightline conveyance to Pond B7-A. The stormwater detention pond is sized to maintain the stream protection flows as defined by the 2019 SWMM EW. Stormwater will discharge from the detention pond and be conveyed westwards to a proposed tightline system before outletting via dispersion trench and bubble-up structure to Stream C.

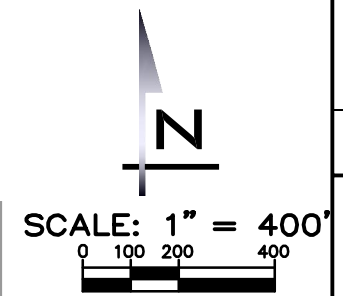
Onsite stormwater will be treated using a biofiltration swale, which is sized to treat the full water quality volume as calculated by Hydraflow software. Please refer to Section 6 for the detention sizing and the water quality selection for the project.

An upstream area of 2.17 acres sheets flows towards Crystal Creek 3. This area will remain undeveloped. This area will be routed through the detention/water quality facilities and, as such, is included in the analysis.

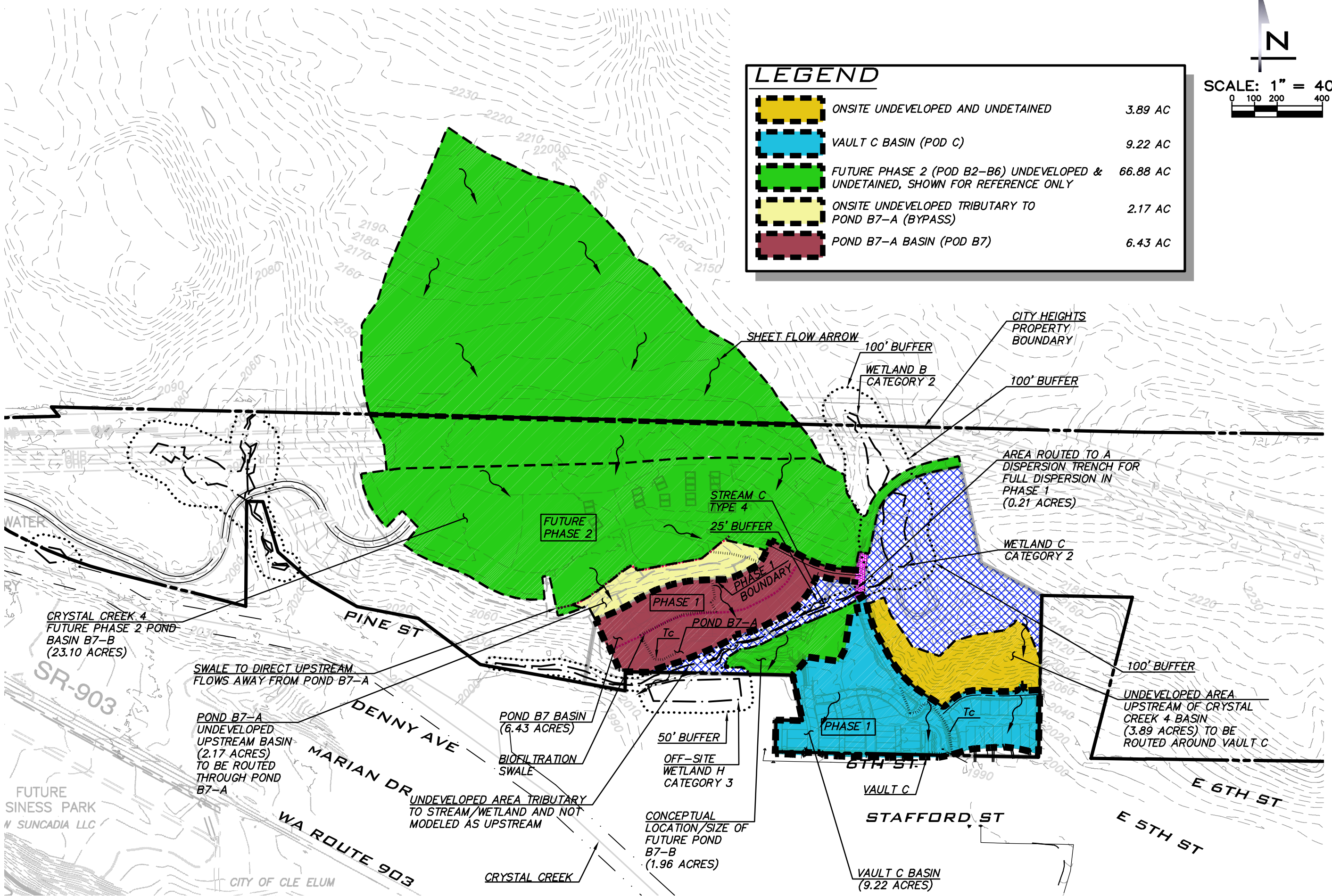
Crystal Creek 4 represents the area north of Crystal Creek 3 that will be developed as part of a future phase. These areas will be routed away from the detention/water quality facilities associated with Phase 1 and, as such, are not included in the analysis. Please note Pond B7-B and its associated future development (Pod B2-B6) will be submitted under a separate permit.



DEVELOPED CONDITIONS EXHIBIT



LEGEND		
	ONSITE UNDEVELOPED AND UNDETAINED	3.89 AC
	VAULT C BASIN (POD C)	9.22 AC
	FUTURE PHASE 2 (POD B2-B6) UNDEVELOPED & UNDETAINED, SHOWN FOR REFERENCE ONLY	66.88 AC
	ONSITE UNDEVELOPED TRIBUTARY TO POND B7-A (BYPASS)	2.17 AC
	POND B7-A BASIN (POD B7)	6.43 AC



DEVELOPED CONDITIONS EXHIBIT
CITY HEIGHTS
 PRELIMINARY DRAINAGE REPORT
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SCALE	AS NOTED
PROJECT MANAGER	BRETT PUDISTS, PE
DESIGNED BY	CHRIS WSCOMB
DRAWN BY	MICHELLE ROBERGE, PE
PLOT DATE	June 16, 2020
JOB NUMBER:	19-349
FIGURE:	DC

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Section 4 Off Site Analysis

Phase 1 of the City Heights development consists of two drainage basins. As part of the EIS process, an offsite analysis for the entire City Heights development was prepared by Encompass Engineering & Surveying. An additional offsite analysis prepared by Barghausen Consulting Engineers, Inc. addresses the downstream system for the City Heights development. Refer to excerpts from the *Grading, Drainage and Utilities Engineering Report* that was prepared by Encompass Engineering & Surveying, dated March 24, 2010 and the *Downstream Drainage Analysis* prepared by Barghausen Consulting Engineers, Inc., dated February 25, 2011 at the end of this section. A supplemental field investigation was conducted by Blueline on Friday, April 24, 2020 to confirm the findings in these reports.

The following is a summary of the findings from the information used in preparing this report for Phase 1 (Pod B7 & C). Refer to the *Geotechnical Engineering Report and Geologic Hazard Assessment* prepared by Terra Associates, Inc. dated June 9, 2020, *Wetlands and Wildlife Habitat Report* prepared by Sewall Wetland Consulting, Inc. dated October 26, 2009, and *Impacts Analysis* prepared by Sewall Wetland Consulting, Inc. dated June 16, 2020 submitted under separate cover.

- The site is located within the Upper Yakima Watershed (DOE Mapping).
- Soils consist of weathered siltstone/sandstone with areas of fill soils east of Summit View Road and silty sand/gravel/silt with areas fill soils containing coal waste west of Summit View Road. See Geotechnical Report submitted under separate cover for more information.
- The site contains two drainage basins that ultimately drain to the Yakima River (see downstream Exhibit at end of this section).
- The site contains onsite wetlands and streams per report by Sewall Wetland Consulting, Inc dated October 26, 2009. (Refer to report submitted under separate cover for Sewall Map Figure 3.4-2).
- The site is not located within a floodplain (FEMA Flood Maps).
- The site contains slopes up to 65% in the waste rock pile area per geologic hazard assessment, Section 4.2 of Geotechnical Report by Terra Associates, Inc. See Geotechnical Report submitted under separate cover for more information.
- For Erosion Hazard Area, refer to Section 4.6 and 4.7 of Geotechnical Report by Terra Associates, Inc. See Geotechnical Report submitted under separate cover for more information. There is a 10' high, 15' wide gully formed by a seasonal stream that crosses Summit View Road.
- For geologic hazard assessment, refer to Section 4.3 of Geotechnical Report by Terra Associates, Inc. See Geotechnical Report submitted under separate cover for more information. Shallow slope failures observed along Summit View Road.
- For Seismic Assessment refer to Section 4.1.4 of Geotechnical Report by Terra Associates, Inc. See Geotechnical Report submitted under separate cover for more information. The coal waste pile of development is classified as Class Site E per IBC.
- For Liquefaction Assessment refer to Section 4.1.3 of Geotechnical Report by Terra Associates, Inc. See Geotechnical Report submitted under separate cover for more information. The potential for liquefaction is low.
- Sedimentation accumulation in the conveyance system downstream was observed during the supplemental field investigation conducted by Blueline on April 24, 2020. Per the DA, the project will not be required to remedy any already existing deficiencies in the existing system. Sediment removal is likely to occur as part of regular City maintenance.



4.1 UPSTREAM CONDITIONS

An upstream area of 3.89 acres sheets flows towards Crystal Creek 5. This area will remain undeveloped and undetained. In the developed condition, this area will be collected via shallow swale and will bypass the detention/water quality facilities and, as such, are not included in the analysis. An upstream area of 2.17 acres sheets flows towards Crystal Creek 3. This area will remain undeveloped. This area will be routed through the detention/water quality facilities and, as such, is included in the analysis.

Crystal Creek 4 represents the area north of Crystal Creek 3 that will be developed as part of a future phase. These areas will be routed away from the detention/water quality facilities associated with Phase 1 and, as such, are not included in the analysis. Please note Pond B7-B and its associated future development (Pod B2-B6) will be submitted under a separate permit.



4.2 DOWNSTREAM ANALYSIS

EXISTING DRAINAGE SYSTEM

Phase 1 of the City Heights development consists of two drainage basins. As part of the EIS process, an offsite analysis for the entire City Heights development was prepared by Encompass Engineering & Surveying. An additional offsite analysis prepared by Barghausen Consulting Engineers, Inc. addresses the downstream system for the City Heights development. Refer to excerpts from the *Grading, Drainage and Utilities Engineering Report* that was prepared by Encompass Engineering & Surveying, dated March 24, 2010 and the *Downstream Drainage Analysis* prepared by Barghausen Consulting Engineers, Inc., dated February 25, 2011 at the end of this section. A supplemental field investigation was conducted by Blueline to confirm the findings in these reports.

A supplemental field investigation was conducted by Blueline on Friday, April 24, 2020, an overcast day and temperatures around 55°F. Downstream Photographs and a corresponding Downstream Drainage Exhibit are included at the end of this section.

EXISTING DOWNSTREAM DRAINAGE PATH

Crystal Creek 3

The Crystal Creek 3 basin generally sheet flows southeast toward an existing onsite stream (Stream C). The stream continues to flow southwest. The stream continues onto private property and could not be seen from public right-of-way. It is assumed the downstream path continues per prior reports completed by Encompass Engineering & Surveying and Barghausen. See the excerpted pages of downstream reports at the end of this section. Stream C is ultimately tributary to Crystal Creek.




Crystal Creek 5

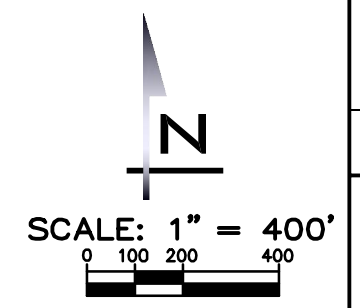
The Crystal Creek 5 basin generally sheet flows south toward 6th Street. Runoff enters an existing ditch along 6th street and outlets to an existing roadside ditch. Flow continues south/southeast across private property and could not be seen from public right-of-way. It is assumed the downstream path continues per prior reports completed by Encompass Engineering & Surveying and Barghausen. See the excerpted pages of downstream reports at the end of this section. The existing roadside ditch is ultimately tributary to Crystal Creek.

Refer to the *Downstream Drainage Exhibit* at the end of this section.



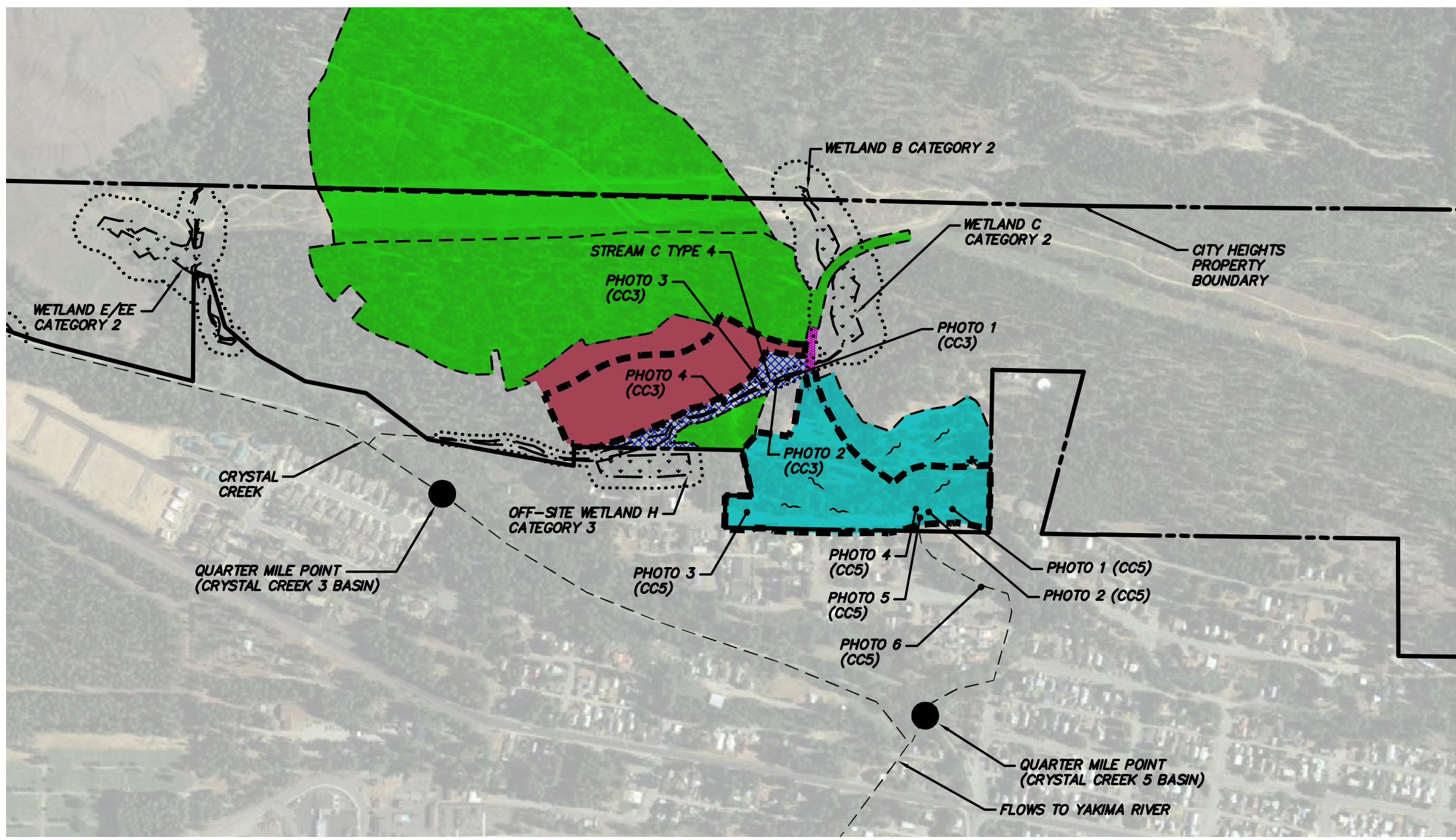
DOWNSTREAM DRAINAGE EXHIBIT

LEGEND		
	CRYSTAL CREEK 5 BASIN	13.11 AC
	CRYSTAL CREEK 3 BASIN	8.60 AC
	CRYSTAL CREEK 4 BASIN, PART OF FUTURE PHASE, SHOWN FOR REFERENCE ONLY	66.88 AC



DOWNSTREAM DRAINAGE EXHIBIT
 CITY HEIGHTS
 PRELIMINARY DRAINAGE REPORT
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SCALE	AS NOTED
PROJECT MANAGER	BRETT PUDISTS, PE
DESIGNED BY	MICHELLE ROBERGE, PE
DRAWN BY	MICHELLE ROBERGE, PE
PLOT DATE	June 16, 2020
JOB NUMBER:	19-349
FIGURE:	DS



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DOWNSTREAM DRAINAGE PHOTOGRAPHS

Note: See the *Downstream Drainage Exhibit* for numbered locations of pictures.

Crystal Creek 5:



Photo 1 – Facing east. Runoff sheet flows west towards culvert under 6th St.



Photo 2 – Facing west. Runoff sheet flows west towards culvert under 6th St.





Photo 3 – Facing north. 18 RCP" culvert crossing 6th St.



Photo 4 – Facing north. 18 RCP" culvert crossing 6th St.





Photo 5– Facing southwest. Runoff flows out of 18" RCP culvert to flat bottom creek, heavily vegetated.



Photo 6 – Facing east. Runoff continues to flow along flat bottom creek, heavily vegetated.



Crystal Creek 3:



Photo 1 – Facing northeast. East of Summit View Drive.



Photo 2 – Facing northeast. East of Summit View Drive. Runoff flows into 48" HDPE culvert





Photo 3 – Facing southwest. West of Summit View Drive. Runoff flows out of 48" HDPE culvert (Crystal Creek 3 Basin 3).



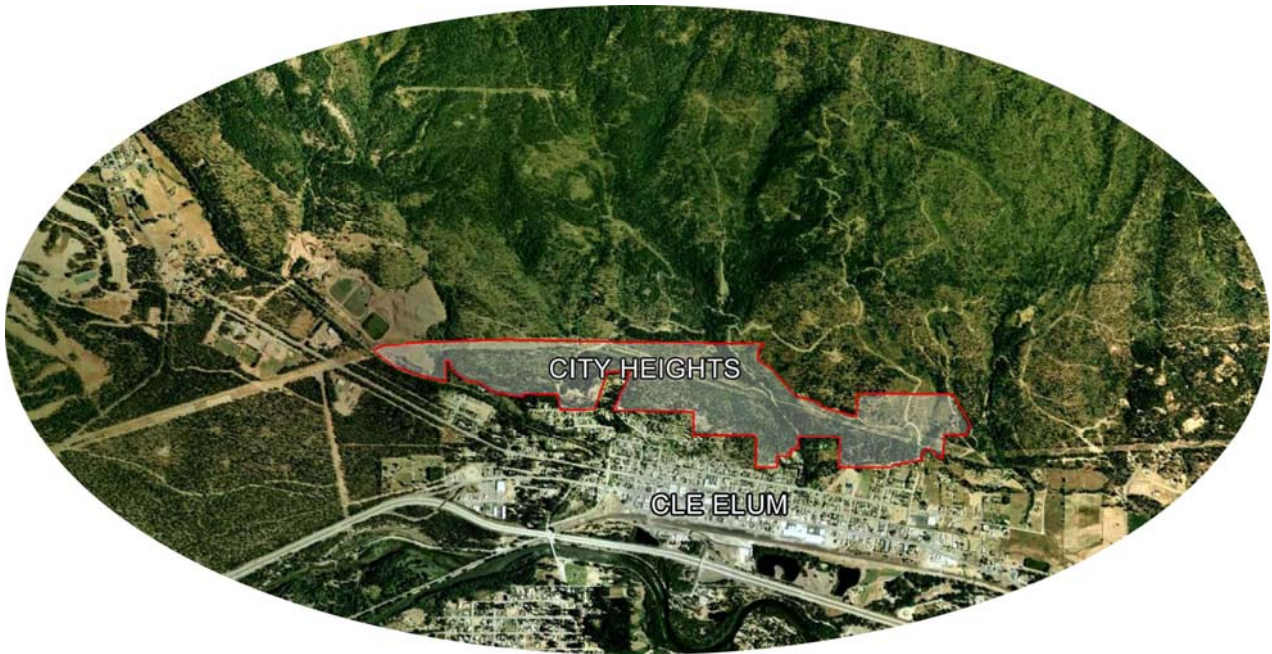
Photo 4 – Facing southwest. Runoff continues to flow through gully.

Grading, Drainage and Utilities Engineering Report that was prepared by Encompass Engineering & Surveying, dated March 24,2010



CITY HEIGHTS, CLE ELUM

GRADING, DRAINAGE, AND UTILITIES TECHNICAL ENGINEERING REPORT



March 24, 2010

Encompass
ENGINEERING & SURVEYING



108 East 2nd Street
Cle Elum, WA 98922
Tel. 509.674.7433
Fax. 509.674.7419

3. STORM DRAINAGE

This section describes alternatives for the management and mitigation of stormwater generated within the City Heights Planned Mixed-Use Development, both during construction and in the developed condition of the project.

3.1 Pre-Development Condition

This section describes existing project site drainage conditions based on different existing features that impact stormwater runoff. A preliminary downstream analysis of the project site has been performed, and the results are presented below. The bulleted items that follow are descriptions of the downstream path to the Yakima River from the City Heights site:

- West Basin is the western most downstream basin that drains directly into Crystal Creek
- Summit View Basin begins at Summit View Road and heads southwest across private property and into Crystal Creek
- Sixth Street Basin begins on Sixth Street near the City of Cle Elum water tanks and heads west, then south and into Crystal Creek
- Peoh Basin begins at the north end of Peoh Street and heads south into the City's 2nd Street stormwater conveyance system
- Montgomery Basin begins at Montgomery Avenue and heads southeast across private lands and into the City's 2nd Street stormwater conveyance system
- Columbia Basin begins at the extension of Columbia Avenue (also known as Creekside Road) and heads south into the City's 2nd Street stormwater conveyance system.

Detailed descriptions of each downstream basin from the City Height's property to the Yakima River are provided in the Downstream Drainage System maps (Figures 3.1A and 3.1B, and the Off-Site Drainage System Analysis Tables in Appendix B). Crystal Creek is identified as Category 4A Water just north (upstream) of the most western end of the City Heights project site, based on the Department of Ecology Water Quality Assessment [303(d) list] for Washington. DOE studies have determined that pollutants such as fecal coliform, dissolved oxygen, chlorine, and ammonia are present in the water. DOE has therefore issued, and Environmental Protection Agency (EPA) has approved, Total Maximum Daily Load (TMDL) criteria for Crystal Creek. See Appendix B for more information on 303(d) list and TMDL criteria. Based on the design criteria and mitigation measures for stormwater and sewer, the proposed City Heights project will not adversely affect the existing water quality of Crystal Creek.

3.1.1 Project Watershed

The City Heights site is located in the northwest quadrant of the Upper Yakima River Watershed. The Upper Yakima River watershed, which is a part of the greater Yakima River watershed, drains an area 2,139 square miles in size. Elevations range from about 7,000 feet above sea level at the crest of the Cascade Mountains to about 1,000 feet above sea level at the confluence of the Yakima and Naches Rivers. This confluence also forms the upper boundary of the Lower Yakima River watershed. This watershed contains some of the most intensively irrigated lands in the United States. The Upper Yakima River watershed is predominantly forested (1,153 square miles) in its higher elevations, and contains 85,000 acres

of irrigated agriculture in its lower elevations. The majority of irrigated acreage drains to the tributaries of Wilson Creek, Manastash Creek, and Sorenson Creek. Below the outlet of the Lake Keechelus dam, the main tributaries to the Upper Yakima River are the Kachess River, Cle Elum River, and Teanaway River. There are many other smaller tributaries to the upper Yakima River.

3.1.2 Project Sub-Basin

There are no known basin studies produced for the watershed that includes the City Heights site. For the purpose of this report, the sub-basin for the proposed City Heights Planned Mixed-Use Development has been delineated based on USGS maps and other available information. The project site is within the sub-basin located on the north side of the City of Cle Elum, encompassing an area from the Town of Roslyn on the west, Cottage Avenue in the City of Cle Elum on the east, the top of Cle Elum Ridge on the north, 3rd Street and SR-903 within the City of Cle Elum on the south. This sub-basin is approximately 470 acres in size. Crystal Creek, multiple unnamed seasonal streams, and the City of Cle Elum stormwater management system are the principal surface water features within the sub-basin that includes the project site.

3.1.3 Site-Specific Drainage Basins

Based on preliminary findings, the majority of the City Heights property hydrology is split between four significant drainage basins. These basins directly affect Crystal Creek, several other seasonal streams, and irrigation ditches. These basins are strongly influenced by snow melt and recharge over the upland areas, including on the City Heights property. Encompass Engineering & Surveying (Encompass) analyzed the aerial topographic map prepared by Degross Aerial Mapping, Inc. (2009), and delineated five separate site-specific drainage basins. These areas are shown in Appendix C. The level of detail utilized for the delineation of the site-specific basins is appropriate for the preliminary storm drainage calculation and analysis for the entire project site. A more detailed analysis of the drainage basins is recommended for the construction design. The site-specific drainage basin descriptions are as follows:

Basin A:

Drainage Basin A is located in the western-most area of the project site, and consists of 822.91 acres of forest land, underlain with ashy and Teanaway loam soils. Only 84.64 acres of this basin is considered in the analysis, as the rest of the area will be by-passed via existing drainage routes. The analyzed area is located in the southern-most portion of the Drainage Basin A, closest to the City of Cle Elum, and limited to the proposed City Heights Planned Mixed-Use Development. Run-off from this basin contributes to the headwaters of Crystal Creek to the southwest.

Basin B:

Drainage Basin B is located east of Drainage Basin A, and consists of 379.44 acres of mixed forest land and pasture, with forest land being the predominant factor. Similar to Drainage Basin A, Drainage Basin B is underlain with ashy and Teanaway loam soils. Only 57.53 acres of this basin is considered in the analysis, as the rest of the area will be by-passed via existing drainage routes. The analyzed area is located in the southern-most portion of Drainage Basin B, closest to the City of Cle Elum, and limited to the proposed City Heights Planned Mixed-Use Development. Run-off from this basin enters the City of Cle Elum storm drainage system to the south.

Basin C:

Drainage Basin C is located east of Drainage Basin B, and consists of 1,174.10 acres of mixed forest land and pasture, with forest land being the predominant factor. Similar to Drainage Basins A and B, Drainage Basin C is underlain with ashy and Teanaway loam soils. Only 179.76 acres of this basin is considered in the analysis, as the rest of the area will be by-passed via existing drainage routes. The analyzed area is located in the southern-most portion of Drainage Basin C, closest to the City of Cle Elum, and limited to the proposed City Heights Planned Mixed-Use Development. Run-off from this basin enters the City of Cle Elum storm drainage system to the south.

Basin D:

Drainage Basin D is located east of Drainage Basin C, and consists of 317.75 acres of mixed forest land and pasture, with pasture being the predominant factor. Drainage Basin D is underlain with Teanaway loam soils. Only 29.78 acres of this basin is considered in the analysis, as the rest of the area will be by-passed via existing drainage routes. The analyzed area is located in the southern-most portion of Drainage Basin C, closest to the City of Cle Elum, and is limited to the proposed City Heights Planned Mixed-Use Development. Run-off from this basin enters the City of Cle Elum storm drainage system to the south.

Basin E:

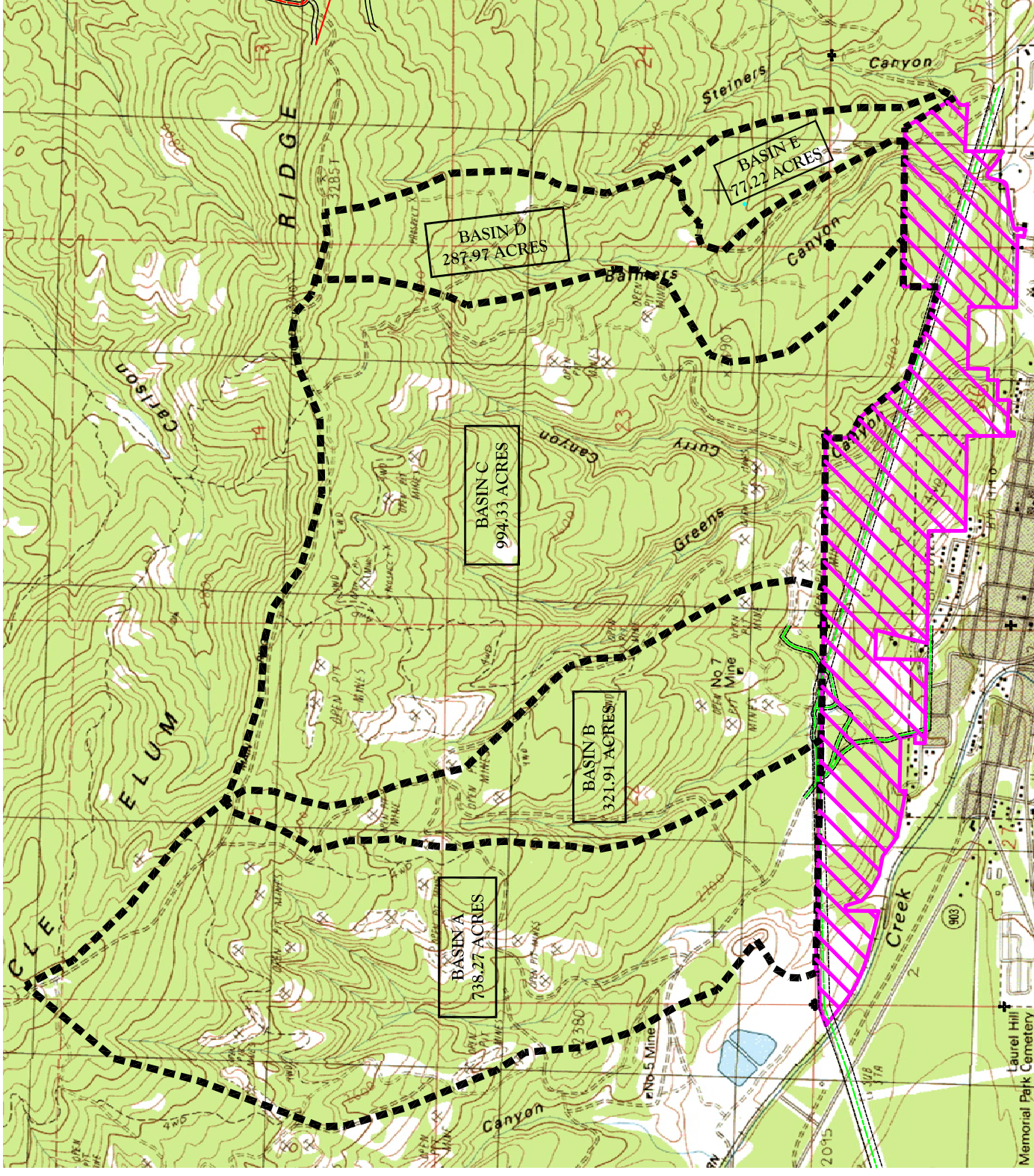
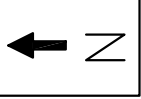
Drainage Basin D is located east of the southeast portion of Drainage Basin D, and consists of 83.51 acres of pasture land. Similar to Drainage Basin D, Drainage Basin E is underlain with Teanaway loam soils. Only 6.29 acres of this basin is considered in the analysis, as the rest of the area will be by-passed via existing routes patterns. The analyzed area is located in the southern-most portion of Drainage Basin C, closest to the City of Cle Elum, and is limited to the proposed City Heights Planned Mixed-Use Development. Run-off from this basin enters the City of Cle Elum storm drainage system to the south.

As it can be seen in the above descriptions, large portions of each site-specific basin are located upstream of the proposed City Heights project site. These upstream basins are not considered in the hydrologic analysis, and they will be by-passed via existing drainage routes that dissect the project site. On the overall scale, the upstream basins discharge directly to these existing drainage routes. Only small portions of the upstream basins, located along the northern property line, may sheet flow onto the project site. These amounts would not adversely affect the intent of this analysis and could be either included in the final storm drainage calculations/analysis or by-passed via proposed rock-lined swales along the northern property line.


3.1.4 Hydrologic Characteristics


Runoff modeling for the proposed City Heights Planned Mixed-Use Development was done using the Santa Barbara Urban Hydrograph method version 4.21B accepted by the Department of Ecology (Ecology) as a proper simulation modeling program. As required by Ecology's 2004 *Stormwater Management Manual for Eastern Washington* (SWMMEW), the run-off analysis is performed for the 2-year and 25-year events. Due to existing flooding issues downstream of the project site, the 100-year storm event was also analyzed. The average annual precipitation in the site area for the 24-hour duration is 2 inches for the 2-year storm, 3.5 inches for the 25-year storm, and 4.75 inches for the 100-year storm events based on Ecology's Isopluvial Maps for Eastern Washington. In order to account for the rain-on-snow event, a water equivalent value is calculated based on the average daily snow depth for Cle Elum and 20 percent moisture content, which is added to the average annual precipitation for each storm event. The water

Figure 3.2 – Upstream Storm Basin Map



Legend

 Upstream Storm Basin Boundary

 Project Site

Scale: 1" = 2000'

Figure 3.2
Upstream Storm Basin Map

November 23, 2009



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APPENDIX B

Off-Site Drainage System / Downstream Analysis

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Basin: West		Sub.		Sub. Number:		
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
see map	Type: Sheet flow, swale, stream, channel, pipe, pond. Size: diameter, surface area	Drainage basin, vegetation, cover, depth, type of sensitive area, volume	%	1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
A	6-ft bottom	Abundant natural veg.	2%	0'		
B	4-ft bottom	Abundant natural veg.	2%	10'-150'	Some erosion & ponding from narrowing channel above	
	4-ft bottom	Abundant natural veg.	2%	200'-400'	Naturally flowing	
C	6-ft bottom	Abundant natural veg.	2%	400'	Crk hits coal mine eroding fill @ bend in crk. Crk then follows N. edge of trail	
	5-ft bottom	Abundant natural veg.	2%-3%	400'-700'	Naturally flowing	
D		Crystal Crk. Crosses trail @NE corner Cie Elum Pines		700'	Joins streams	
	7-ft bottom	Abundant natural veg.	3%	700'-850'		
E	8-ft bottom		3%	850'	Stream bends into fill for coal mine trail	Sloughing & erosion of fill
	6-ft bottom		3%	850'-950'	Naturally flowing	
F	8-ft bottom		3%	950'	Sloughing & erosion on edge trail	
	6-ft bottom			950'-1100'	Naturally flowing	
G		No evidence of flooding		1100"	Boulder in crk for riprap (recent)	
H		Some erosion of fill on trail		1200'-1250'	Boulder in crk for riprap (recent)	
	6-ft bottom	Abundant natural veg.	3%+	1250'-1450'	Naturally flowing	
I		Concrete Bridge w/5' cm.p. CMP caved in some in center trail	3%	1450'	Flows under coal mine trail	

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Basin: West		Sub.		Sub. Number:		
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
see map	Type: Sheet flow, swale, stream, channel, pipe, pond. Size: diameter, surface area	Drainage basin, vegetation, cover, depth, type of sensitive area, volume	%	1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
I cont.		Riprap on corner 30' below bridge no evidence of erosion		1475'		
	8-ft bottom swale	Abundant Nat. Veg.	3%-4%	1475'-1600'	Naturally flowing	
J	10-ft bottom swale	Abundant Nat. Veg.	3%-4%	1600'	Bend in crk. Erosion of bank, underwelling outside bend	Trees & Debris Jams
	5-ft bottom swale	Abundant Nat. Veg.	3%-4%	1600'-1750'	Naturally flowing	
K	5-ft bottom swale	Abundant Nat. Veg.	3%-4%	1750'-1850'	Naturally flowing	Minor erosion S bank flooding N gradual slope
	5-ft bottom swale	Abundant Nat. Veg.		1850'-2000'	Naturally flowing	
L	6-ft bottom swale	Abundant Nat. Veg.	3%-4%	2000'-2100'	Flood canal to N	Evident flooding man made burn S.
M	6-ft bottom swale	Abundant Nat. Veg.	3%-4%	2200'	Eroding N bank under mining	
			3%-4%	2200'-2450'	Naturally flowing, minor erosion, evidence flooding	
N		Bridge Across Driveway	3%-4%	2450'		No obstructions
O				2475'	18" iron pipe exposed x-ing crk	
P	Bridge crossing 2nd St.	20-ft concrete deck	2500'			No obstructions
	7-ft bottom swale	Abundant Nat. Veg.	2%-3%	2525%-2700%	Naturally flowing	
Q	Wood bridge deck	15-ft wood deck	2%	2700'	Naturally flowing	No obstructions
		Natural veg.	2%	2700'-2900'	Flowing w/ minor ponding, some erosion riprap & obstructions	Veg. in stream

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Basin: West		Sub.		Sub. Number:		
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
see map	Type: Sheet flow, swale, stream, channel, pipe, pond: Size: diameter, surface area	Drainage basin, vegetation, cover, depth, type of sensitive area, volume	%	1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
R	Conc. Bridge x-ing 1st	20-ft concrete deck		2900"	Grass & Debris up stream causing ponding. Gravel & Debris under Bridge restriction flow.	
S	Wooden walk bridge			2950"		Severe erosion on dirt bank supporting bridge
	7-ft bottom swale	Abundant veg. w/ some debris in flow	2%	3000'-3000'	Flowing with minor obstructions	
T	Wood deck bridge in alley	Debris & sed. Restricting flow (minor)	1%-2%	3200'		
	8-ft bottom swale	Abundant veg.	2%	3200'-3350'	Flowing with minor debris obstructions	
	10-ft bottom swale	Vegetated w/ minor debris in crk	1%	3350'-4300'	Some slack water & ponding debris jam 75' upstream bridge restricting flow	No erosion restricting flow
	Conc. bridge x-ing S. Cle Elum way		1%	4300'		
U					Slack water under bridge & downstream alder cluster up hill bridge no other obstructions	
					18' cmp plastic corr.	
					Down side bridge heads west across into area w/ponding water & possible plugged culvert	
	12-ft bottom swale	Vegetated slack water		4300'-4500'	No obstructions	

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Basin: Summit View		Sub.		Sub. Number:		
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
see map	Type: Sheet flow, swale, stream, channel, pipe, pond: Size: diameter, surface area	Drainage basin, vegetation, cover, depth, type of sensitive area, volume	%	1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
	35-ft wide	Vegetated swale w/debris	3%-4%	450'-600'		
E	N side driveway	Swale narrows & bends to follow drive	2%-3%	600"	35' swale to v-ditch some erosion in constricted bend	
		Natural veg.	3%	600'-700'	Debris in crk not likely to restrict flow	
F	30'-40' wide sheet flow	Natural veg.	3%	700'-950'	Broad sheet flow thru thick veg. & debris new deposits of sand & gravel	
		Abundant nat. veg.		950'-1100'	Heavy veg. no erosion & no apparent restrictions	
		24" concrete culvert	2%-3%	1100'	Erosion along bank where crk 90's into culvert	
G		No obstruction in culvert				
		Natural veg.	1%-2%	1100'-1300'	Debris & veg. in ditch N apparent restrictions	
		1300' is ~ 100' upstream culvert xing@NE Cle Elum Pines				

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Basin:6th Street		Sub.		Sub. Number:		
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
	see map	Type: Sheet flow, swale, stream, channel, pipe, pond. Size: diameter, surface area		1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
A	18" plastic corr. 8" cmp		3%	0'	Dead skunks in 18" pipe otherwise ok	
	12" steel pipe					
	V-ditch	Heavily veg.	3%	0'-200'	Debris in ditch that do no appear to restrict flow	
	Sheet flow to v-ditch	Heavily veg.		200'-300'	Debris in ditch that do no appear to restrict flow	
B	18" cone culvert			300'		
					Main drainage starts 100' N 18" conc culvert @Base slag pile seeping out of bottom	
C	Flat bottom crk	Heavily veg. w/debris	2%	0-100'	Areas of ponding stagnant water	
	18" conc. Culvert			100'	Same as 300' above	
D	24" cmp other end 18"		2%	130'	Drops 2.5	
	3-ft bottom swale	Heavily veg.	2%	200'-600'	Naturally flowing thru veg.	
	2-ft bottom swale	Heavily veg.	2%	200'-600'	Naturally flowing thru veg. & debris	

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Basin: 6th Street		Sub.		Sub. Number:		
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
see map	Type: Sheet flow, swale, stream, channel, pipe, pond. Size: diameter, surface area	Drainage basin, vegetation, cover, depth, type of sensitive area, volume	%	1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
E		3-18" conc. Culv.		600'	N. plugged-S. unobstructed-middle 1/2 filled gravel	
				630'	Other end culverts under trail. All 3 partially blocked heavily veg.	
		2-ft bottom	2%	630'-850'	Heavily veg. no restriction to water flow	
F		18" conc. w/1" plastic pipe/w trash rack		850'	Appears to have no obstructions	12" cmp enters up stream of 18" conc. Along w/1" plastic pipe in 18" conc.
					No direction of flow from 18" conc. w/trash pack to 302 Stafford Rd.	
G		24" cmp.		~1250'	Can't find other end culvert	
		2-ft bottom	2%	1250'-1375'	Grass in ditch no restriction	
H		24" cmp		1375'-1400'		
		4-ft bottom	2%	1400'-1475'	No restrictions	
I		2-24" conc.		1475'-1550"	No restrictions	
		4-ft bottom		1550'-1600'	No restrictions Trib. 50' up from wooden bridge 2450	
					Go to Basin: West, pg2	

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

	Basin: Peoh		Sub.		Sub. Number:	
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
see map	Type: Sheet flow, swale, stream, channel, pipe, pond. Size: diameter, surface area	Drainage basin, vegetation, cover, depth, type of sensitive area, volume	%	1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
A	18" Wooden @ culvert	Prop-Line Rd. x-ing	3%-4%	0-30	No obstructions in culvert	
	2-3 ft bottom swale	Heavy Veg. grass/shrubs	5%-6%	30'-100'	Naturally flowing	
	10-20 ft bottom swale	Heavy Veg. grass/shrubs	10%-15%	100'-230'		
B	Sheet flow thru alley	No culverts		230	Area of concern, 1 small cb nearby & no culverts	
C	CB SE of 90° bend in alley	6" ductile iron out to (s)		275	Grass around lid, not in best condition to catch water, sed to bottom pipe	
D	CB SE 4th/4-s alley	18" plastic corr. In (N) &out (S)		415	CB in good working condition	
E	CB 3rd/Alley to N	18" Plastic Corr. In (N0 12" PVC out (S)		575	CB in good working condition	
F	CB 24" cmp stand pipe w/round CB lid				No pipes visible 4' down to H2O/sediment	

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Basin: Montgomery		Sub.		Sub. Number:		
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
see map	Type: Sheet flow, swale, stream, channel, pipe, pond. Size: diameter, surface area	Drainage basin, vegetation, cover, depth, type of sensitive area, volume	%	1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
A	(1.) 36" cmp (2.) 30" cmp		1%	A-B ~ 350'		Under Montgomery Rd.
B	Fenced Stretched Across channel		1%-2%	B-C ~ 100'	Possible flow Restriction	
C	Building built over channel			C-D ~ 50'	Wood Bracing not stable	Building set on ~4' concrete walls @ East + West edges of channel w/wooden braces in water @ mid span
D	Channel enters tunnel			D-E ~ 350'		Arched tunnel measuring 3.8' wide X 4.0' high w/concrete wind walls + concret armored bank
E	Man hole lid (no manhole)			E-F ~ 850'		Ring and lid set in gravel enclosing capped 6" ABX stub set vertically, directly over tunnel
F	Vault w/round lid			F-G ~ 200'		Hand made vault uneven shape cannot see in-flow from north 36" concrete out flow heading east

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Basin: Montgomery		Sub.		Sub. Number:		
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
see map	Type: Sheet flow, swale, stream, channel, pipe, pond. Size: diameter, surface area	Drainage basin, vegetation, cover, depth, type of sensitive area, volume	%	1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
G	Vault (Round lid)	Custom Vault odd-shaped		G-H ~ 250'		36" concrete in-flow from west cannot see out flow to east
H	Vault (Round lid)	Flowing West to East		H-I ~ 300'		Unable to see in flow or out flow
I	Vault (Round Lid)	Flowing West to East		I-J ~ 400'		Unable to see inflow or outflow
J	Out flow to swale	Outflow pipe is 44" wide by 48" high concrete arch pipe				Swale flows East
K	6' diameter cmp under paved st.	~ 60' long	1%	K-L ~ 100'		Ditch w/~36" homemade metal culvert enters swale @ W. end 6' culvert
L	5' tall X 6' wide cmp squash pipe under paved parking lot entry	~ 40' long	<1%	L-M ~ 120'		
M	Same description as "L"		<1%	M-N ~ 120'		

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Basin: Montgomery		Sub.		Sub. Number:		
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
see map	Type: Sheet flow, swale, stream, channel, pipe, pond. Size: diameter, surface area	Drainage basin, vegetation, cover, depth, type of sensitive area, volume	%	1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
N	6' wide X 4' tall cmp squash pipe	~ 50' long running under paved st.	<1%	N-O ~ 400'		Partially silted @ E. end
O	Wire fence stretched across channel		<1%	O-P ~ 75'	Possible flow restriction	
P	3' tall X 4' wide cmp squash pipe under farm crossing		<1%	P-Q ~ 125'		Pipe beat up & misshapen
Q	Fence stretched across channel		<1%	Q-R ~ 25'		Suspended above H20 no flow restriction
R	6' wide X 4' high cmp squash pipe	Under paved street	<1%	R-S ~ 175%		~30' long pipe
S	6' wide X 4' deep concrete box culvert	~ 55' long under SR970		S-T ~ 70'		
T	7' wide x 4' high concrete box culvert	~25' long	1%	T-U ~ 50'		Bottom partially silted

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

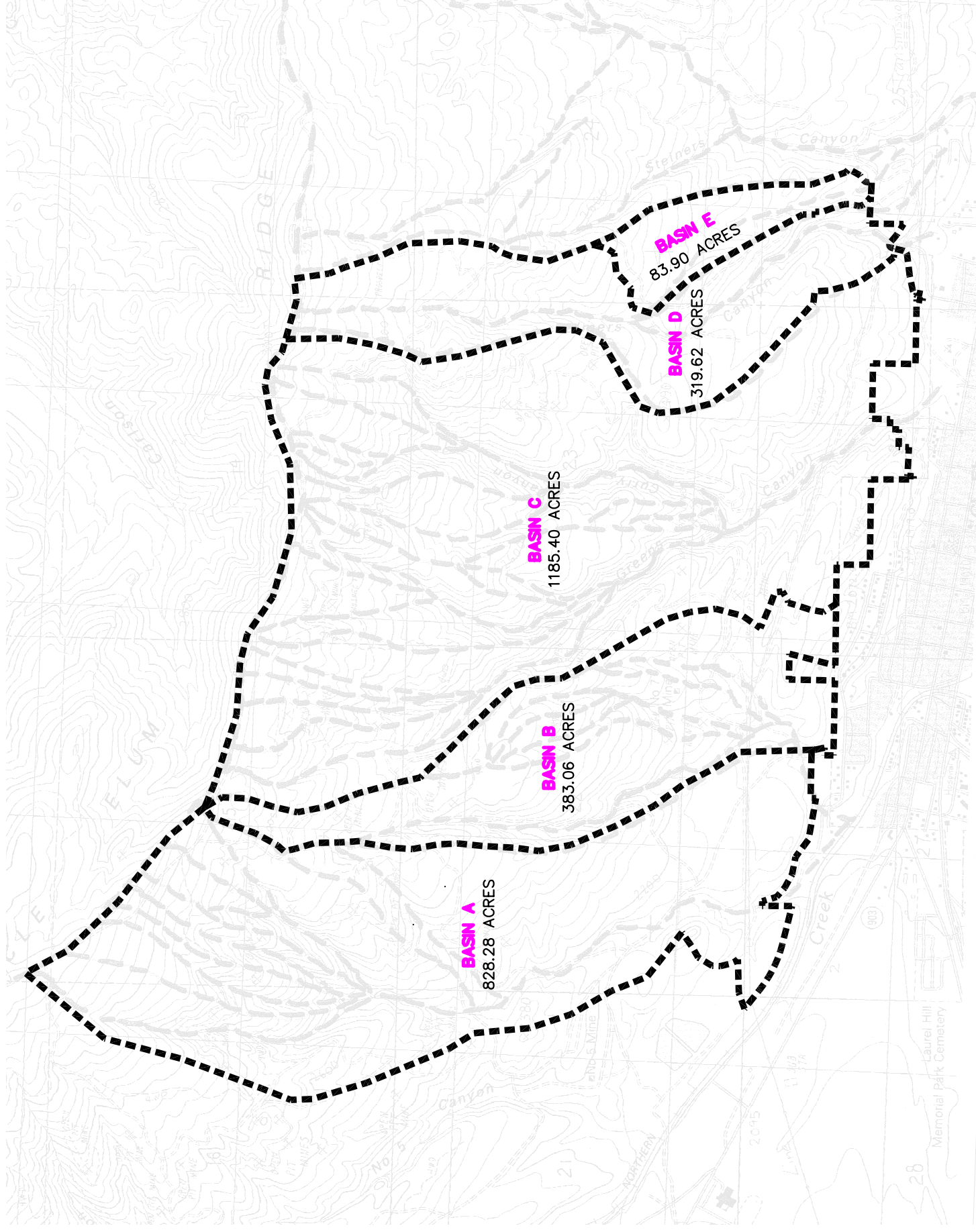
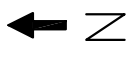
Basin: Montgomery		Sub.		Sub. Number:		
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
see map	Type: Sheet flow, swale, stream, channel, pipe, pond. Size: diameter, surface area	Drainage basin, vegetation, cover, depth, type of sensitive area, volume	%	1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
U	36" cmp culvert	~ 30' long under dirt rd.	1%	U-V ~ 70'		
V	36" cmp culvert	~20' long	1%	V-W ~ 70'		
W	(2) 48" concrete culverts (side by side)	~40' running under RR tracks	2%	W-X ~ 50'		
X	48" cmp culvert	~20' long running under gravel rd.	1%	X-Y ~ 250'		
Y	36" diameter DIP suspended over H20		1%-2%	Y-Z ~1300'		Connects flowing ditch south to north. No flow restriction
Z	Wire fence suspended over channel		1%	Z-AA ~600'		No flow restrictions
AA	Bend in Stream		1%-2%			
BB	Creek feeds swamp	Swamp filled w/cat tails to N. of bend in stream	<1%	BB-CC ~1200'		Definite H20 detention area
CC	Bend in creek		1%	CC-DD ~ 550'		
DD	6' diameter concrete culvert	Flowing under overpass for freeway on ramp ~150' long culvert	2%	DD-EE ~ 1300'		

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Basin: Columbia		Sub. #4		Sub. Number:		
Symbol	Drainage, Component Type, Name and Size	Drainage Component Description	Slope	Distance from site discharge	Existing Problems/Potential Problems	Observations of field inspector, resource reviewer, or resident
	see map	Type: Sheet flow, swale, stream, channel, pipe, pond: Size: diameter, surface area	%	1/4 mi = 1,320 ft.	Constrictions, under capacity, ponding, overtopping, flooding, habitat or organism destruction, scouring, bank sloughing, sedimentation, incision, other erosion	Tributary area, likelihood of problem overflow pathways, potential impacts
A	24" Black Plastic Corrugated Pipe	~ 40' long under gravel rd.	1%	A-B ~ 140'		Channel splits for ~ 120'
B	18" cmp culvert under gravel DW		4%	B-C ~ 100'		Channel re-joins
C	30" cmp culvert	Under gravel rd.	3%	C-D ~ 250'		
D	24" cmp culvert	Under paved st.	3%-4%	D-E ~ 150'		
E	24" Black corrugated plastic pipe	~ 20' long buried in rip-rap & dirt	3%-4%	E-F ~ 125'		Pipe laid to protect SSMH @ W. Edge ditch from washout
F	Bend in channel 18" cone culvert	90° turn to E.	1%-2%	F-G ~ 125'		Channel B joined by small ditch from W.
G	18" cone culvert	~ 55'	1%-2%	G-H ~ 225'		S. ~ 10' of culvert is 24" cmp sleeved over concrete
H	Homemade ~36" culvert under concrete SW	~ 10' long made of old fuel tank w/ends cut out	2%-3%	H-I ~ 15'		
I	Dumps into Montgomery Downstream		2%-3%			
		(See location "K" in Basin: Montgomery)				

APPENDIX C

Project Specific Sub-basins Map



Scale: 1" = 2000'

Figure C.1
Project Specific Sub-Basins

November 23, 2009



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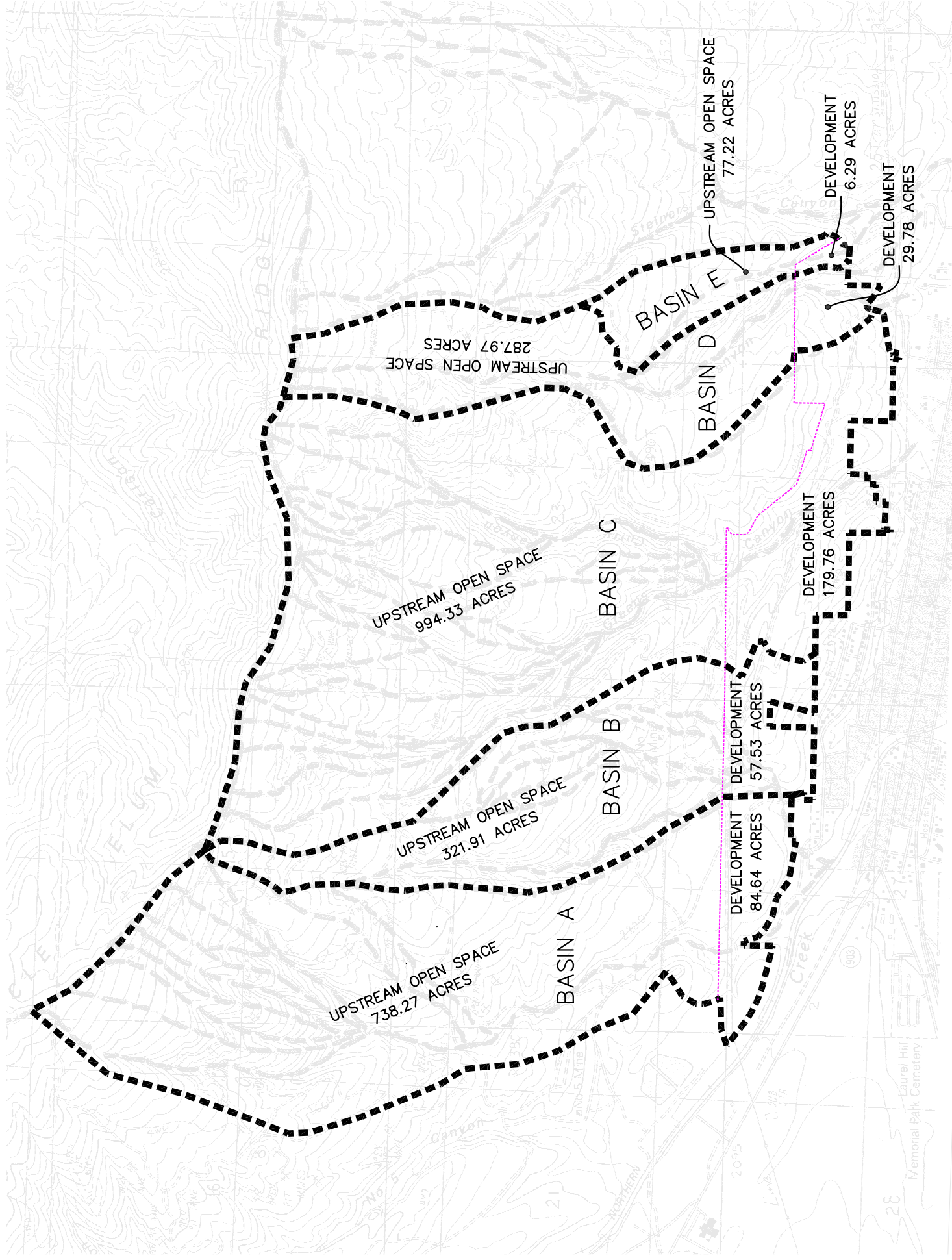
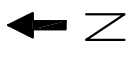


Figure C.2
Pre-Development Sub-Basins Breakdown

Scale: 1" = 2000'

November 23, 2009



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**Downstream Drainage Analysis prepared by Barghausen Consulting Engineers, Inc.,
dated February 25, 2011**

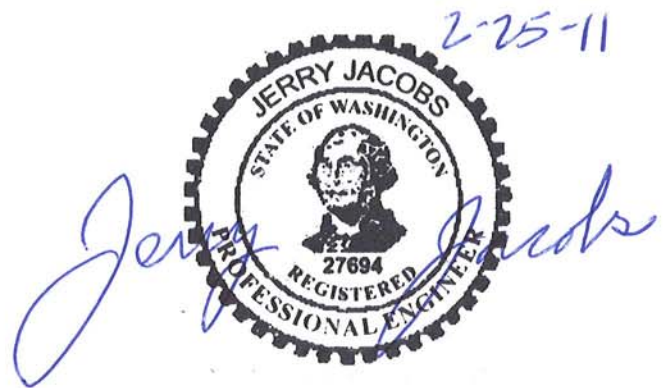


DOWNSTREAM DRAINAGE ANALYSIS

Proposed City Heights Project Cle Elum, Washington

Prepared for:
Green Canyon LLC / High Mark Resources LLC / Cooper Pass LLC
206 West First Street
Cle Elum, Washington 98922
(509) 674-6828

February 25, 2011
Our Job No. 14953



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EXHIBIT B BASIN MAP

EXHIBIT C DOWNSTREAM DRAINAGE COURSE MAP

EXHIBIT D FEMA MAP

EXHIBIT E BASIN SUMMARIES TO DETERMINE FLOW RATES

EXHIBIT F ANALYSIS OF CAPACITIES AND CONVEYANCE PIPES FOR EACH BASIN

1.0 INTRODUCTION / GENERAL INFORMATION

INTRODUCTION/GENERAL INFORMATION

The 358-acre site of the City Heights planned mixed-use development is located within the Urban Growth Area north of the City Limits of Cle Elum in Kittitas County, Washington. The site is within an upland region above the Yakima River Valley on the south face of Cle Elum Ridge, bounded to the south by the Mine Heritage Trail, West 6th Street, West 5th Street, East Russ Street, North Montgomery Avenue, East 3rd Street, North Columbia Avenue, and West Cemetery Road, and to the north by undeveloped woodlands and former coal mine areas. Please refer to the Vicinity Map.

Encompass Engineering and Surveying, a company located in Cle Elum, Washington, prepared a detailed grading, drainage, and utilities technical engineering report for this overall development dated March 24, 2010. In that report, a preliminary off-site analysis was performed on all of the drainage basins draining through the City Heights project and through the City of Cle Elum to the Yakima River further downstream. In that analysis several problem areas were identified. In addition, based on conversations with City personnel and site visits, one in January 2010 and one in February 2011, our office performed a subsequent analysis of the downstream drainage system based on City personnel's indications of downstream drainage problems occurring within the City of Cle Elum.

The proposed City Heights project site is within a watershed located on the north side of the City of Cle Elum, encompassing an area from the town of Roslyn on the west, Cottage Avenue in the City of Cle Elum on the east, the top of the Cle Elum Ridge on the north, Third Street and SR-903 within the City of Cle Elum on the south.

The proposed City Heights property hydrology is divided into four significant drainage basins.

Basin A (West Basin)

Drainage Basin A is located in the western portion of the project and consists of approximately 777 acres of forest land. Runoff from this basin contributes to the headwater of Crystal Creek to the southwest. The West Basin is the westernmost downstream basin that drains directly into Crystal Creek.

Basin B (Summit View Basin)

Drainage Basin B is located east of Drainage Basin A and consists of approximately 449 acres of mixed forest land and pasture. Runoff from this basin enters Crystal Creek downstream of Basin A. Summit View Basin begins at Summit View Road and heads southwest across private property and into Crystal Creek. Please refer to the Downstream Drainage System Map in Exhibit C for more detail. Approximately seven (7) acres of the drainage basin known as Sixth Street Basin is also tributary to the downstream conveyance system for Basins A and B. Sixth Street Basin begins on Sixth Street near the City of Cle Elum water tank and heads west, then south, and into Crystal Creek.

Basin C (Montgomery Basin)

Drainage Basin C is located east of Drainage Basin B and consists of approximately 1,124 acres of mixed forest land and pasture. Runoff from this Basin is tributary to the Second Street storm system within the City of Cle Elum.

Approximately 10 acres of the drainage basin known as Peoh Basin is also tributary to Basin C, known as Montgomery Basin. Peoh Basin begins at the north end of Peoh Street and heads south into the City's Second Street stormwater conveyance system. Montgomery Basin begins at Montgomery Avenue and heads southeast across private land and into the City Second Street stormwater conveyance system.

Basin D (Columbia Basin)

Drainage Basin D is located east of Drainage Basin C and consists of approximately 300 acres of mixed forest land and pasture. Storm runoff from this basin drains to the same downstream conveyance system as Basin C, connecting up at Second Street and then flowing east, ultimately draining to the Yakima River. Columbia Basin begins at the extension of Columbia Avenue (also known as Creekside Road) and heads south into the City's Second Street stormwater conveyance system.

A detailed description of each downstream basin from the City Heights property to the Yakima River is provided in the Downstream Drainage System Map within the Appendix of this report.

FEMA has performed a flood analysis of Crystal Creek coursing through the City of Cle Elum. Based on the FEMA study, portions of West Second Street and West First Street between Bullitt Avenue and Stafford Avenue are within a Zone B floodplain. Zone B is designated as the area between limits of the 100-year flood and the 500-year flood, or certain areas subject to 100-year flooding with average depth less than 1 foot, or where the contributing drainage area is less than 1 square mile, or areas protected by levies from the base flood.

The entire City of Cle Elum and its Urban Growth Area are acknowledged as being located within a highly erosive area susceptible to frequent flooding. Many flooding events have occurred in recent years from the poorly maintained and deteriorated drainage structure and undersized storm drainage system within the City Limits.

The development of the project site would create a large amount of impervious surface and decrease the amount of pervious area, therefore increasing the duration of the peak surface water runoff. Due to the existing flooding issue downstream of the project site, 100-year storm event detention for the developed runoff is proposed to be implemented to maintain existing runoff rates to the downstream system.

Given that the proposal will comply with all applicable stormwater management regulations under the developed condition, and the project proposes to detain the 100-year storm event based on past flooding experiences in the area, any storm and/or flood events beyond the 100-year storm event is considered unavoidable adverse impact.

A basin analysis is performed to determine an estimated 100-year peak flow rate for each basin and then analysis of the conveyance pipe and ditches was performed to determine adequate capacity to convey the flow from each basin. The majority of the conveyance pipes analyzed were determined to be undersized; however, it should be noted that the Santa Barbara Urban Hydrograph (SBUH) methodology uses to estimate the peak flow creates higher than actual flow rates, especially for forested and pasture conditions, which most of the upstream basin consists of.

The City Heights project will provide flow control matching the 2-year, 25-year, and 100-year release rate to match the pre-developed runoff rate for the area of the City Heights project contributing to each basin, thereby there should be no impact to the peak flow rate coming into the City from this project. However, the duration of the peak flow will increase. Sediment accumulation in the conveyance system from all of the basins appears to be a major problem in the City of Cle Elum.

Vactoring out the catch basins and conveyance pipes from the City mains and removal of the excess vegetation within the open channels must be implemented to increase flow rates through the City conveyance system.

Conclusions and Recommendations

A detailed description of each downstream basin from the City Heights property to the Yakima River, including tributary area, estimated 100-year peak flow rate, and recommendations to minimize flooding problems are provided in the Drainage System Table in Appendix C.

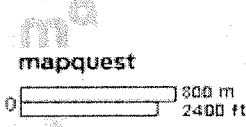
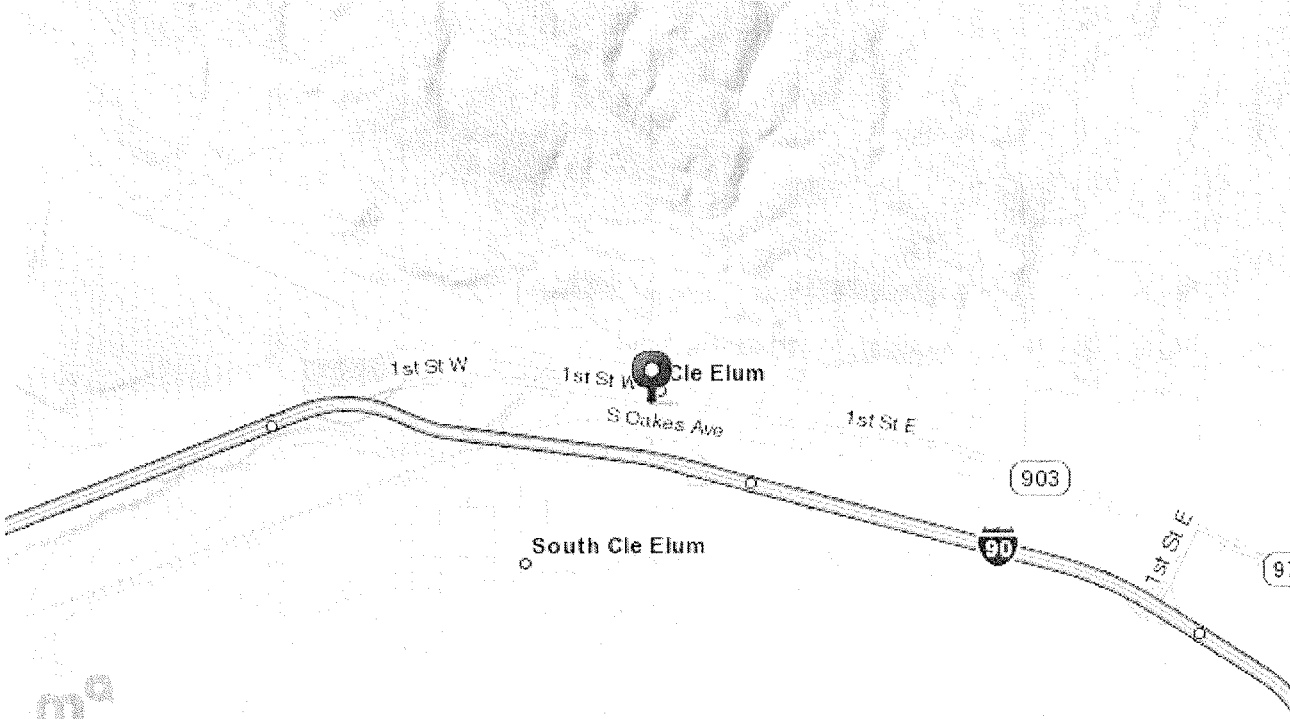
VICINITY MAP



Notes

Map of:

119 W 1st St
Cle Elum, WA 98922-1105



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APPENDIX

EXHIBIT A
OFF-SITE ANALYSIS DRAINAGE SYSTEM
TABLE

West Basin

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Drainage Component Type/Size (see map)	Condition	Estimated 100-Year/24-Hour Flow Rate (cfs)	Existing/Potential Problems	Action Recommended
A 6-foot-wide channel bottom	Abundant vegetation	284 cfs		No action required
B 4-foot bottom	Abundant vegetation		Some erosion	No action required
C 6-foot bottom	Abundant vegetation		None noted	No action required
D 7-foot bottom	Creek crosses trail		None noted	No action required
E 8-foot bottom		407 cfs	None noted	No action required
F 8-foot bottom			Sloughing and erosion on trail edge	No action required
G 6-foot bottom	No evidence of flooding		None noted	No action required
H 6-foot bottom	Some erosion of fill on trail		None noted	No action required
I 5-foot CMP culvert	CMP caved in some in trail center		None noted	No action required
J 10-foot bottom	Abundant vegetation		Trees and debris jams	Remove excess vegetation, trees, and debris jamming channel.
K 5-foot bottom	Abundant vegetation		Minor erosion on south bank	Place riprap on south bank and repair erosion.
L 6-foot bottom	Abundant vegetation		Evident flooding	Remove excess vegetation, trees, and debris jamming channel.
M 6-foot bottom	Abundant vegetation		Minor erosion and flooding evidence	Place riprap and repair erosion
N Bridge	Across driveway		None noted	No action required
O			None noted	No action required
P Bridge crossing 2nd Street	20-foot concrete deck		None noted	No action required
Q Wood bridge	15-foot wood deck		None noted	No action required
R Bridge crossing 1st Street	20-foot concrete deck		Some erosion and obstructions downstream of bridge	Remove obstructions in channel.
S Wooden walk bridge 7-foot bottom	Abundant vegetation with some debris		Grass and gravel upstream causing ponding. Gravel and debris under bridge. Severe erosion in channel supporting bridge	Remove grass, gravel, and debris upstream and under bridge. Place riprap in side slope of channel and repair erosion.

West Basin

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Drainage Component Type/Size (see map)	Condition	Estimated 100-Year/24-Hour Flow Rate (cfs)	Existing/Potential Problems	Action Recommended
T Wood bridge in alley	Debris and sediment restricting flow		Minor debris obstructions downstream of bridge	Remove debris and sediment in channel
10-foot bottom	Vegetated with minor debris		Debris jam in channel	Remove debris jam in channel.
U 12-foot bottom	Vegetated slack water		None noted	No action required
V Concrete bridge under railroad tracks	10- by 7-foot RCB		No obstructions	No action required

Summit View Basin

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2				
Drainage Component Type/Size (see map)	Condition	Computed SBUH 100-Year Flow Rate (cfs)	Existing/Potential Problems	Action Recommended
A 48-inch CPEP Culvert Discharges to 10-foot-wide bottom swale	Unobstructed	127 ± * 100-year flow rate was computed by SBUH methodology, which appears to be yielding inflated flow rates.	Some debris that is not disrupting flow	No action required
B Old bridge crossing			Bridge and debris restrict flow	No action required
C V-shape channel 1:1 side slopes	Fallen trees in channel		Mass erosion undercut banks	No action required
D 20- to 35-foot-wide bottom	New sediment in stream		None noted	No action required
E Swale narrows	Follows north side driveway		Some erosion in bend	No action required
F 30- to 40-foot-wide swale to 24-inch RCP	Abundant vegetation		Erosion along bank where creek bends into culvert	Replace 24-inch RCP with 48-inch culvert with wing walls
G				

6th Street Basin

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Drainage Component Type/Size (see map)	Condition	Estimated 100-Year/24-Hour Flow Rate (cfs)	Existing Potential Problems	Action Recommended
A 18-inch CPEP 8-inch CMP 12-inch steel pipe discharge to V-ditch	Pipes clear. V-ditch heavily vegetated.		Debris in ditch does not appear to restrict flow	No action required
B 18-inch RCP			None noted	No action required
C Flat bottom creek	Heavily vegetated with debris		Areas of ponding	No action required
D 18-inch RCP to 24-inch CMP			None noted	No action required
E Three 18-inch RCPs			N. plugged, S. clear, middle 1/2 filled with gravel	Clean out sediment
F 18-inch RCP			No obstructions	No action required
G 24-inch CMP	Partially filled with sediment		Downstream end buried	Clean out sediment
H 24-inch CMP	Partially filled with sediment			Clean out sediment
I Two 24-inch RCPs	Clear		No restrictions	No action required

Peoh Basin

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Drainage Component Type/Size (see map)	Condition	Estimated 100-Year/24-Hour Flow Rate (cfs)	Existing/Potential Problems	Solution to Flooding Problem
A 18-inch wood culvert 2- to 3-foot bottom swale 10- to 20-foot bottom swale	Prop. – Line Rd. x-ing Heavily vegetated Heavily vegetated		No obstructions	The Peoh basin has a very small upstream contributing area of approximately 26 acres of forest. The flows from this area are minor compared to the other basins. City personnel did not indicate any flooding problems in this downstream course; however, it appears from the field reconnaissance that several of the catch basins need to be vactored.
B Sheetflow through alley	No culverts		None noted	No action required
C Catch basin southeast of bend in alley	6-inch DIP out to south		Sediment of IE to pipe	No action required
D 18-inch CPEP	Catch basin to catch basin		Catch basin in good condition	No action required
E Catch basin in 3rd Street alley to north	18-inch CPEP in 12-inch PVC out		Catch basin in good condition	No action required
F Catch basin 24-inch standpipe			Full of water and sediment	No action required

Montgomery Basin

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2			
Drainage Component Type/Size (see map)	Condition	Estimated 100-Year Flow by SBUH (cfs)	Existing/Potential Problems
A 36-inch CMP 30-inch CMP		362* * Since the 100-year flow rate was computed by SBUH, the rate is likely highly inflated.	None noted City has indicated that there are flooding problems in this downstream course. 36-inch and 30-inch culverts are likely needed to be replaced with larger.
B Fence across channel			Possible flow restriction
C Building built over channel			Wood bracing in center of channel not stable
D Channel enters tunnel	3.8 feet wide and 4.0 feet high with concrete wing walls		None noted
E Manhole lid (no MH)	Covers 6-inch stub over tunnel		None noted
F Vault with round lid	36-inch RCP out to east		None noted
G Vault odd shaped (custom built)	36-inch RCP in from west		Cannot see outflow
H Vault	Flowing west-to-east		Cannot see inflow or outflow pipes
I Vault	Flows west-to-east		None noted
J 44-inch-wide by 48-inch-high arch pipe	Outflows to swale		Swale flows east
			No action required
			No action required

Montgomery Basin

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Drainage Component Type/Size (see map)	Condition	Estimated 100-Year Flow by SBUH (cfs)	Existing/Potential Problems	Action Recommended
K 6-foot-diameter CMP	Under paved street	492 cfs*	Ditch and 36-inch culvert enter swale at west end of 6-foot CMP	No action required
L 5- by 6-inch arch pipe	Under paved parking lot entry		None noted	No action required
M			None noted	No action required
N 6-foot-wide by 4-foot-high CMP arch	Under paved street		Partially silted at east end	Remove accumulated sediment from bottom of culvert
O Wire fence across channel			Possible flow restriction	No action required
P 3-foot-high by 4-foot-wide CMP arch	Under farm crossing		Pipe beat up and misshapen	Replace arch culvert
Q Fence across channel	Suspended above water		No restriction	No action required
R 6-foot-wide by 4-foot-high CMP arch	Under paved street		30-foot-long pipe	No action required
S 6- by 4-foot RCB	Under SR-970		55-foot long	No action required
T 7- by 4-foot RCB	Bottom partially silted		25 feet long	No action required
U 36-inch CMP culvert	Under dirt road		30 feet long	Locations U, V, W, X, and Y all are culverts smaller in diameter than the upstream culverts contributing. They have to be upsized.
V 36-inch CMP			20 feet long	
W Two 48-inch RCP culverts	Side by side		Under railroad tracks	
X 48-inch CMP	Under gravel road		20 feet long	
Y 36-inch DIP	Suspended over water		No restriction	
Z Wire fence	Suspended over channel		No restriction	No action required
AA Bend in stream			None noted	No action required
BB Creek feeds swamp			Stormwater detention area	No action required
CC Bend in creek			None noted	No action required
DD 72-inch RCP	Under freeway overpass		150 feet long	No action required
EE	Change in channel vegetation		None noted	No action required

Montgomery Basin

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Drainage Component Type/Size (see map)	Condition	Estimated 100-Year Flow by SBUH (cfs)	Existing/Potential Problems	Action Recommended
FF Pond inlet to stream	Beaver dam		Partial flow restriction	No action required
GG Stream meets river			None noted	No action required

Columbia Basin				
OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2				
Drainage Component Type/Size (see map)	Condition	Estimated SBUH 100-Year Flow (cfs)	Existing/Potential Problems	Action Recommended
A 24-inch CPEP	Under gravel road 40 feet long	138 cfs* * Flows determined with SBUH are substantially higher than what actually occurs, especially in a forested or pasture condition, which these basins are modeled as.	Channel splits for approximately 120 feet	The City has indicated there are flooding problems in this Columbia Basin downstream drainage course. Based on the slopes given, all of these culverts are undersized.
B 18-inch CMP culvert	Under gravel driveway		Channel reconnects	The City has indicated there are flooding problems in this Columbia Basin downstream drainage course. Based on the slopes given, all of these culverts are undersized.
C 30-inch CMP culvert	Under gravel road		None noted	The City has indicated there are flooding problems in this Columbia Basin downstream drainage course. Based on the slopes given, all of these culverts are undersized.
D 24-inch CMP culvert	Under paved street		None noted	The City has indicated there are flooding problems in this Columbia Basin downstream drainage course. Based on the slopes given, all of these culverts are undersized.

Columbia Basin

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Drainage Component Type/Size (see map)	Condition	Estimated SBUH 100-Year Flow (cfs)	Existing/Potential Problems	Action Recommended
E 24-inch CPEP	20 feet long		None noted	The City has indicated there are flooding problems in this Columbia Basin downstream drainage course. Based on the slopes given, all of these culverts are undersized.
F 18-inch RCP culvert	Bend in channel		None noted	The City has indicated there are flooding problems in this Columbia Basin downstream drainage course. Based on the slopes given, all of these culverts are undersized.
G 18-inch RCP culvert	55 feet long		None noted	The City has indicated there are flooding problems in this Columbia Basin downstream drainage course. Based on the slopes given, all of these culverts are undersized.
H 36-inch culvert	Under sidewalk, 10 feet long		Homemade from old fuel tanks	The City has indicated there are flooding problems in this Columbia Basin downstream drainage course. Based on the slopes given, all of these culverts are undersized.

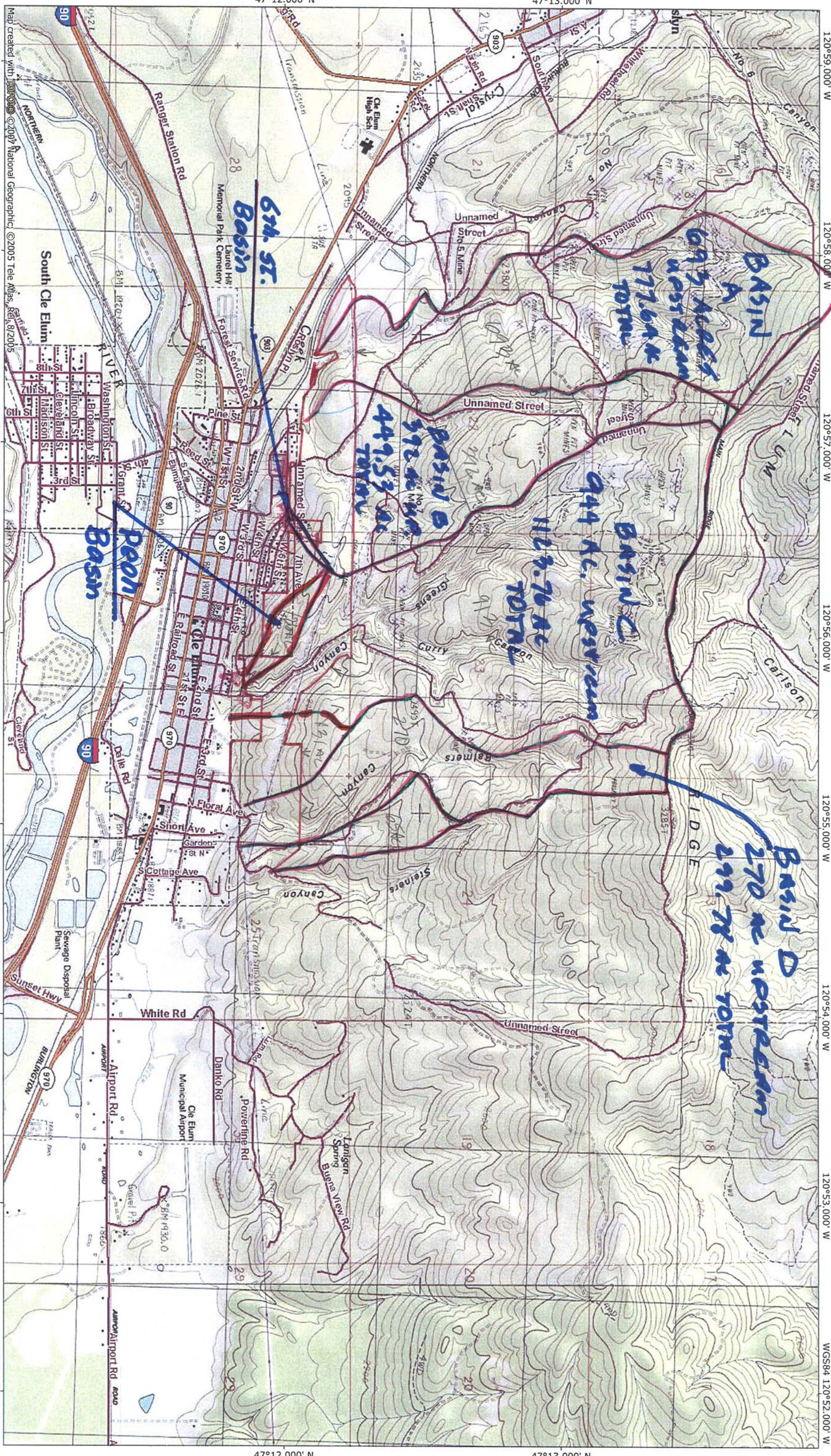
Columbia Basin

OFF-SITE ANALYSIS DRAINAGE SYSTEM TABLE SURFACE WATER DESIGN MANUAL, CORE REQUIREMENT #2

Drainage Component Type/Size (see map)	Condition	Estimated SBUH 100-Year Flow (cfs)	Existing/Potential Problems	Action Recommended
I Connects to Montgomery downstream				The City has indicated there are flooding problems in this Columbia Basin downstream drainage course. Based on the slopes given, all of these culverts are undersized.

These are an indication of channel/culvert capacity problem. All existing culverts must be replaced with minimum 36-inch culverts.

**EXHIBIT B
BASIN MAP**



Map created with  ©2007 National Geographic. ©2005 Tele Atlas, Rel. 8/2005



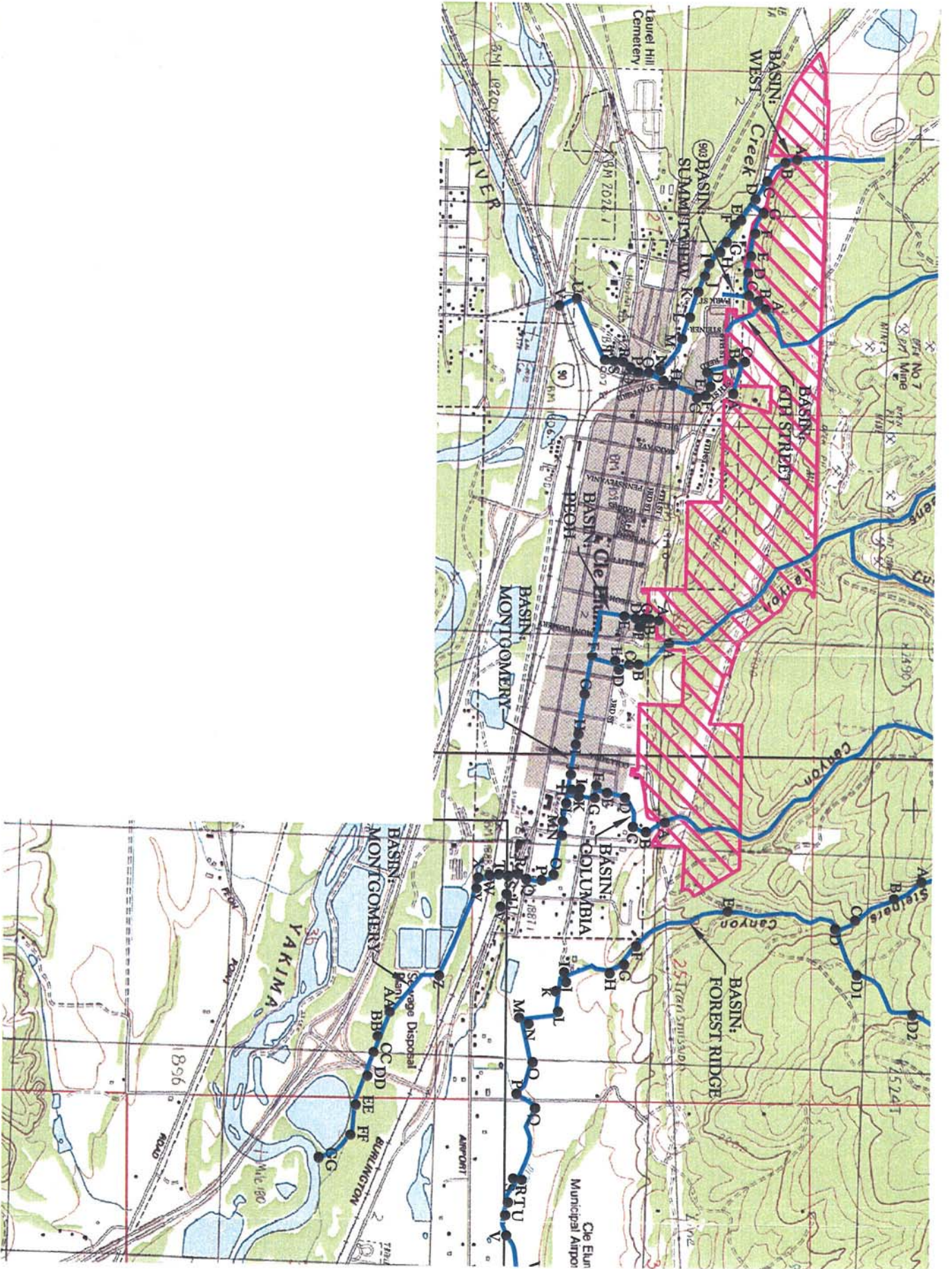
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 16 1/2°
 WGS84 120°52.000' W

47°12.000' N 47°13.000' N

120°59.000' W 120°58.000' W 120°57.000' W 120°56.000' W 120°55.000' W 120°54.000' W 120°53.000' W 120°52.000' W

47°12.000' N 47°13.000' N

EXHIBIT C
DOWNSTREAM DRAINAGE COURSE MAP



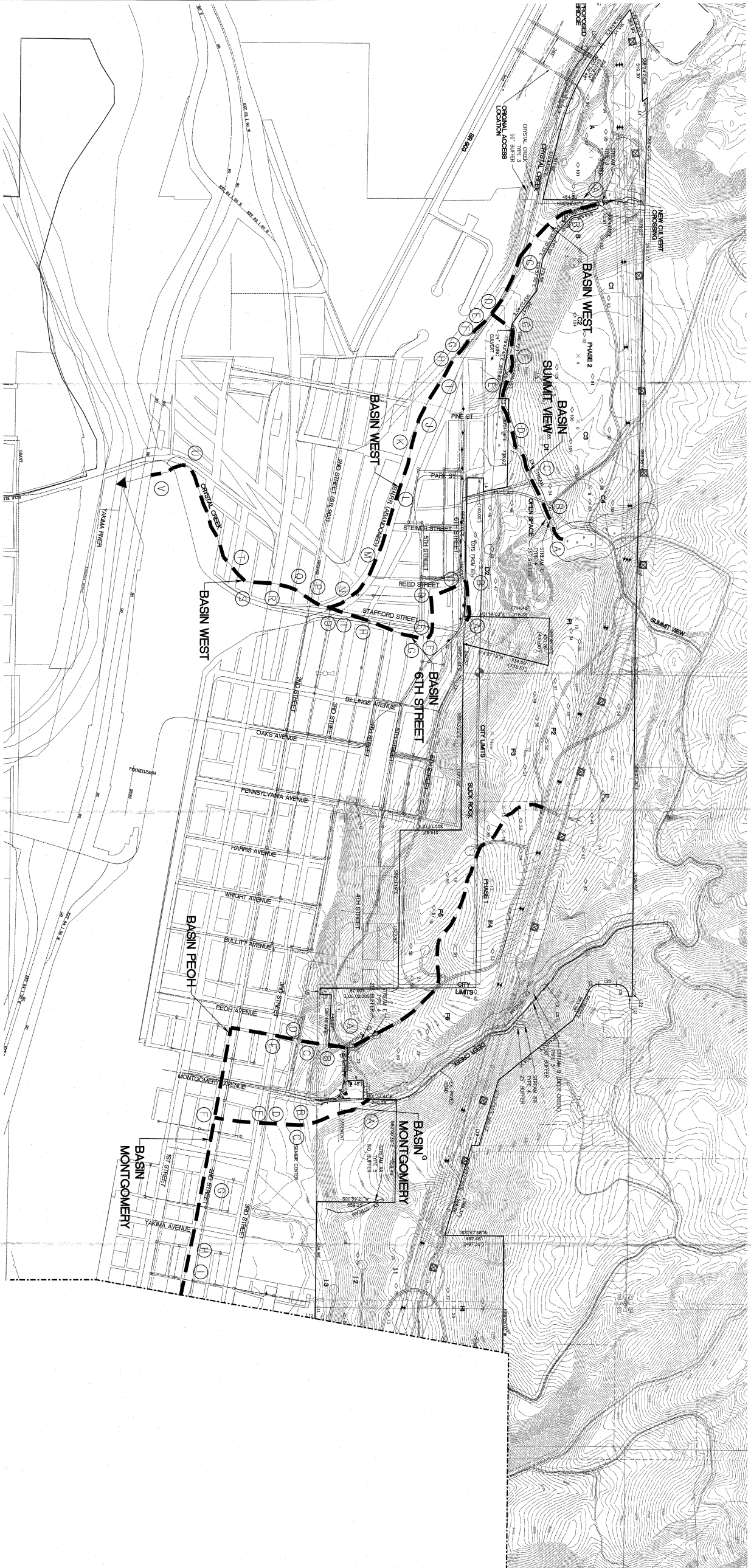
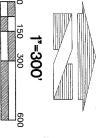
Legend

- A See Downstream Table for Site Description
- Downstream Path
- ▨ Project Site

Scale: 1" = 2000'

Downstream Drainage System

November 23, 2009



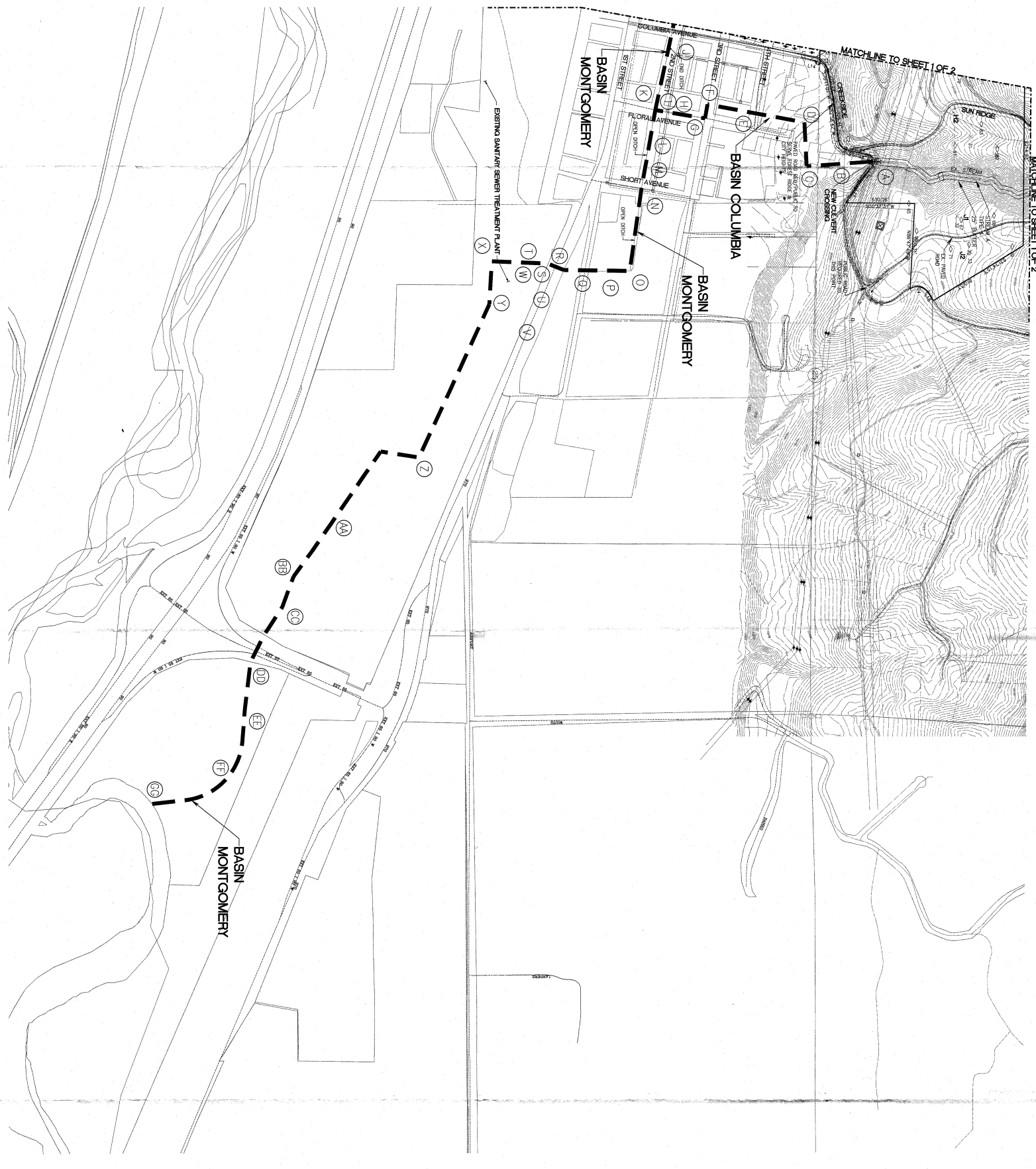
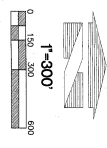
LEGEND

	DOWNSTREAM DRAINAGE LINE
	PROPOSED BASIN
	ALTERNATIVE BASIN LOCATION
	PROPOSED BRIDGE
	STORM DRAINAGE CATCHER
	TEST PIT LOCATION
	EXISTING POWER POLE
	EXISTING TRANSMISSION TOWER

TOTAL ESTIMATED EARTHWORK QUANTITIES FOR CONSTRUCTION OF THE DRAINAGE SYSTEM ARE NOT INCLUDING MAIN ACCESS ROAD GRADING. FILE: 5/20/2011 11:58:00 AM

Job Number 14953		18215 72ND AVENUE SOUTH KENT, WA 98032 (425)251-6222 (425)251-6782 FAX	Designed <u>SMF</u> Drawn <u>SMF</u> Checked <u>SMF</u> Approved <u>CSB</u> Date <u>2/28/11</u>	Scale: Horizontal 1"=300' Vertical N/A	For: GREEN CANYON LLC / HIGH MARK RESOURCES LLC / COOPER PASS LLC 206 WEST FIRST STREET CLE ELUM, WA 98922 (509) 674-6828	Title: DOWNSTREAM DRAINAGE SYSTEM EXHIBIT CITY HEIGHTS CLE ELUM, WASHINGTON	No. Date By Ck'd Appr. Revision
Sheet 1 of 2		CIVIL ENGINEERING, LAND PLANNING, SURVEYING, ENVIRONMENTAL SERVICES					

DOWNSTREAM DRAINAGE SYSTEM EXHIBIT



LEGEND	
	DOWNSTREAM DRAINAGE LINE
	PROPOSED ROADWAY
	EXISTING ROAD
	PROPOSED ROAD LOCATION
	PROPOSED BRIDGE
	STRAIN DRAINAGE COLLECTOR
	TEST PIT LOCATION
	EXISTING POWER POLE
	EXISTING TRANSMISSION TOWER
	1" = 30'
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TOTAL ESTIMATED EARTHWORK QUANTITIES FOR THIS SITE DEVELOPMENT AREAS NOT INCLUDING MAIN ACCESS ROAD (SHOWN) FULL-SCALE OR

Job Number 14953	18215 72ND AVENUE SOUTH KENT, WA 98032 (425)251-6222 (425)251-8782 FAX CIVIL ENGINEERING, LAND PLANNING, SURVEYING, ENVIRONMENTAL SERVICES	Designed <u>AMF</u> Drawn <u>AMF</u> Checked <u>AMF</u> Approved <u>AMF</u> Date <u>2/23/11</u>	Scale: Horizontal 1"=300' Vertical N/A	For: GREEN CANYON LLC / HIGH MARK RESOURCES LLC / COOPER PASS LLC 206 WEST FIRST STREET CLE ELUM, WA 98922 (509) 674-6828	Title: DOWNSTREAM DRAINAGE SYSTEM EXHIBIT CITY HEIGHTS CLE ELUM, WASHINGTON	No. Date By Ck. Appr. Revision
Sheet 2 of 2						

Section 5 Core Elements

Compliance with Core Elements 1 through 8, per Section 2.7 of the 2019 SWMMEW, are listed below.

Core Element #1: Preparation of a Stormwater Site Plan:

Road and Storm Plans under separate cover and Storm Drainage Report herein have been prepared for the subject property.

Core Element #2: Construction Stormwater Pollution Prevention Plan (SWPPP):

The project will include temporary measures (silt fence, construction entrance) as well as permanent measures (seeding, landscaping) for control of stormwater during construction to be designed at the final engineering permit phase. See Section 7 for more information.

Core Element #3: Source Control of Pollution:

The site is mostly residential and is, therefore, anticipated to have minimal opportunities for pollution. The community will have an HOA which is encouraged to share educational information to future residents regarding water quality and to promote voluntary use of BMP's.

Core Element #4: Preservation of Natural Drainage Systems:

The site consists of two drainage basins with separate discharge locations divided by an existing onsite stream (Stream C). In the existing condition, runoff from the Crystal Creek 5 basin sheets flows south towards a ditch along 6th Street. Runoff continues east along a ditch prior to outleting to an existing roadside ditch. In the developed condition, Crystal Creek 5 will enter the proposed conveyance system which will be routed to a biofiltration swale and a detention vault (Vault C), prior to outleting into the existing roadside ditch.

In the existing condition, runoff from the Crystal Creek 3 basin sheet flows southeast towards an existing onsite stream (Stream C), which is ultimately tributary to Crystal Creek. In the developed condition, Crystal Creek 3 will enter the proposed conveyance system (includes a biofiltration swale) which will be routed to a detention pond (Pond B7-A), prior to outleting into Stream C.

The proposed project will preserve the natural drainage system. See Section 4 of this report for the downstream analysis.

Core Element #5: Runoff Treatment:

The project proposes more than 5,000 SF of pollution generating hard surface (PGHS), is not a commercial or industrial site, and does not discharge to a wetland or phosphorous sensitive receiving waters. Per Figure 2.3 of the 2019 SWMMEW, basic water quality treatment is required.

Core Element #6: Flow Control:

The project will implement flow control BMPs per Chapter 6 of the 2019 SWMMEW. A detention pond (Pond B7-A) and detention vault (Vault C) are proposed per BMP F6.10 and BMP F6.12 to meet the allowable developed peak flows and not exceed the pre-developed rates for the following storm events: 50% of the 2-year storm event, 25-year storm event, and 100-year storm event (per DA).

Core Element #7: Operation and Maintenance:

An Operation and Maintenance Manual will be provided with the final engineering submittal.



Core Element #8: Local Requirements:

The project has been designed using the guidelines and requirements established in the 2019 Department of Ecology (DOE) Stormwater Management Manual for Eastern Washington (SWMMEW) and the City Heights Annexation and Development Agreement (DA), dated November 8, 2011. The DA contains references to local requirements and vesting.



Section 6 Permanent Stormwater Control Plan

6.1 EXISTING HYDROLOGY

The existing site is undeveloped and mostly forested. There are existing bike trails that are within the premises of Phase 1 site, part of the City Heights development. For modelling purposes, the existing site was modeled as the existing condition in accordance with Section 2.7.7 of the 2019 SWMMEW. There are two basin that generate runoff: the Crystal Creek 3 basin that outlets to an onsite stream (Stream C) prior to entering Crystal Creek and the Crystal Creek 5 basin that outlets to an existing roadside ditch prior to entering Crystal Creek south of the site. Refer to the *Existing Conditions Exhibit* Included in Section 2 of this report for more information. The existing condition areas used to run the drainage model are summarized below. Refer to Appendix for full Hydraflow report.

TRIBUTARY TO CRYSTAL CREEK 3

EXISTING CONDITIONS

Onsite Pervious

Forest (CN=73)	6.43	ac
TOTAL FOREST (SOIL GROUP C)	6.43	ac

Upstream Pervious

Forest (CN=73)	2.17	ac
TOTAL FOREST (SOIL GROUP C)	2.17	ac
TOTAL EXISTING CONDITIONS	8.60	ac

TRIBUTARY TO CRYSTAL CREEK 5

EXISTING CONDITIONS

Pervious

Forest (CN=73)	8.16	ac
Pasture (CN=79)	0.91	ac
TOTAL PERVIOUS (SOIL GROUP C)	9.07	ac

Impervious

Road (Existing Summit View Rd, CN=98)	0.15	ac
TOTAL IMPERVIOUS	0.15	ac
TOTAL EXISTING CONDITIONS	9.22	ac



6.2 DEVELOPED HYDROLOGY

The project proposes 68 lots. Flows for each basin will be collected by the proposed conveyance systems and conveyed to the detention and water quality facilities.

There are two basins analyzed for Phase 1, part of the City Heights development. The developed basins for the Crystal Creek 3 basin and Crystal Creek 5 basin match the existing basins.

For the Crystal Creek 3 basin, runoff will be routed to Pond B7-A before discharging to a location that will mimic existing drainage patterns. Pond B7-A is sized to detain developed runoff in order to maintain the stream protection flow of the existing forested site. The upstream areas will remain undeveloped and runoff will be collected and routed through Pond B7-A as bypass and discharged to the downstream system.

For the Crystal Creek 5 basin, runoff will be routed to Vault C before discharging to a location that will mimic existing drainage patterns. Vault C is sized to detain developed runoff in order to maintain the stream protection flow of the site, which is mostly forested with an existing drive. Upstream areas will remain undeveloped and will be routed around the detention/water quality facilities and, as such are not included in the analysis.

Onsite storm drain infrastructure will collect and convey drainage for the site. Please refer to the Road and Storm Drainage Plans for more information on the proposed storm drain improvements. The areas used to run the drainage model associated with the developed basins conditions are summarized below and on the following pages. Refer to Appendix for full Hydraflow report.

The percent impervious for each type of area is listed in the area tables below. Lot area coverage is based on maximized house and garage footprints. The majority of lots contain 60% impervious coverage or less. Lots that are between 60% and 70% coverage are modeled as 70% impervious. Right-of-way and alley impervious areas are based on the road sections and is increased where there are driveway cuts in the right-of-way. The drainage tract for the pond is assumed 80% impervious based on the area associated with the access road and area below the maximum water surface of the pond. The open space tracts are assumed to have 10% impervious coverage to account for trail areas, bike paths and parking. The impervious coverage for each basin was conservatively rounded up to the nearest 5% for the Hydraflow models.

TRIBUTARY TO CRYSTAL CREEK 3 (Pond B7-A)

DEVELOPED CONDITIONS

Impervious (CN=98) *

Lots (60% impervious: Lots 41-68)	2.31	ac
50' ROW (68% impervious)	1.06	ac
Drainage Tract (80% impervious)	0.56	ac
Open Space Tracts (10% impervious)	0.03	ac
TOTAL IMPERVIOUS	3.96	ac



Pervious (CN=79) *

Lots (40% pervious: Lots 41-68)	1.54	ac
50' ROW (32% pervious)	0.50	ac
Drainage Tract (20% pervious)	0.14	ac
Open Space Tracts (90% pervious)	0.29	ac
TOTAL PERVIOUS (SOIL GROUP C)	2.47	ac

Onsite Upstream Pervious (Bypass)

Forest (CN=73)	2.17	ac
TOTAL FOREST (SOIL GROUP C)	2.17	ac
TOTAL DEVELOPED CONDITIONS	8.60	ac

*Actual impervious is 3.96 ac (approximately 62% of site) and actual pervious is 2.44 ac (approximately 38% of site). Drainage model conservatively assumes 4.18 ac impervious (65% of site, CN=98) and 2.25 ac pervious (35% of site, Pasture CN=79).

TRIBUTARY TO CRYSTAL CREEK 5 (Vault C)**DEVELOPED CONDITIONS**Impervious (CN=98) *

Lots (60% impervious: Lots 1-19, 24-25, 30-40)	1.57	ac
Lots (70% impervious: Lots 20-23, 26-29)	0.29	ac
45' ROW (73% impervious)	0.25	ac
50' ROW (60% impervious)	0.53	ac
Alleys (90% impervious)	0.93	ac
Amenity Area (Outfitter) (35% impervious)	0.42	ac
Open Space/Drainage Tracts (10% impervious)	0.27	ac
TOTAL IMPERVIOUS	4.26	ac

Pervious (CN=79) *

Lots (40% pervious: Lots 1-19, 24-25, 30-40)	1.05	ac
Lots (30% pervious: Lots 20-23, 26-29)	0.13	ac
45' ROW (27% pervious)	0.09	ac
50' ROW (40% pervious)	0.35	ac
Alleys (10% pervious)	0.10	ac
Outfitter (65% pervious)	0.78	ac
Open Space/Drainage Tracts (90% pervious) **	2.46	ac
TOTAL PERVIOUS (SOIL GROUP C)	4.96	ac
TOTAL DEVELOPED CONDITIONS	9.22	ac



*Actual impervious is 4.26 ac (approximately 46% of site) and actual pervious is 4.96 ac (approximately 54% of site). Drainage model conservatively assumes 4.61 ac impervious (50% of site, CN=98) and 4.61 ac pervious (50% of site, 50% Pasture CN=79/50% Forest CN=73).

**Pervious areas for this basin are modeled as 50% Pasture CN=79 and 50% Forest CN=73 in anticipation that forested areas will remain where feasible to preserve the natural feel of the development.



6.3 DESIGN PARAMETERS

The flow control and water quality elements are designed per 2019 SWMMWEW.

- Rain Distribution: SCS Type 1A
- 24-hrs Precipitations:

Storm Event Return Period	24-hr Depth (inches)
6-month (WQ)	1.40
2-year	2.00
10-year	3.25
25-year	3.50
100-year	4.75

Per Section 4.3.9 of the 2019 SWMMWEW, including rain-on-snow and snowmelt design, is optional guidance for detention and water quality design. However, rain-on-snow and snowmelt design requirements are applied for this project per City Heights Annexation and Development Agreement, dated November 8, 2011. The 2019 SWMMWEW does not contain snowmelt adjustment factors for Cle Elum. Snowmelt adjustment factors for another relatively close, similar location were used to determine the water equivalent precipitation adjustment for Cle Elum.

Cle Elum:

Avg Annual Precipitation (2019 SWMMWEW Figure 4.1): 25 inches

Avg Daily Snow Depth (inches 2019 SWMMWEW Table 4.9): to determine

Wenatchee:

Avg Annual Precipitation (2019 SWMMWEW Figure 4.1): 10 inches

Avg Daily Snow Depth (inches 2019 SWMMWEW Table 4.9) 2.67 inches

$$2.67'' * 25'' / 10'' = 6.675''$$

$$6.675'' * 20\% \text{ moisture content} = 1.34''$$

(1.34'' to be added to each design storm, not including water quality storm)

- 24-hr precipitation depths with applied snowmelt adjustment factor are as below:

Storm Event Return Period Including snowmelt design factor	24-hr Depth (inches)
6-month (WQ)	1.40
2-year	3.34
10-year	4.59
25-year	4.84
100-year	6.09



6.4 FLOW CONTROL

The proposed Phase 1, part of City Heights development, will implement Basic Water Quality Treatment and match 50% of the 2-year peak flow and the full 10 year peak flow, 25-year peak flow and 100-year peak flow as described in the 2019 SWMMEW and City Heights Annexation and Development Agreement, dated November 8, 2011

The existing and developed site conditions were modeled using the Hydraflow hydrology model. Vault C is proposed for the Clear Creek 5 basin and Pond B7-A is proposed for the Clear Creek 3 basin so that the developed discharge peak flows match the pre-developed peak flows for 50% of the 2-year peak flow up to the full 25-year peak flow and full 100-year peak flow (Core Element #6).

Approximately 0.21 acres of Summit View Road right-of-way will be collected via thickened edge and catch basin and routed to a dispersion trench for full dispersion. Refer to sizing at the end of this section.



POND/VAULT PERFORMANCE

Pond B7A:

The pond is sized to detain developed runoff in order to maintain the stream protection flow of the existing site conditions. The undeveloped areas runoff will be routed through the project site to the pond and eventually will be bypassed. Please see table below for discharge calculations to include the bypassing of the undeveloped areas runoff.

	A	B	C	D	E	F	G
Storm Event	Existing ¹ Peak Flow (cfs)	Existing ² Peak Flow (cfs)	Existing Match Flow (cfs)*	Dev ³ Peak Flow (cfs)	Dev ⁴ Peak Flow (cfs)	Dev ⁵ Peak Flow (cfs) **	100-year Elevation
2-year	1.25	0.42	1.05	3.98	4.40	1.03	
10-year	2.73	0.92	3.65	6.03	6.95	2.92	
25-year	3.06	1.03	4.09	6.44	7.47	3.47	
100-year	4.79	1.62	6.41	8.48	10.1	5.84	106.22

1: Existing: onsite existing area

2: Existing: onsite existing area + onsite upstream (bypass) area

3: Dev: unmitigated onsite developed area

4: Dev: unmitigated onsite developed area + onsite upstream (bypass) area (column B + column D)

5: Dev: mitigated onsite developed area + onsite upstream (bypass) area

* Existing Match Flow (includes onsite upstream bypass area) = 50% onsite undeveloped peak flow + onsite upstream (bypass) area, these are the allowable peak flows used for designing the detention facility

** Developed peak flows for mitigated onsite developed area + onsite upstream (bypass) area are obtained from Hydraflow

The required volume for the proposed pond is 25,912 cubic feet. The design water surface elevation (100-Year water surface elevation) corresponds to a depth of 6.22 feet which is determined based on the 100-year mitigated outflow and the Hydraflow discharge peak stage. See full Hydraflow output in Appendix.

The proposed water surface elevation will be 6.5'. The provided pond volume will exceed the minimum required. The proposed 6.5' deep pond will provide 28,289 cubic feet of live storage. The proposed pond is therefore adequately sized to accommodate the required flow control.

<p>Pond B7-A - Live Storage Volume Required = 25,912 cubic feet Provided = 28,289 cubic feet</p>



Vault C:

The Vault is sized to detain developed runoff in order to maintain the stream protection flow of the existing pre-developed site conditions. The onsite areas upstream, 3.89 ac, will remain undeveloped and undetained. This area will be collected via shallow swale and will bypass the vault/water quality facilities and, as such, is not included in the analysis. Please see table below for discharge calculations to include the bypassing of the undeveloped areas runoff.

Storm Event	Existing ¹ Peak Flow (cfs)	Existing Match Flow ² (cfs)	Dev ³ Peak Flow (cfs)	Dev ⁴ Peak Flow (cfs)*	100-year Elevation
2-year	1.98	0.99	4.79	0.98	
10-year	4.15	4.15	7.69	2.55	
25-year	4.62	4.62	8.28	3.05	
100-year	7.16	7.16	11.25	7.10	108.50

1: Existing: onsite existing

2: Existing: onsite allowable peak flows

3: Dev: unmitigated onsite developed area

4: Developed: mitigated onsite developed area

**Developed peak flows for mitigated onsite developed areas are obtained from Hydraflow*

The required volume for the proposed vault is 33,136 cubic feet. The design water surface elevation (100-Year water surface elevation) corresponds to a depth of 8.5 feet which is determined based on the 100-year mitigated outflow and the Hydraflow discharge peak stage. See full Hydraflow output on Appendix.

The provided pond volume will exceed the minimum required. The proposed 8.5'x96'x42' vault will provide 34,272 cubic feet of live storage. The proposed pond is therefore adequately sized to accommodate the required flow control.

<p>Vault C - Live Storage Volume Required = 33,136 cubic feet Provided = 34,272 cubic feet</p>



FLOW DISPERSION TRENCH DESIGN

Approximately 0.21 acres of Summit View Road right-of-way will be collected via thickened edge and catch basin and routed to a dispersion trench for full dispersion.

Per BMP F6.42 Full Dispersion in the 2019 SWMMEW, discharge points with between 0.2 and 0.5 cfs discharge for the 100-year storm shall use only dispersion trenches to disperse flows. Dispersion trenches shall be designed to accept surface flows (free discharge) from a pipe, culvert, or ditch end, shall be aligned perpendicular to the flow path, and shall be minimum 2' by 2' in section, 50' in length, filled with 0.75- to 1.5-in washed rock, and provided with a level notched grade board. The 50' dispersion trench can treat up to 0.5 cfs, which equates to 10' length of trench for each 0.1 cfs. The 100-year storm based on the areas tributary to the dispersion trench (below) is 0.298 cfs based on Hydraflow output and, therefore, 30 ft of trench is required. A 30' dispersion trench is proposed for full dispersion.

TRIBUTARY TO DISPERSION TRENCH

DEVELOPED CONDITIONS

Impervious (CN=98) *

45' ROW (73% impervious)	0.15	ac
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TOTAL IMPERVIOUS	0.15	ac
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Pervious (CN=79) *

45' ROW (27% pervious)	0.06	ac
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TOTAL PERVIOUS (SOIL GROUP C)	0.06	ac
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TOTAL DEVELOPED CONDITIONS	0.21	ac
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6.5 WATER QUALITY

The project proposes more than 5,000 SF of pollution generating hard surface (PGHS), is not a commercial or industrial site, and does not discharge to a wetland or phosphorous sensitive receiving waters. Per Figure 2.3 of the 2019 SWMMEW, the project will comply with basic water quality requirements using a biofiltration swale upstream of detention pond (B7-A) and Vault (C). The project is not required to provide oil control BMPs, metals treatment BMPs, or phosphorus treatment BMPs.

Per email coordination with the City of Cle Elum on 6/1/2020, the water quality precipitation depth assumptions have been deemed acceptable. The 2-year, 24-hour precipitation depth (2.00 in) is multiplied by the C_{wqs} coefficient from Table 4.5 in the 2019 SWMMEW (0.70 for Climate Region 1) to determine the water quality precipitation depth (1.4 in). The water quality design flow rate for the 6-month, 24-hour storm is then determined with Hydraflow analysis model for each basin.

It is anticipated that basic water quality treatment Pond B7-A and Vault C will be satisfied using the BMP T5.40 design requirements per Section 5.5.5 of the 2019 SWMMEW. The biofiltration swale will also act as a conveyance element with capacity for the 25-year and 100-year storms if it is located online. An online trapezoidal shape with 3:1 side slope has been proposed. Refer to water quality flow rates and sizing included on the following pages.

Per Section 5.5.5 of the 2019 SWMMEW, Manning's Equation (Equation 5.3) is used to estimate the bottom width of the biofiltration swale. Manning's Equation for English units is as follows:

$$Q = (1.486 * A * R^{0.667} * S^{0.5}) / n$$

where:

Q = flow (cfs)

A = cross-sectional area of flow (square feet [sf])

R = hydraulic radius of flow cross section (feet [ft])

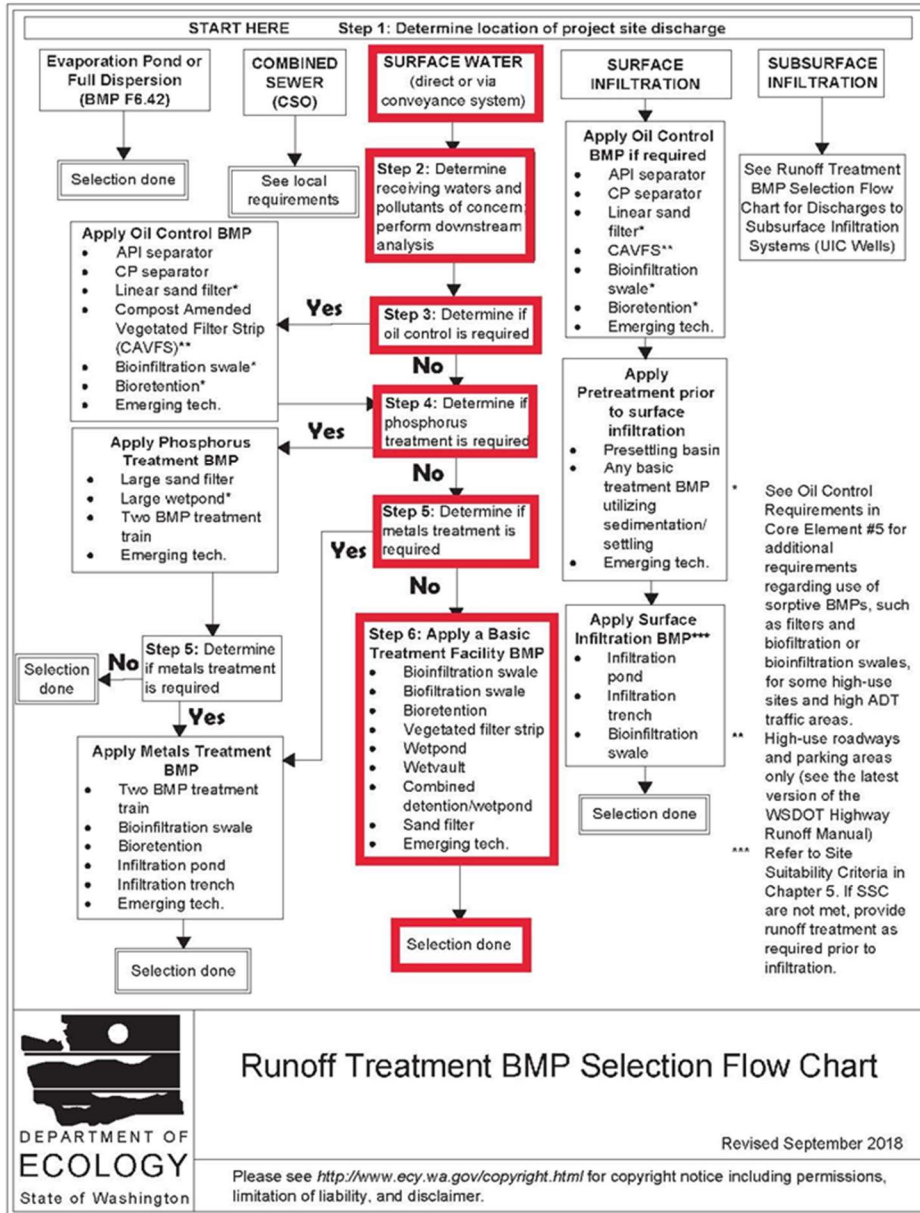
S = longitudinal slope of biofiltration swale (feet per foot [ft/ft])

n = Manning's roughness coefficient.

n = 0.20 for a biofiltration swale with less dense vegetation such as meadow or pasture



Figure 5.1: Runoff Treatment BMP Selection Flow Chart



POND B7-A

BMP	FLOW RATE FOR 6-MONTH STORM EVENT (CFS) ¹	SWALE BOTTOM WIDTH (FT)	REQUIRED SWALE LENGTH (FT) ²	PROVIDED SWALE LENGTH (%) ³	SLOPE (%) ⁴	FLOW DEPTH (FT)	VELOCITY AT WQ DESIGN FLOW RATE, V (FT/SEC)	VELOCITY AT 100-YR FLOW RATE, V (FT/SEC) ⁵
Pond B7-A Swale, 1.5%	0.979	3	91.2	682	1.5	0.48	0.456 < 1	0.861 < 2
Pond B7-A Swale, 5%	0.979	3	139	682	5	0.35	0.695 < 1	1.344 < 2

1. The flow rate is conservatively taken to be the full flow rate tributary to Pond B7-A (including upstream). There is a high point in the road, which will divide the biofiltration swale, and therefore the amount of flow to each swale will be less.
2. Required length is determined based on velocity associated with the water quality design flow rate.
3. The provided length is the full length of swale shown on the plans minus an assumed 20' of driveway width per lot.
4. The slope of the swale varies based on road grade. Minimum and maximum slopes have been provided to show variation in flow depths, velocities, and required length of swale.
5. The maximum velocity is checked to ensure flows do not cause erosion. Velocity not to exceed 2 ft/sec per the 2019 SWMMEW.

VAULT C

BMP	FLOW RATE FOR 6-MONTH STORM EVENT (CFS) ¹	SWALE BOTTOM WIDTH (FT)	REQUIRED SWALE LENGTH (FT) ²	PROVIDED SWALE LENGTH (%)	SLOPE (%)	FLOW DEPTH (FT)	VELOCITY AT WQ DESIGN FLOW RATE, V (FT/SEC)	VELOCITY AT 100-YR FLOW RATE, V (FT/SEC) ³
Vault B7-A Swale	0.836	3	96.4	100	2	0.41	0.482 < 1	0.985 < 2

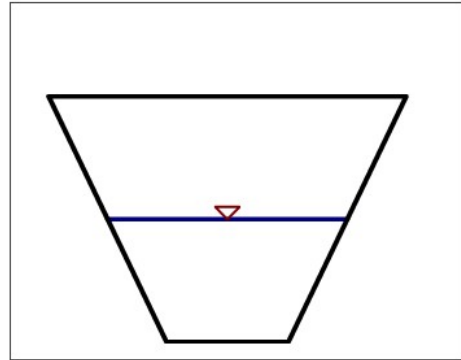
1. The flow rate for the sizing the biofiltration swale upstream of Vault C is conservatively taken to be the full flow rate tributary to Vault C (includes non-PGHS). There will be a portion of area tributary to the vault (lots 1-8) that cannot physically be routed to this swale. Minimal PGHS is anticipated on lots 1-8 (driveway areas, ~3200sf). Based on the existing grades in 6th street, a portion of existing road (not developed/required for treatment) will drain to proposed catch basins that are routed to the biofiltrations swale. Water quality will be provided for this non-target area to offset the PGHS on lots 1-8 that will tie directly into Vault C without water quality treatment.
2. Required length is determined based on velocity associated with the water quality design flow rate.
3. The maximum velocity is checked to ensure flows do not cause erosion. Velocity not to exceed 2 ft/sec per the 2019 SWMMEW.



Crystal Creek 3 (Pond B7-A):

1.5% slope scenario

	Input	Output
Q (cfs)	0.00	0.98
n	0.200	0.200
B (ft)	3.00	3.00 Trap.
LSSlope (X:1)	3.00	3.00
RSSlope (X:1)	3.00	3.00
y (ft)	0.48	0.48
S (ft/ft)	0.015	0.015

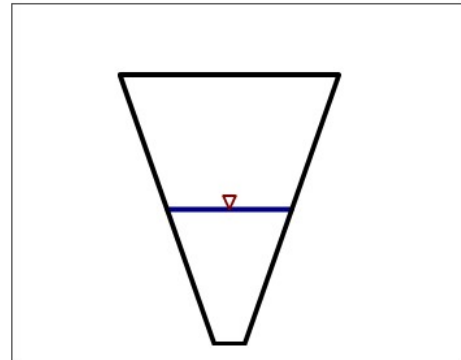


A (sf)	2.147	V (ft/s)	0.456
Pw (ft)	6.053		
R (ft)	0.355		

Job: City Heights Phase 1
By:

Description: Pond B7-A - WQ flow, 1.5% slope
Date: 6/16/2020

	Input	Output
Q (cfs)	0.00	10.10
n	0.200	0.200
B (ft)	3.00	3.00 Trap.
LSSlope (X:1)	3.00	3.00
RSSlope (X:1)	3.00	3.00
y (ft)	1.54	1.54
S (ft/ft)	0.015	0.015



A (sf)	11.730	V (ft/s)	0.861
Pw (ft)	12.737		
R (ft)	0.921		

Job: City Heights Phase 1
By:

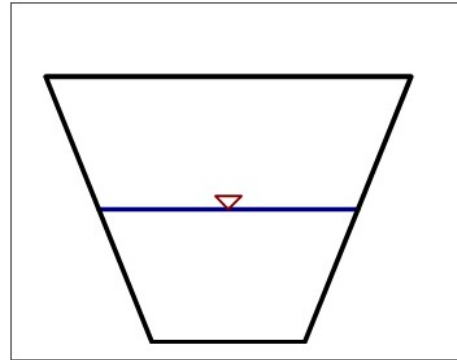
Description: Pond B7-A - 100-yr flow, 1.5% slope
Date: 6/16/2020

The flow depth for flow during the 100-year 24-hrs storm is 1.54' which is slightly higher than the total depth (1.50'). As mentioned, the flow rate is conservatively taken to be the full flow rate tributary to Pond B7-A (including upstream). There is a high point in the road, which will divide the biofiltration swale, and therefore the amount of flow to each swale will be less. Also, the maximum velocity for the total depth of channel is less than 2 ft/s and does not cause erosion.



5% slope scenario

	Input	Output
Q (cfs)	0.00	0.98
n	0.200	0.200
B (ft)	3.00	3.00 Trap.
LSSlope (X:1)	3.00	3.00
RSSlope (X:1)	3.00	3.00
y (ft)	0.35	0.35
S (ft/ft)	0.050	0.050

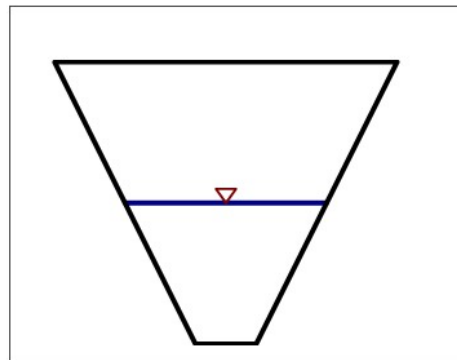


A (sf)	1.408	V (ft/s)	0.695
Pw (ft)	5.202		
R (ft)	0.271		

Job: City Heights Phase 1
By:

Description: Pond B7-A - WQ flow, 5% slope
Date: 6/16/2020

	Input	Output
Q (cfs)	0.00	10.10
n	0.200	0.200
B (ft)	3.00	3.00 Trap.
LSSlope (X:1)	3.00	3.00
RSSlope (X:1)	3.00	3.00
y (ft)	1.16	1.16
S (ft/ft)	0.050	0.050



A (sf)	7.519	V (ft/s)	1.344
Pw (ft)	10.338		
R (ft)	0.727		

Job: City Heights Phase 1
By:

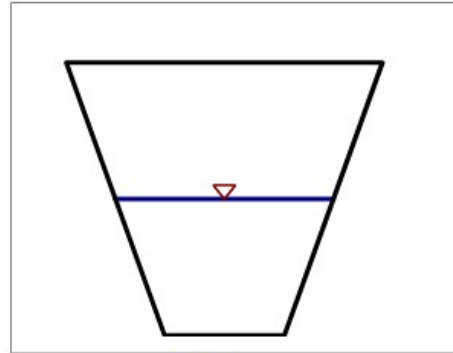
Description: Pond B7-A - 100-yr flow, 5% slope
Date: 6/16/2020

The flow depth for flow during the 100-year, 24-hrs storm is 1.16' which is lower than the total depth (1.50'). Also, the maximum velocity for the total depth of channel is less than 2 ft/s and does not cause erosion.



Crystal Creek 5 (Vault C):

	Input	Output
Q (cfs)	0.00	0.84
n	0.200	0.200
B (ft)	3.00	3.00 Trap.
LSSlope (X:1)	3.00	3.00
RSSlope (X:1)	3.00	3.00
y (ft)	0.41	0.41
S (ft/ft)	0.020	0.020

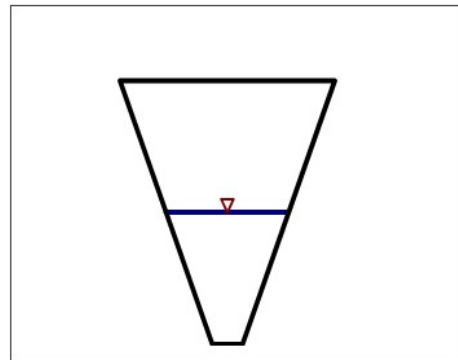


A (sf)	1.736	V (ft/s)	0.482
Pw (ft)	5.595		
R (ft)	0.310		

Job: City Heights Phase 1
By:

Description: Vault C - WQ flow
Date: 6/16/2020

	Input	Output
Q (cfs)	0.00	11.25
n	0.200	0.200
B (ft)	3.00	3.00 Trap.
LSSlope (X:1)	3.00	3.00
RSSlope (X:1)	3.00	3.00
y (ft)	1.51	1.51
S (ft/ft)	0.020	0.020



A (sf)	11.419	V (ft/s)	0.985
Pw (ft)	12.575		
R (ft)	0.908		

Job: City Heights Phase 1
By:

Description: Vault C - 100-yr flow
Date: 6/16/2020

The flow depth for flow during the 100-year, 24-hrs storm is 1.51' which is lower than the total depth (2.00'). Also, the maximum velocity for the total depth of channel is less than 2 ft/s and does not cause erosion.



6.6 LID BMP IMPLEMENTATION

LID BMPs will be implemented for the project to the maximum extent feasible per the 2019 SWMMEW requirements. The feasibility and planned implementation of the applicable BMPs will be discussed at final engineering.



6.7 CONVEYANCE SYSTEM DESIGN

Per the City Heights Annexation and Development Agreement, dated November 8, 2011 the storm drain conveyance system will be designed to convey the 100-year storm. The precipitation rate for the 100-year, 24-hour storm event is 6.09 inches per hour.

The conveyance system will be designed at final engineering.



Section 7 SWPPP

A SWPPP will be submitted under a separate cover with the final engineering submittal.



Section 8 Special Reports and Studies

Refer to the *Geotechnical Engineering Report and Geologic Hazard Assessment* prepared by Terra Associates, Inc. dated June 9, 2020, *Wetlands and Wildlife Habitat Report* prepared by Sewall Wetland Consulting, Inc. dated October 26, 2009, and *Impacts Analysis* prepared by Sewall Wetland Consulting, Inc. dated June 16, 2020 included under separate cover.



Section 9 Other Permits

At this time, no other permits related to the City Heights project are assumed to be required.



Section 10 Operation and Maintenance

An operations and maintenance manual will be provided with the final engineering submittal.



Appendix

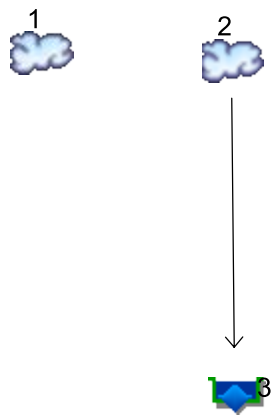


Crystal Creek 5 Detention Vault C Output



Watershed Model Schematic

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Tuesday, 06 / 16 / 2020

Return Period (Yrs)	Intensity-Duration-Frequency Equation Coefficients (FHA)			
	B	D	E	(N/A)
1	0.0000	0.0000	0.0000	-----
2	0.0000	0.0000	0.0000	-----
3	0.0000	0.0000	0.0000	-----
5	0.0000	0.0000	0.0000	-----
10	0.0000	0.0000	0.0000	-----
25	0.0000	0.0000	0.0000	-----
50	0.0000	0.0000	0.0000	-----
100	0.0000	0.0000	0.0000	-----

File name: SampleFHA.idf

$$\text{Intensity} = B / (T_c + D)^E$$

Return Period (Yrs)	Intensity Values (in/hr)												
	5 min	10	15	20	25	30	35	40	45	50	55	60	
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
25	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

T_c = time in minutes. Values may exceed 60.

*1-yr column is the 6 mo, 24 hr precip

Precip. file name: E:\Projects\19349\Engineering\Hydraflow\Phase 1\Vault\precip.pcp

Storm Distribution	Rainfall Precipitation Table (in)							
	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
SCS 24-hour	1.40	3.34	0.00	3.30	4.59	4.84	6.80	6.09
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-1st	0.00	0.00	0.00	2.75	0.00	0.00	6.50	0.00
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Custom	0.00	0.00	0.00	2.80	0.00	0.00	6.00	0.00

TR55 Tc Worksheet

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No. 1

PRE (Crystal Creek 5)

<u>Description</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>Totals</u>
Sheet Flow				
Manning's n-value	= 0.350	0.011	0.011	
Flow length (ft)	= 200.0	0.0	0.0	
Two-year 24-hr precip. (in)	= 3.34	3.34	0.00	
Land slope (%)	= 18.00	0.00	0.00	
Travel Time (min)	= 13.66	+ 0.00	+ 0.00	= 13.66
Shallow Concentrated Flow				
Flow length (ft)	= 254.00	0.00	0.00	
Watercourse slope (%)	= 6.00	0.00	0.00	
Surface description	= Unpaved	Paved	Paved	
Average velocity (ft/s)	=3.95	0.00	0.00	
Travel Time (min)	= 1.07	+ 0.00	+ 0.00	= 1.07
Channel Flow				
X sectional flow area (sqft)	= 0.00	0.00	0.00	
Wetted perimeter (ft)	= 0.00	0.00	0.00	
Channel slope (%)	= 0.00	0.00	0.00	
Manning's n-value	= 0.015	0.015	0.015	
Velocity (ft/s)	=0.00	0.00	0.00	
Flow length (ft)	({0})0.0	0.0	0.0	
Travel Time (min)	= 0.00	+ 0.00	+ 0.00	= 0.00
Total Travel Time, Tc				14.70 min

Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Tuesday, 06 / 16 / 2020

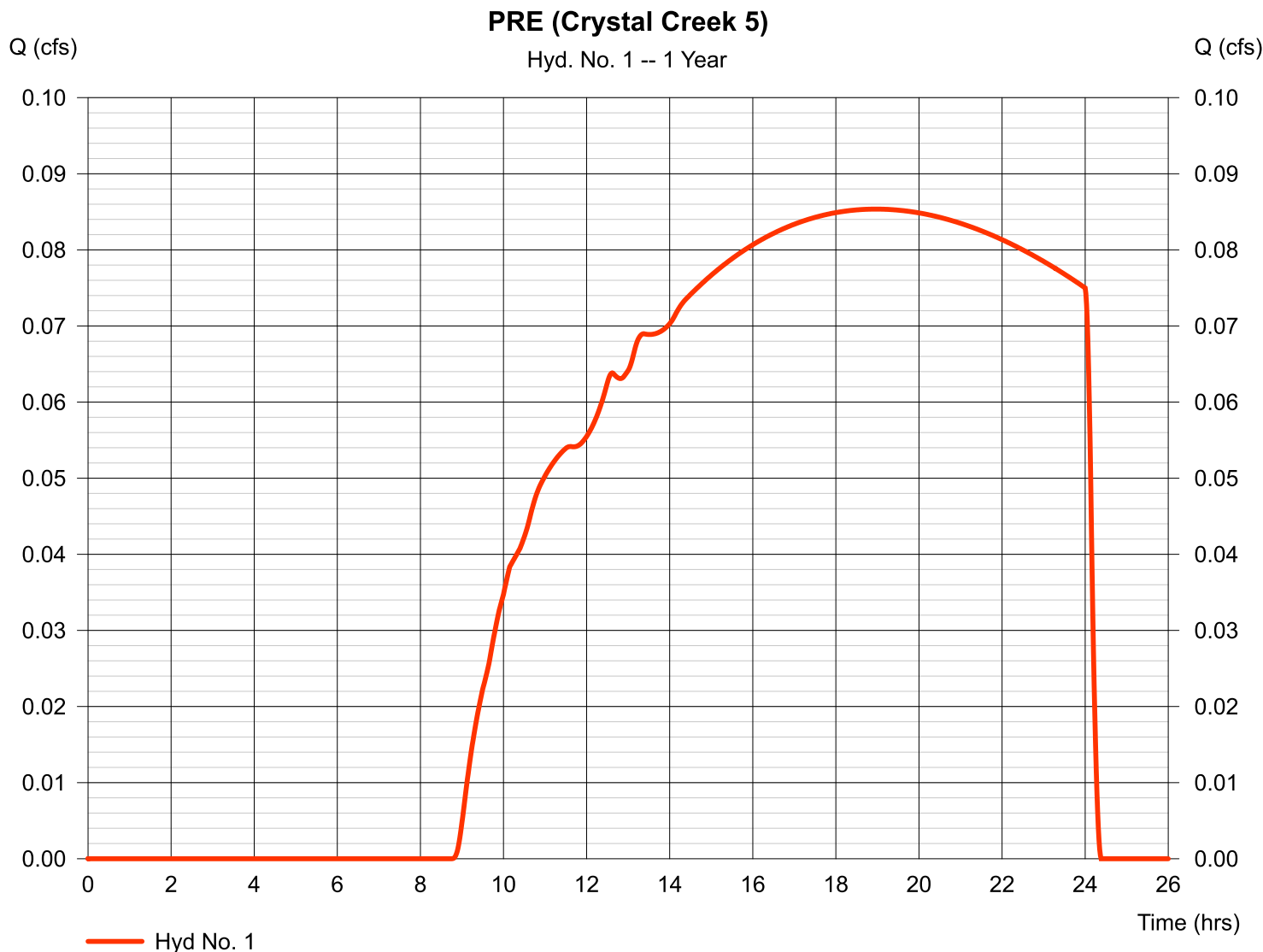
Hyd. No. 1

*1-yr is model for the 6 mo, 24 hr precip

PRE (Crystal Creek 5)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.085 cfs
Storm frequency	= 1 yrs	Time to peak	= 18.97 hrs
Time interval	= 1 min	Hyd. volume	= 3,865 cuft
Drainage area	= 9.220 ac	Curve number	= 74*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 14.70 min
Total precip.	= 1.40 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(8.160 x 73) + (0.910 x 79) + (0.150 x 98)] / 9.220



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

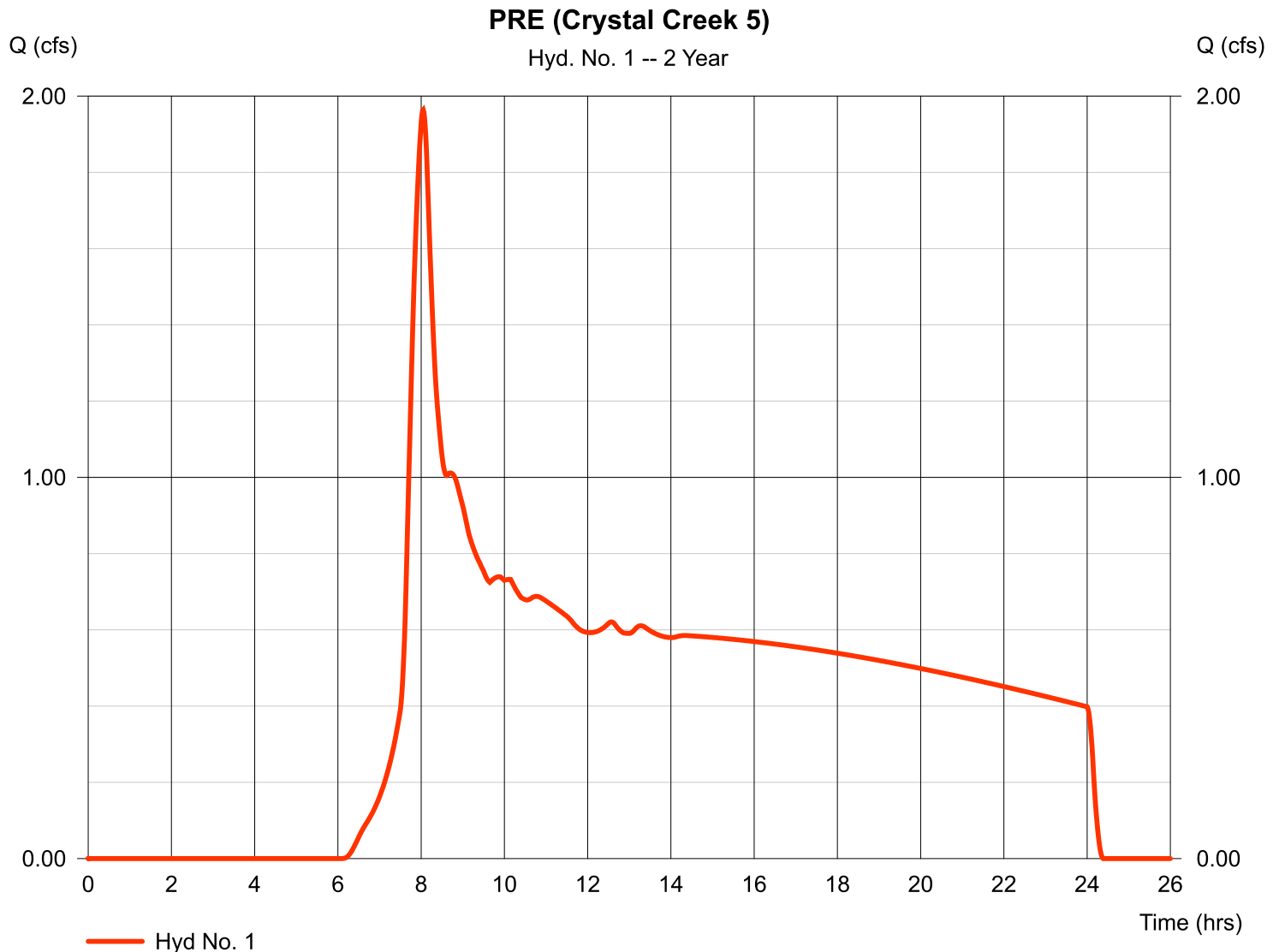
Tuesday, 06 / 16 / 2020

Hyd. No. 1

PRE (Crystal Creek 5)

Hydrograph type	= SCS Runoff	Peak discharge	= 1.964 cfs
Storm frequency	= 2 yrs	Time to peak	= 8.05 hrs
Time interval	= 1 min	Hyd. volume	= 37,846 cuft
Drainage area	= 9.220 ac	Curve number	= 74*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 14.70 min
Total precip.	= 3.34 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(8.160 x 73) + (0.910 x 79) + (0.150 x 98)] / 9.220



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

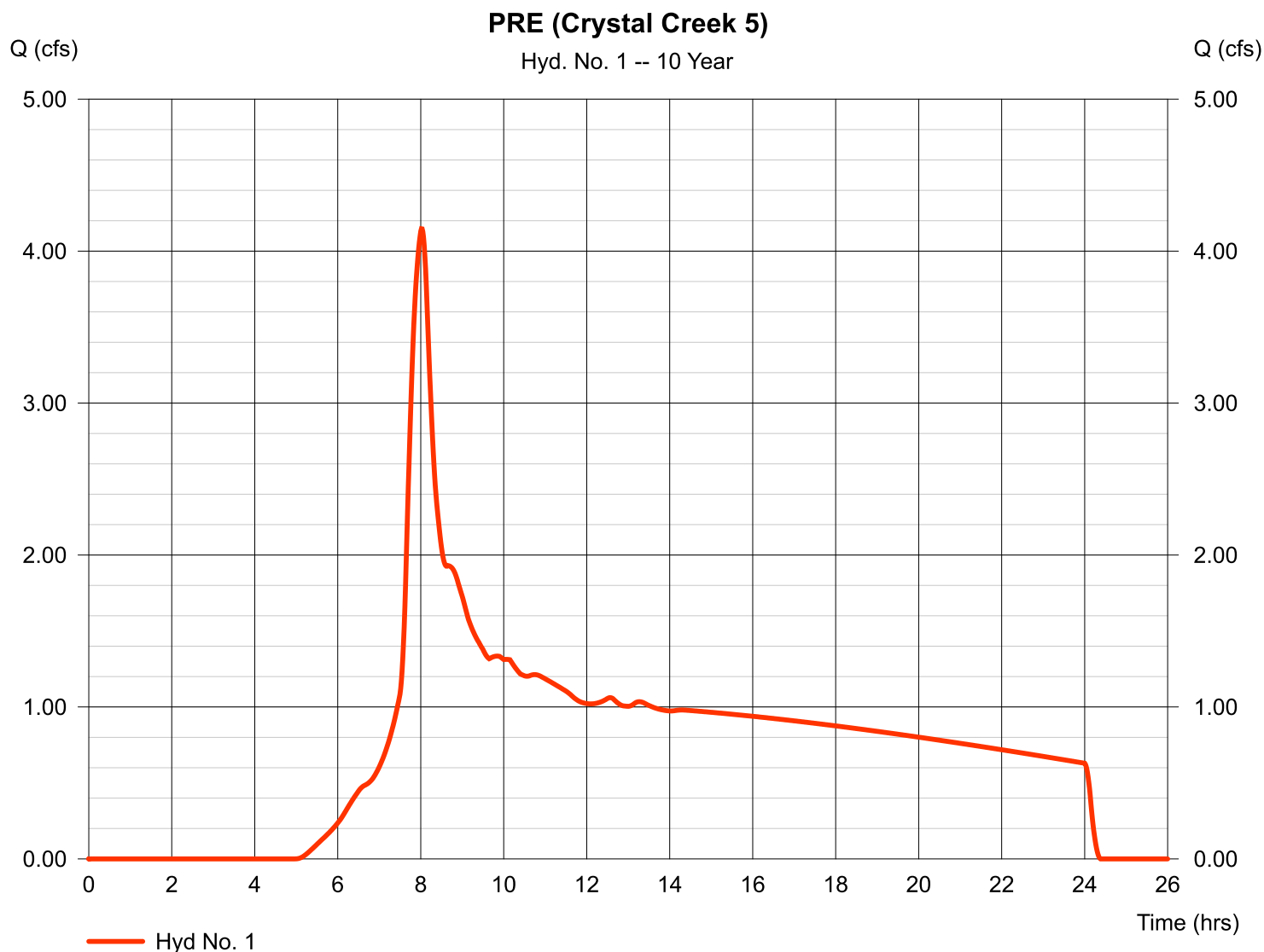
Tuesday, 06 / 16 / 2020

Hyd. No. 1

PRE (Crystal Creek 5)

Hydrograph type	= SCS Runoff	Peak discharge	= 4.147 cfs
Storm frequency	= 10 yrs	Time to peak	= 8.02 hrs
Time interval	= 1 min	Hyd. volume	= 68,337 cuft
Drainage area	= 9.220 ac	Curve number	= 74*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 14.70 min
Total precip.	= 4.59 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(8.160 x 73) + (0.910 x 79) + (0.150 x 98)] / 9.220



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

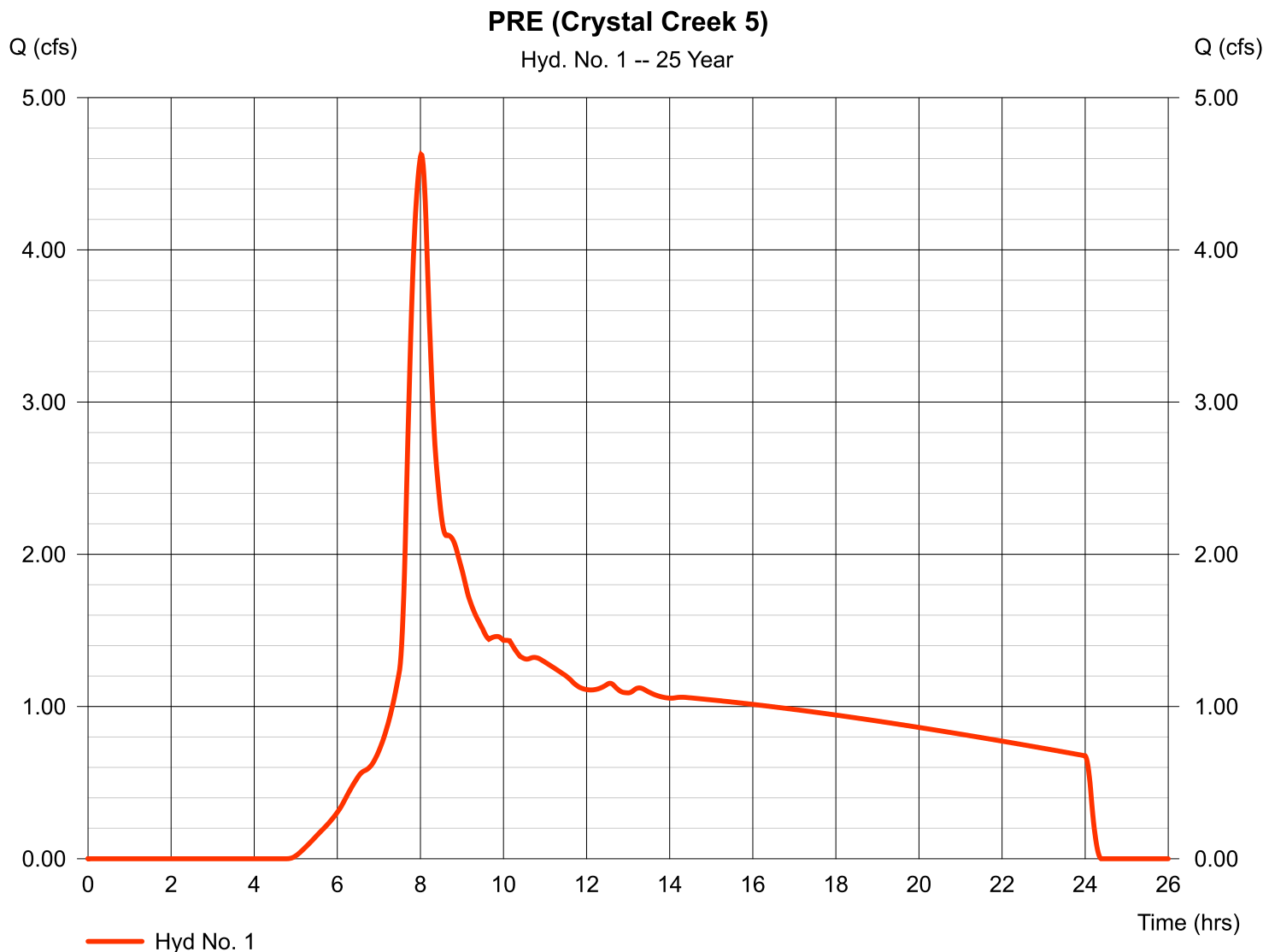
Tuesday, 06 / 16 / 2020

Hyd. No. 1

PRE (Crystal Creek 5)

Hydrograph type	= SCS Runoff	Peak discharge	= 4.626 cfs
Storm frequency	= 25 yrs	Time to peak	= 8.02 hrs
Time interval	= 1 min	Hyd. volume	= 74,880 cuft
Drainage area	= 9.220 ac	Curve number	= 74*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 14.70 min
Total precip.	= 4.84 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(8.160 x 73) + (0.910 x 79) + (0.150 x 98)] / 9.220



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

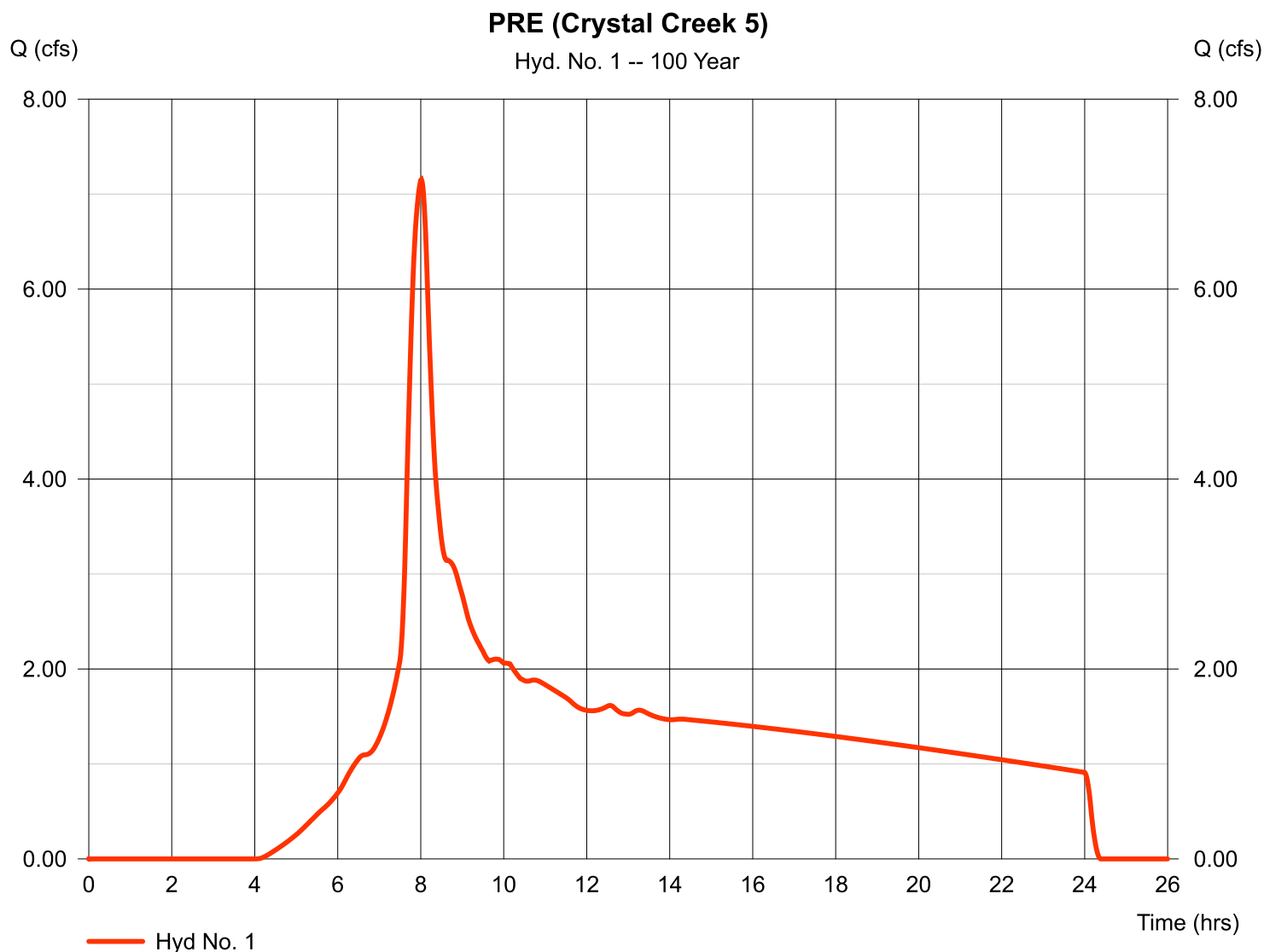
Tuesday, 06 / 16 / 2020

Hyd. No. 1

PRE (Crystal Creek 5)

Hydrograph type	= SCS Runoff	Peak discharge	= 7.155 cfs
Storm frequency	= 100 yrs	Time to peak	= 8.02 hrs
Time interval	= 1 min	Hyd. volume	= 109,131 cuft
Drainage area	= 9.220 ac	Curve number	= 74*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 14.70 min
Total precip.	= 6.09 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(8.160 x 73) + (0.910 x 79) + (0.150 x 98)] / 9.220



TR55 Tc Worksheet

Hyd. No. 2

Onsite PRE (Crystal Creek 3)

<u>Description</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>Totals</u>
Sheet Flow				
Manning's n-value	= 0.350	0.011	0.011	
Flow length (ft)	= 200.0	0.0	0.0	
Two-year 24-hr precip. (in)	= 3.34	0.00	0.00	
Land slope (%)	= 18.00	0.00	0.00	
Travel Time (min)	= 13.66	+ 0.00	+ 0.00	= 13.66
Shallow Concentrated Flow				
Flow length (ft)	= 110.00	0.00	0.00	
Watercourse slope (%)	= 18.00	0.00	0.00	
Surface description	= Unpaved	Paved	Paved	
Average velocity (ft/s)	=6.85	0.00	0.00	
Travel Time (min)	= 0.27	+ 0.00	+ 0.00	= 0.27
Channel Flow				
X sectional flow area (sqft)	= 0.00	0.00	0.00	
Wetted perimeter (ft)	= 0.00	0.00	0.00	
Channel slope (%)	= 0.00	0.00	0.00	
Manning's n-value	= 0.015	0.015	0.015	
Velocity (ft/s)	=0.00	0.00	0.00	
Flow length (ft)	({0})0.0	0.0	0.0	
Travel Time (min)	= 0.00	+ 0.00	+ 0.00	= 0.00
Total Travel Time, Tc				13.90 min

Hydrograph Report

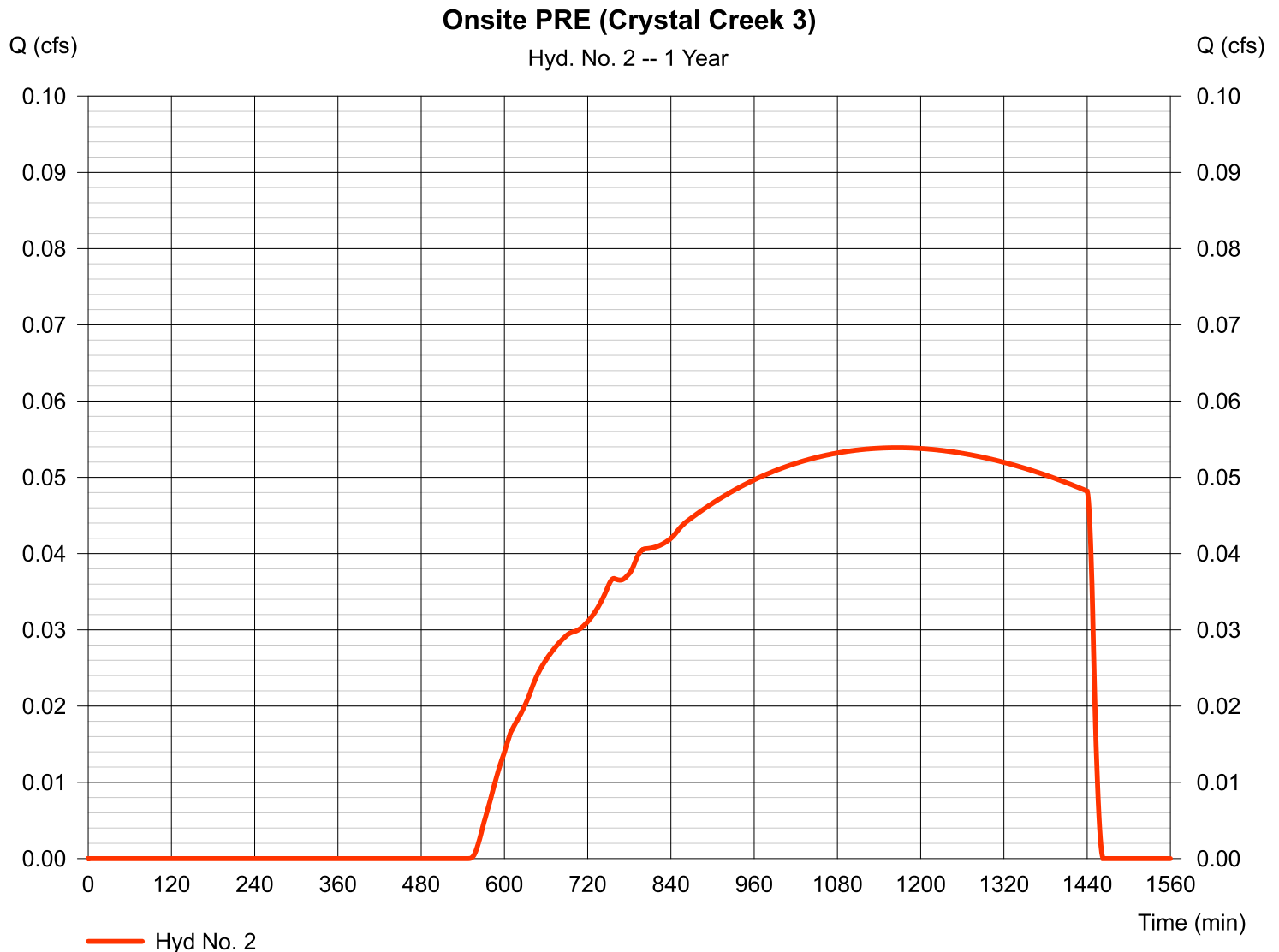
Hyd. No. 2

*1-yr is model for the 6 mo, 24 hr precip

Onsite PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.054 cfs
Storm frequency	= 1 yrs	Time to peak	= 1167 min
Time interval	= 1 min	Hyd. volume	= 2,334 cuft
Drainage area	= 6.430 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 13.90 min
Total precip.	= 1.40 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(6.430 x 73)] / 6.430



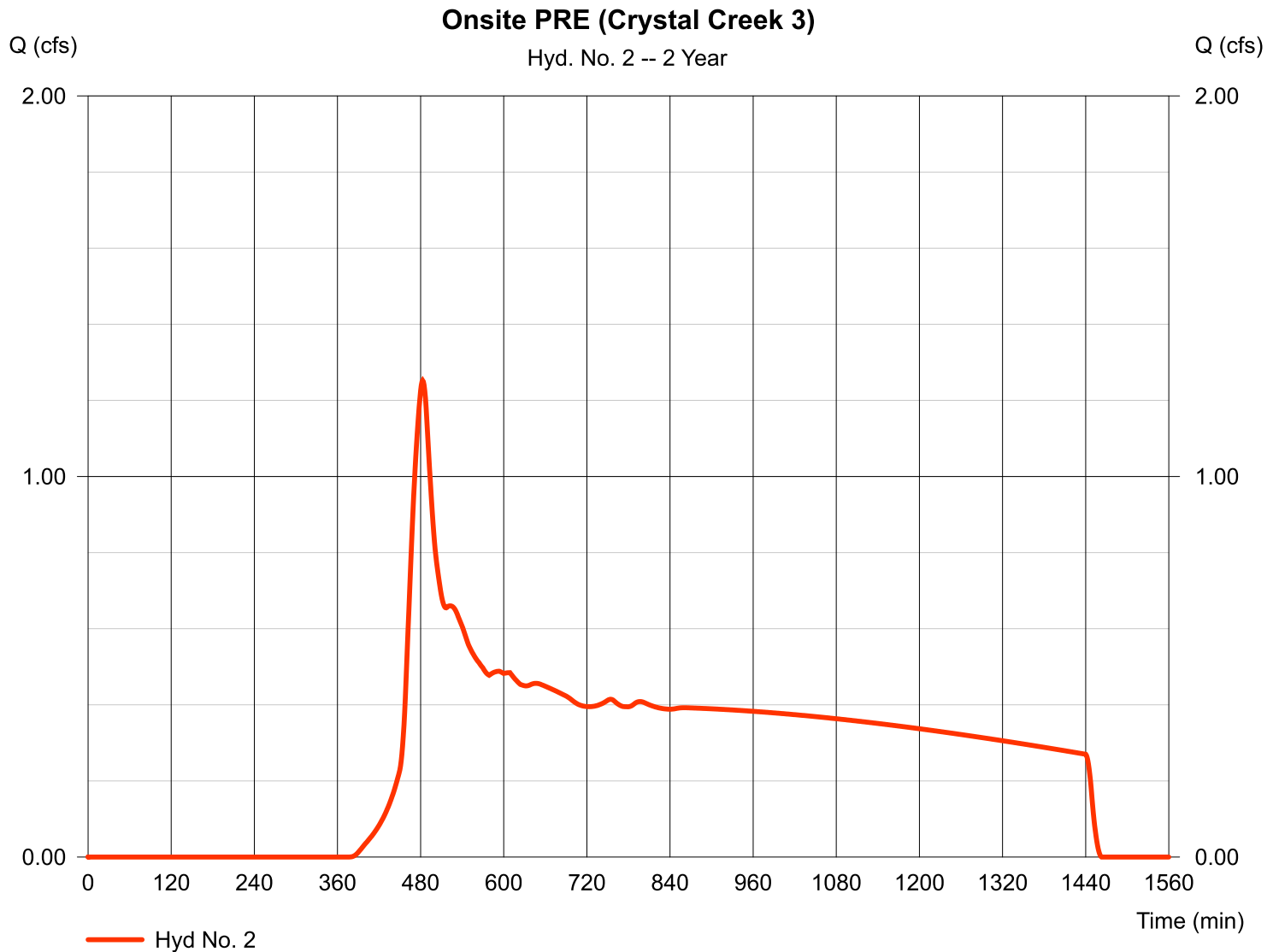
Hydrograph Report

Hyd. No. 2

Onsite PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 1.252 cfs
Storm frequency	= 2 yrs	Time to peak	= 483 min
Time interval	= 1 min	Hyd. volume	= 25,055 cuft
Drainage area	= 6.430 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 13.90 min
Total precip.	= 3.34 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(6.430 x 73)] / 6.430



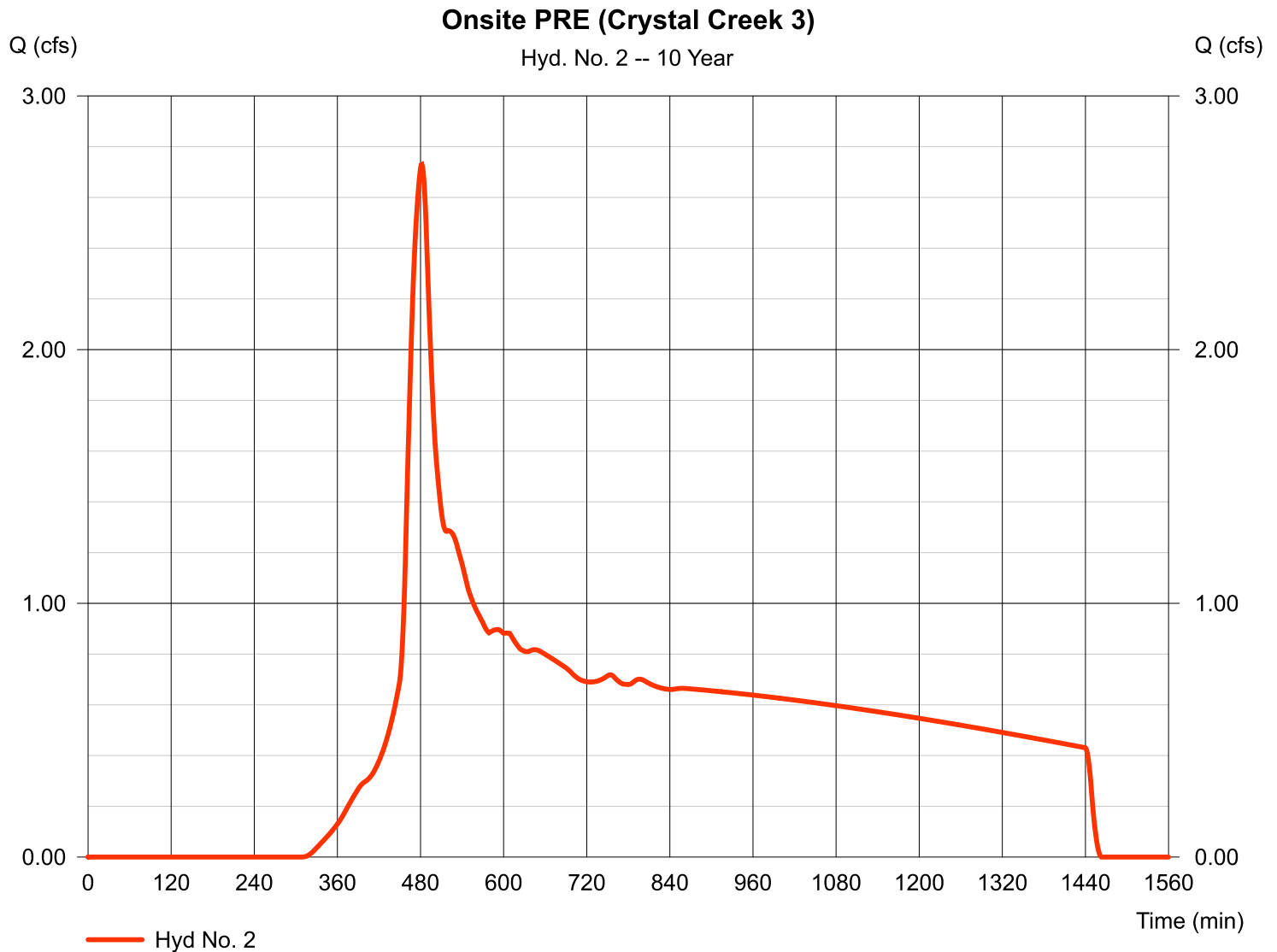
Hydrograph Report

Hyd. No. 2

Onsite PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 2.730 cfs
Storm frequency	= 10 yrs	Time to peak	= 482 min
Time interval	= 1 min	Hyd. volume	= 45,837 cuft
Drainage area	= 6.430 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 13.90 min
Total precip.	= 4.59 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(6.430 \times 73)] / 6.430$



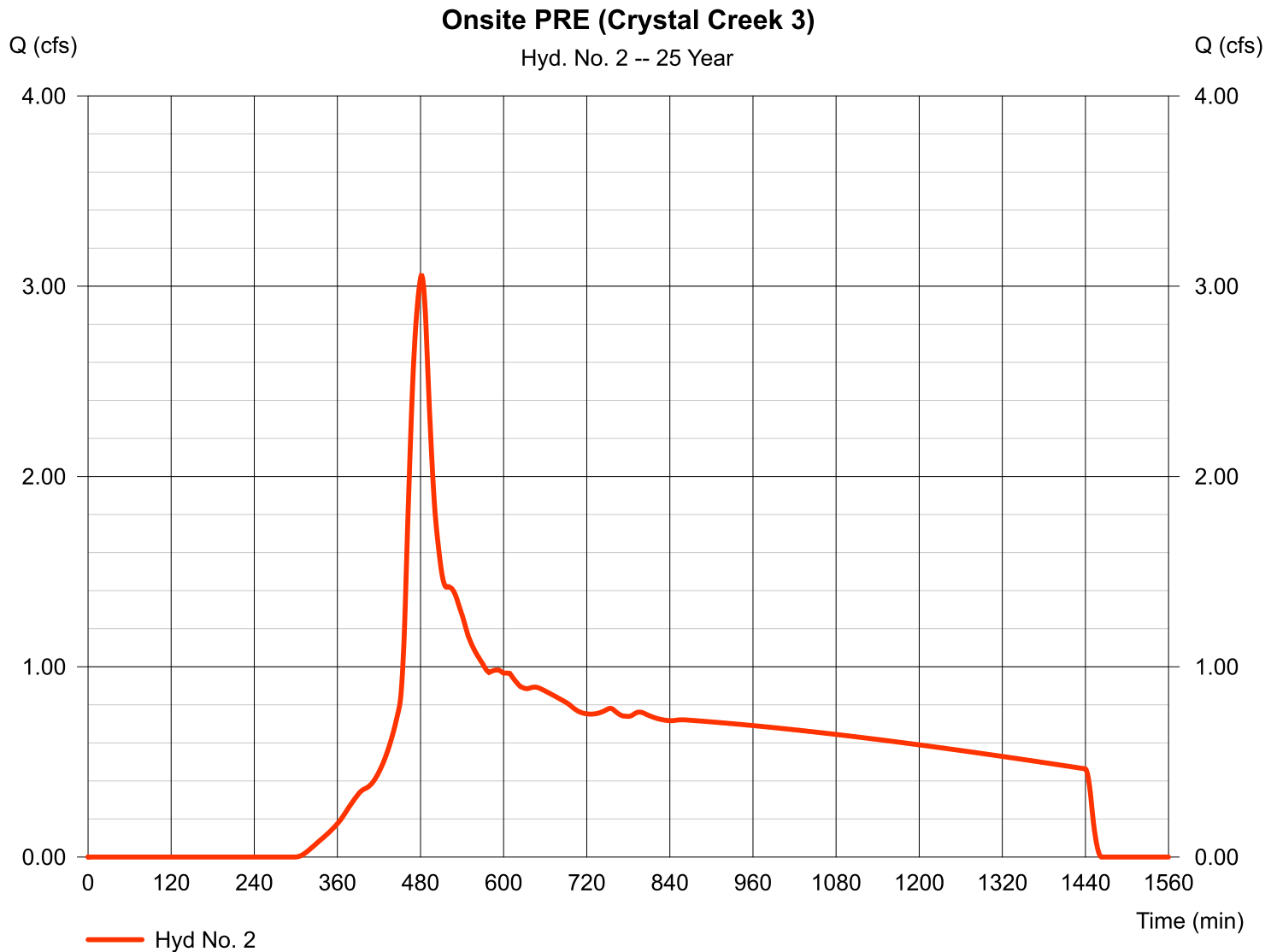
Hydrograph Report

Hyd. No. 2

Onsite PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 3.055 cfs
Storm frequency	= 25 yrs	Time to peak	= 481 min
Time interval	= 1 min	Hyd. volume	= 50,316 cuft
Drainage area	= 6.430 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 13.90 min
Total precip.	= 4.84 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(6.430 x 73)] / 6.430



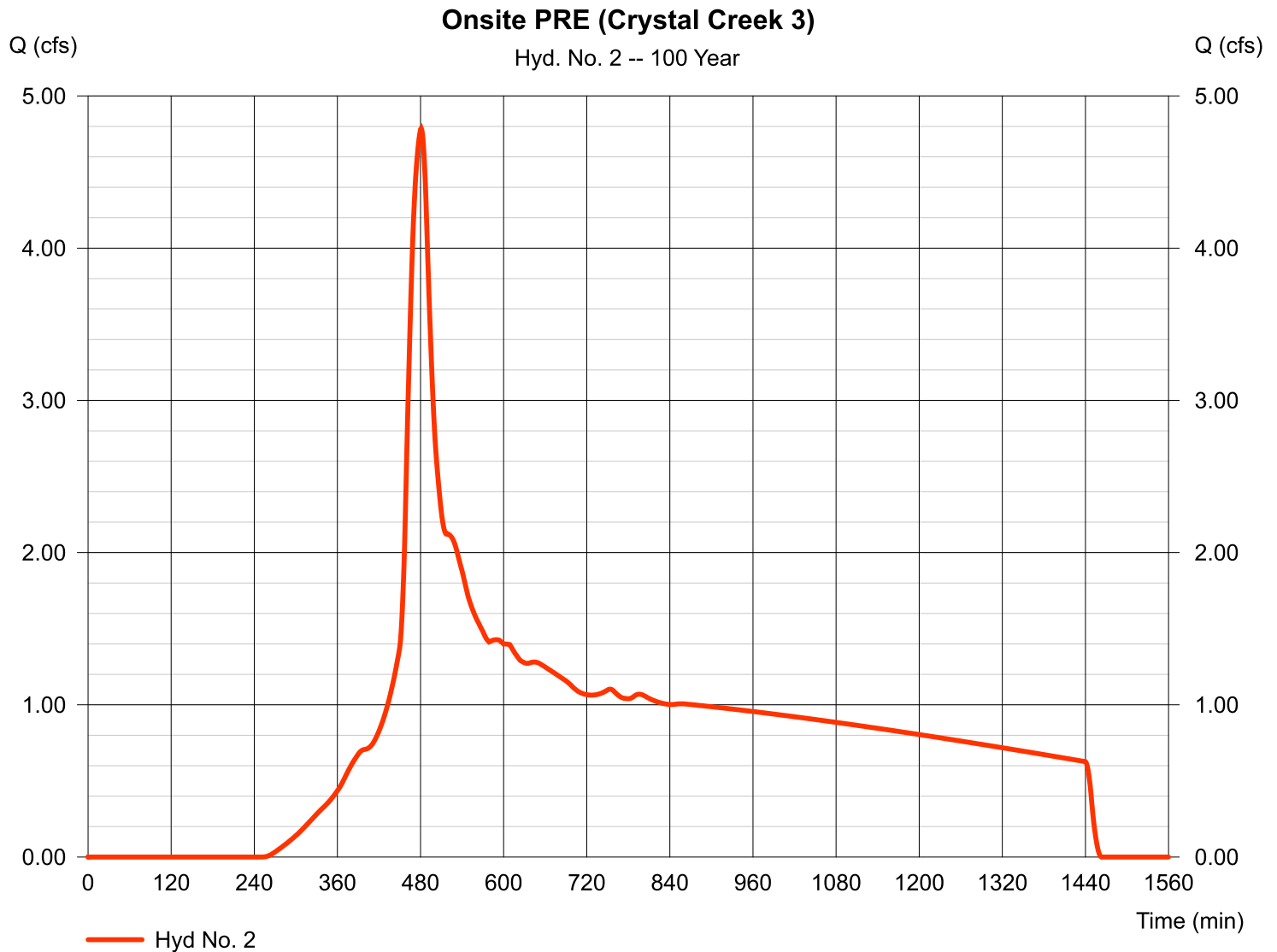
Hydrograph Report

Hyd. No. 2

Onsite PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 4.787 cfs
Storm frequency	= 100 yrs	Time to peak	= 481 min
Time interval	= 1 min	Hyd. volume	= 73,837 cuft
Drainage area	= 6.430 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 13.90 min
Total precip.	= 6.09 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(6.430 x 73)] / 6.430



TR55 Tc Worksheet

Hyd. No. 3

Upstream Post (Crystal Creek 3)

<u>Description</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>Totals</u>
Sheet Flow				
Manning's n-value	= 0.350	0.011	0.011	
Flow length (ft)	= 209.0	0.0	0.0	
Two-year 24-hr precip. (in)	= 3.34	0.00	0.00	
Land slope (%)	= 12.00	0.00	0.00	
Travel Time (min)	= 16.64	+ 0.00	+ 0.00	= 16.64
Shallow Concentrated Flow				
Flow length (ft)	= 0.00	0.00	0.00	
Watercourse slope (%)	= 0.00	0.00	0.00	
Surface description	= Paved	Paved	Paved	
Average velocity (ft/s)	=0.00	0.00	0.00	
Travel Time (min)	= 0.00	+ 0.00	+ 0.00	= 0.00
Channel Flow				
X sectional flow area (sqft)	= 0.00	0.00	0.00	
Wetted perimeter (ft)	= 0.00	0.00	0.00	
Channel slope (%)	= 0.00	0.00	0.00	
Manning's n-value	= 0.015	0.015	0.015	
Velocity (ft/s)	=0.00	0.00	0.00	
Flow length (ft)	0.0	0.0	0.0	
Travel Time (min)	= 0.00	+ 0.00	+ 0.00	= 0.00
Total Travel Time, Tc				16.60 min

Hydrograph Report

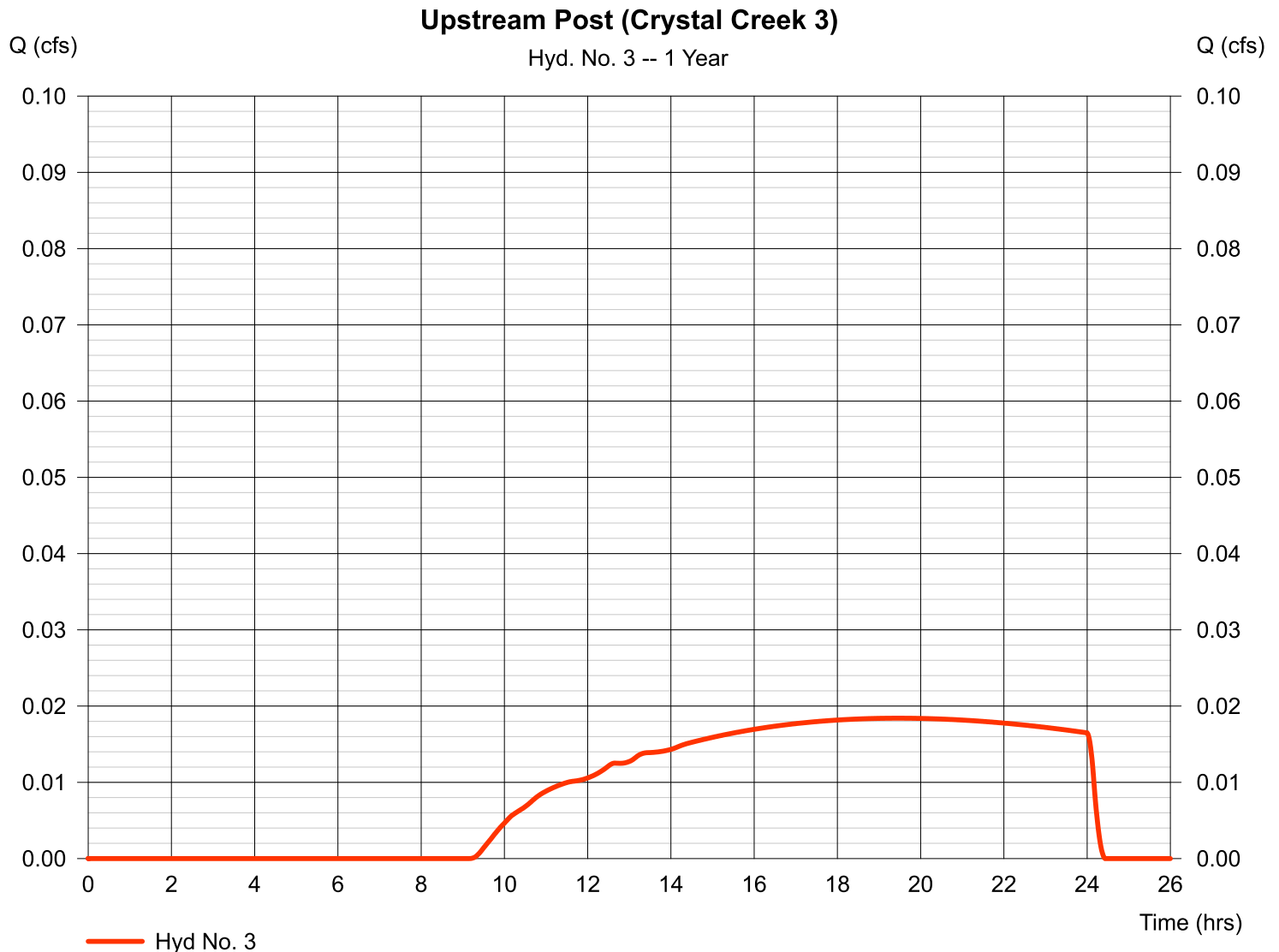
Hyd. No. 3

*1-yr is model for the 6 mo, 24 hr precip

Upstream Post (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.018 cfs
Storm frequency	= 1 yrs	Time to peak	= 19.47 hrs
Time interval	= 1 min	Hyd. volume	= 798 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 1.0 %	Hydraulic length	= 1 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 1.40 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(2.170 \times 73)] / 2.170$



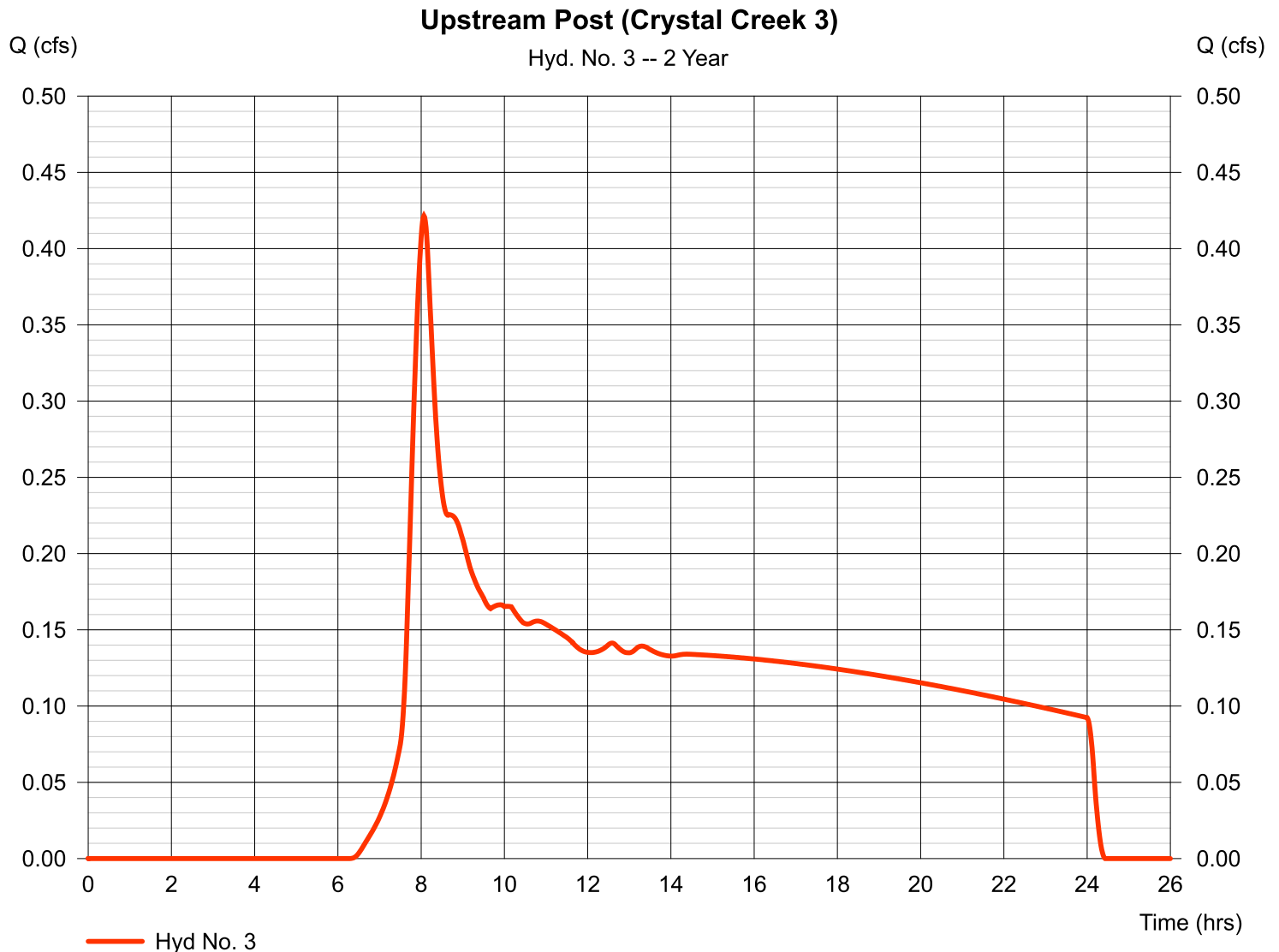
Hydrograph Report

Hyd. No. 3

Upstream Post (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.421 cfs
Storm frequency	= 2 yrs	Time to peak	= 8.07 hrs
Time interval	= 1 min	Hyd. volume	= 8,561 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 1.0 %	Hydraulic length	= 1 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 3.34 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(2.170 \times 73)] / 2.170$



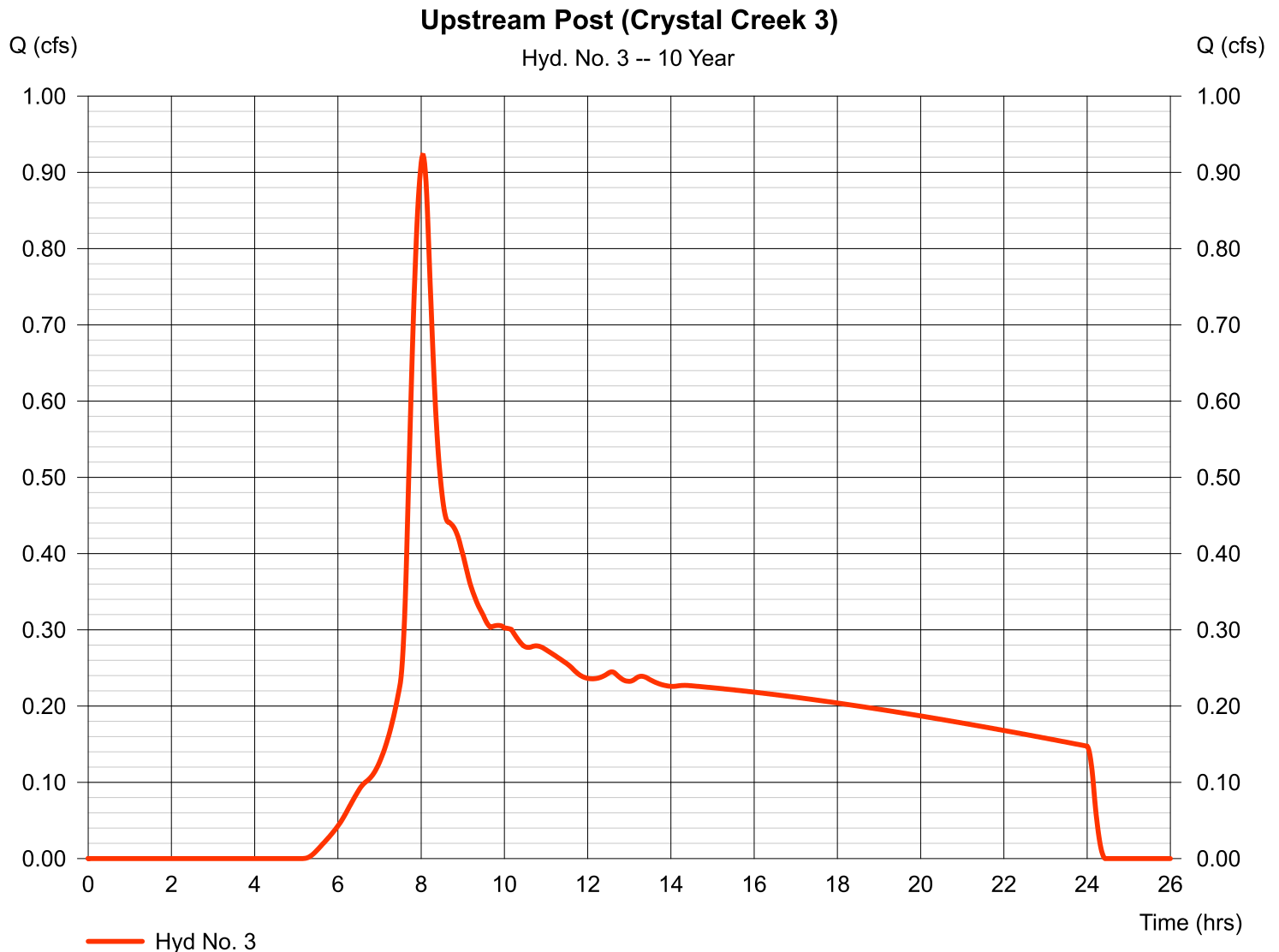
Hydrograph Report

Hyd. No. 3

Upstream Post (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.922 cfs
Storm frequency	= 10 yrs	Time to peak	= 8.03 hrs
Time interval	= 1 min	Hyd. volume	= 15,662 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 1.0 %	Hydraulic length	= 1 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 4.59 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(2.170 \times 73)] / 2.170$



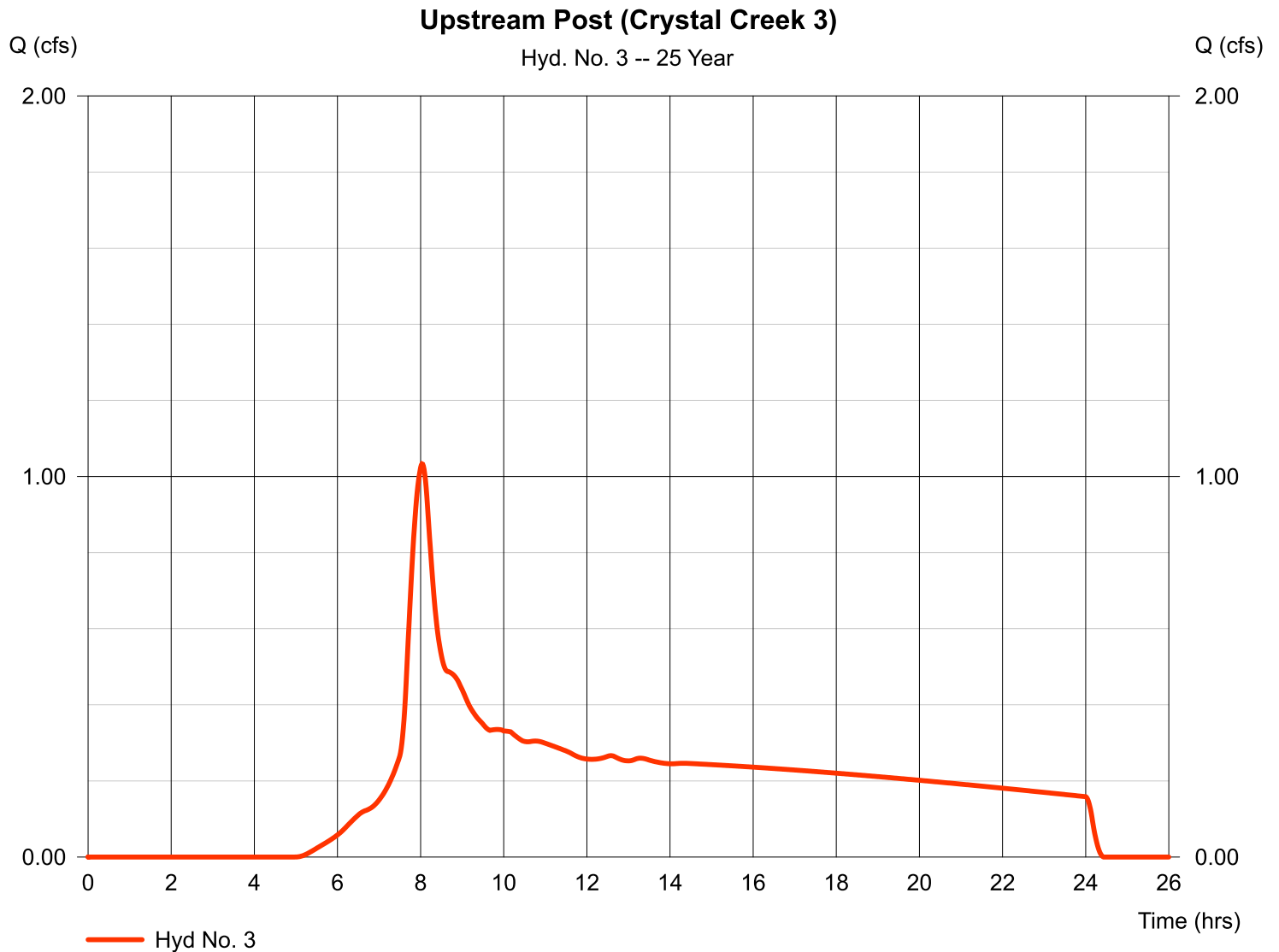
Hydrograph Report

Hyd. No. 3

Upstream Post (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 1.033 cfs
Storm frequency	= 25 yrs	Time to peak	= 8.03 hrs
Time interval	= 1 min	Hyd. volume	= 17,193 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 1.0 %	Hydraulic length	= 1 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 4.84 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(2.170 x 73)] / 2.170



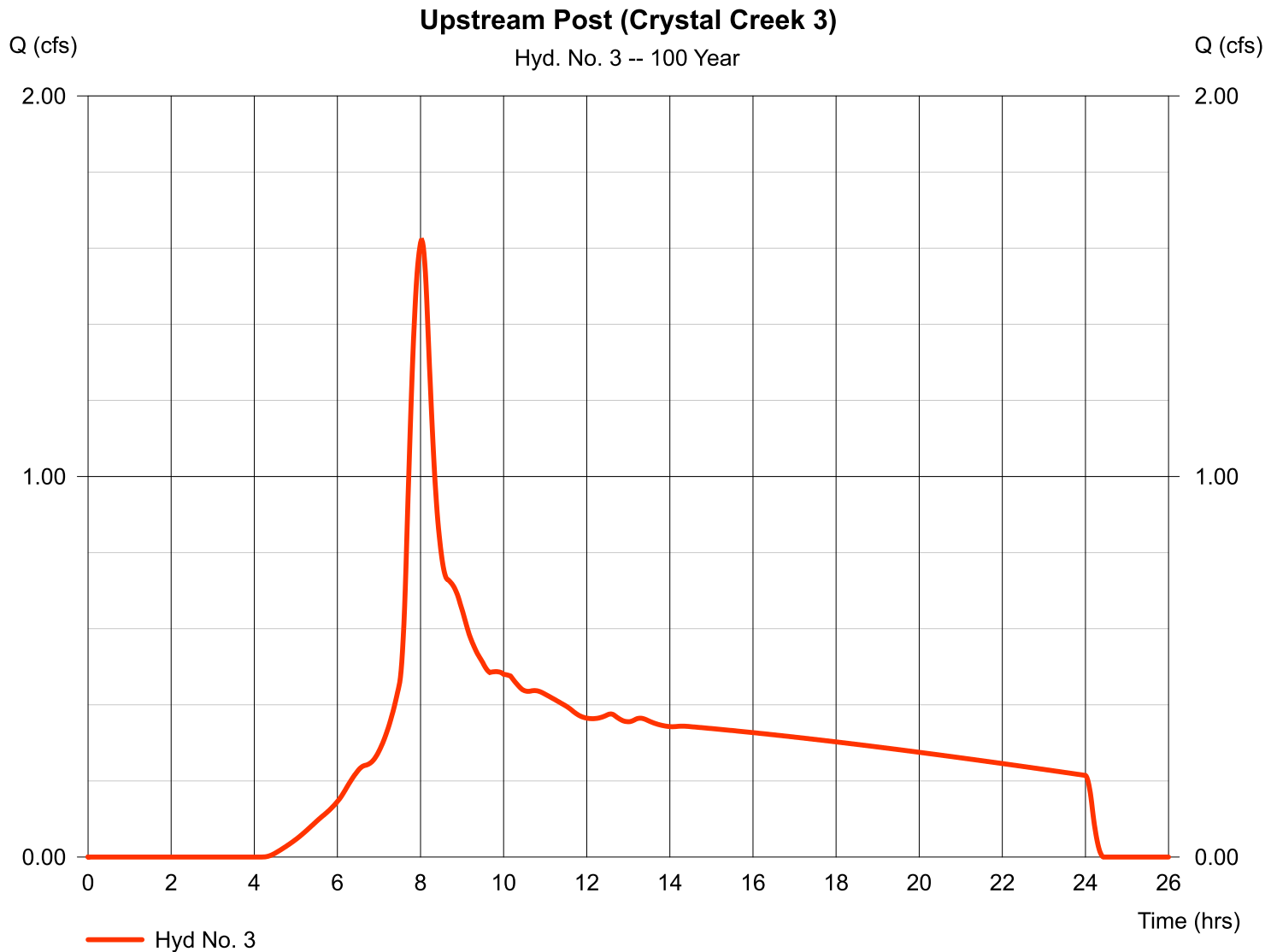
Hydrograph Report

Hyd. No. 3

Upstream Post (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 1.620 cfs
Storm frequency	= 100 yrs	Time to peak	= 8.03 hrs
Time interval	= 1 min	Hyd. volume	= 25,230 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 1.0 %	Hydraulic length	= 1 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 6.09 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(2.170 \times 73)] / 2.170$



TR55 Tc Worksheet

Hyd. No. 4

POST (Crystal Creek 3)

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow							
Manning's n-value	= 0.350		0.011		0.011		
Flow length (ft)	= 95.0		0.0		0.0		
Two-year 24-hr precip. (in)	= 3.34		0.00		0.00		
Land slope (%)	= 19.00		0.00		0.00		
Travel Time (min)	= 7.37	+	0.00	+	0.00	=	7.37
Shallow Concentrated Flow							
Flow length (ft)	= 40.00		6.00		0.00		
Watercourse slope (%)	= 2.00		33.00		0.00		
Surface description	= Paved		Unpaved		Paved		
Average velocity (ft/s)	=2.87		9.27		0.00		
Travel Time (min)	= 0.23	+	0.01	+	0.00	=	0.24
Channel Flow							
X sectional flow area (sqft)	= 11.25		0.08		0.00		
Wetted perimeter (ft)	= 12.48		0.52		0.00		
Channel slope (%)	= 4.00		12.00		0.00		
Manning's n-value	= 0.350		0.012		0.015		
Velocity (ft/s)	=0.79		12.27		0.00		
Flow length (ft)	357.0		223.0		0.0		
Travel Time (min)	= 7.49	+	0.30	+	0.00	=	7.79
Total Travel Time, Tc							15.40 min

Hydrograph Report

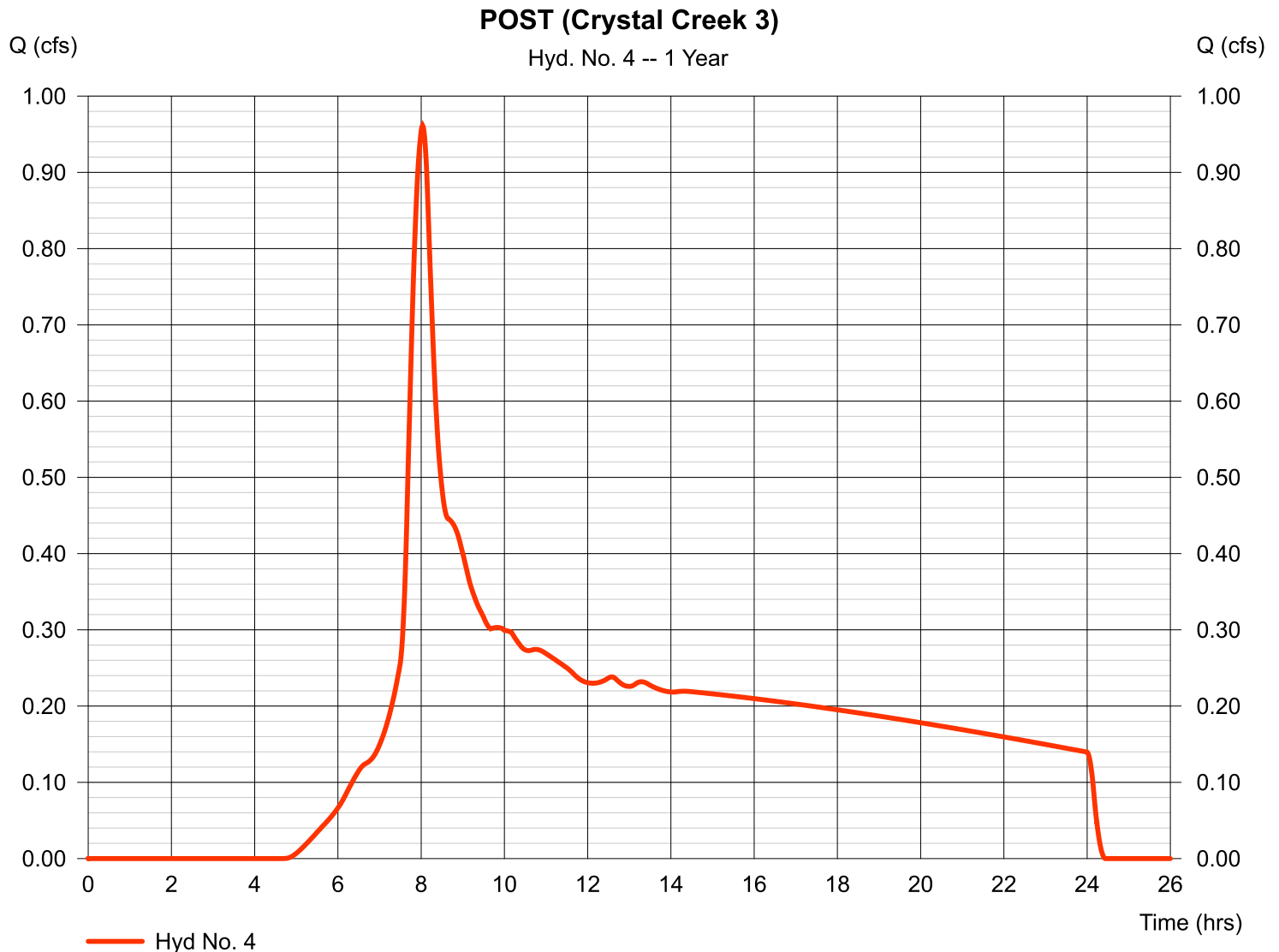
Hyd. No. 4

*1-yr is model for the 6 mo, 24 hr precip

POST (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.961 cfs
Storm frequency	= 1 yrs	Time to peak	= 8.03 hrs
Time interval	= 1 min	Hyd. volume	= 15,588 cuft
Drainage area	= 6.430 ac	Curve number	= 91*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.40 min
Total precip.	= 1.40 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(4.180 x 98) + (2.250 x 79)] / 6.430



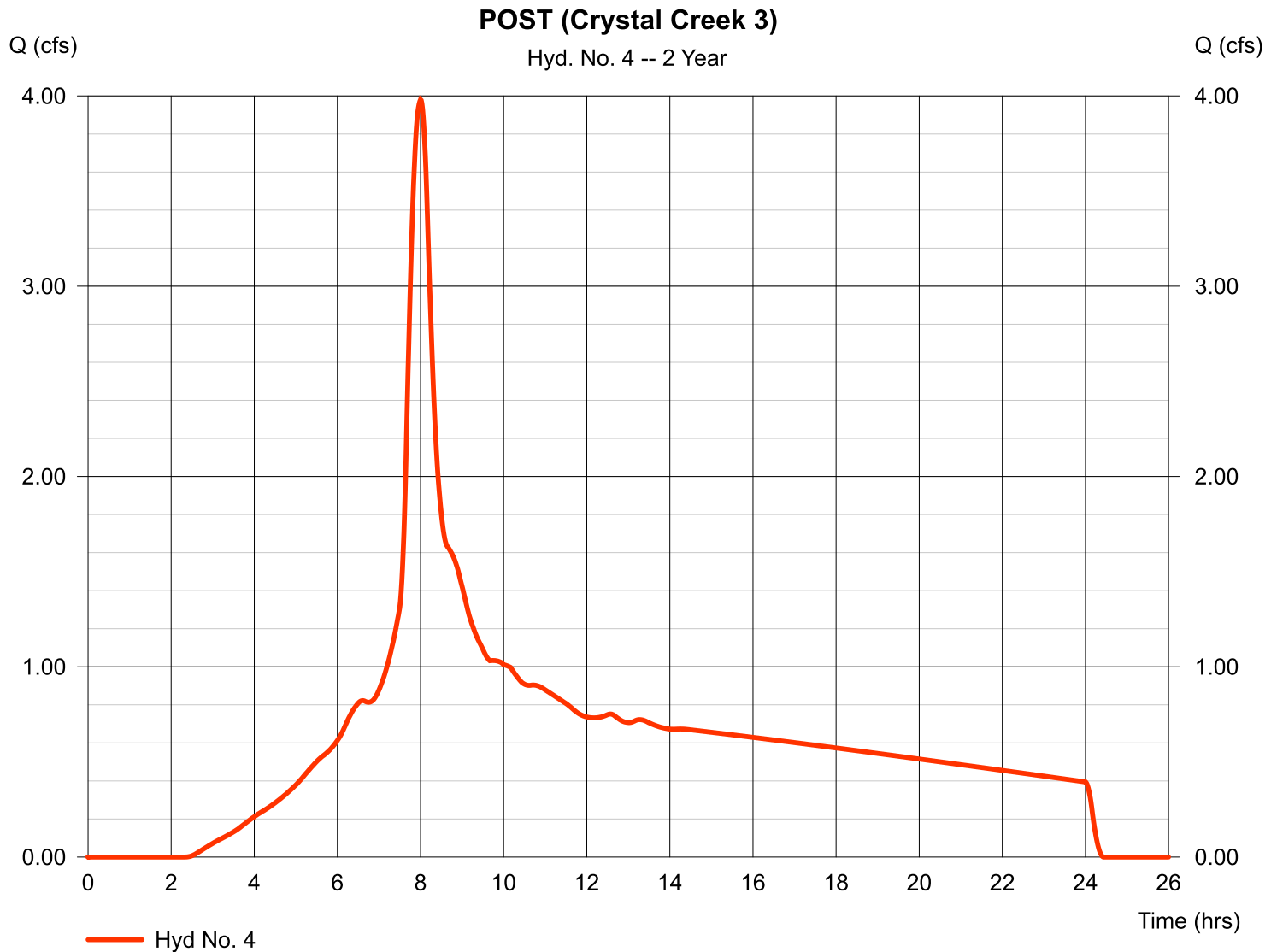
Hydrograph Report

Hyd. No. 4

POST (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 3.981 cfs
Storm frequency	= 2 yrs	Time to peak	= 8.00 hrs
Time interval	= 1 min	Hyd. volume	= 56,481 cuft
Drainage area	= 6.430 ac	Curve number	= 91*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.40 min
Total precip.	= 3.34 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(4.180 x 98) + (2.250 x 79)] / 6.430



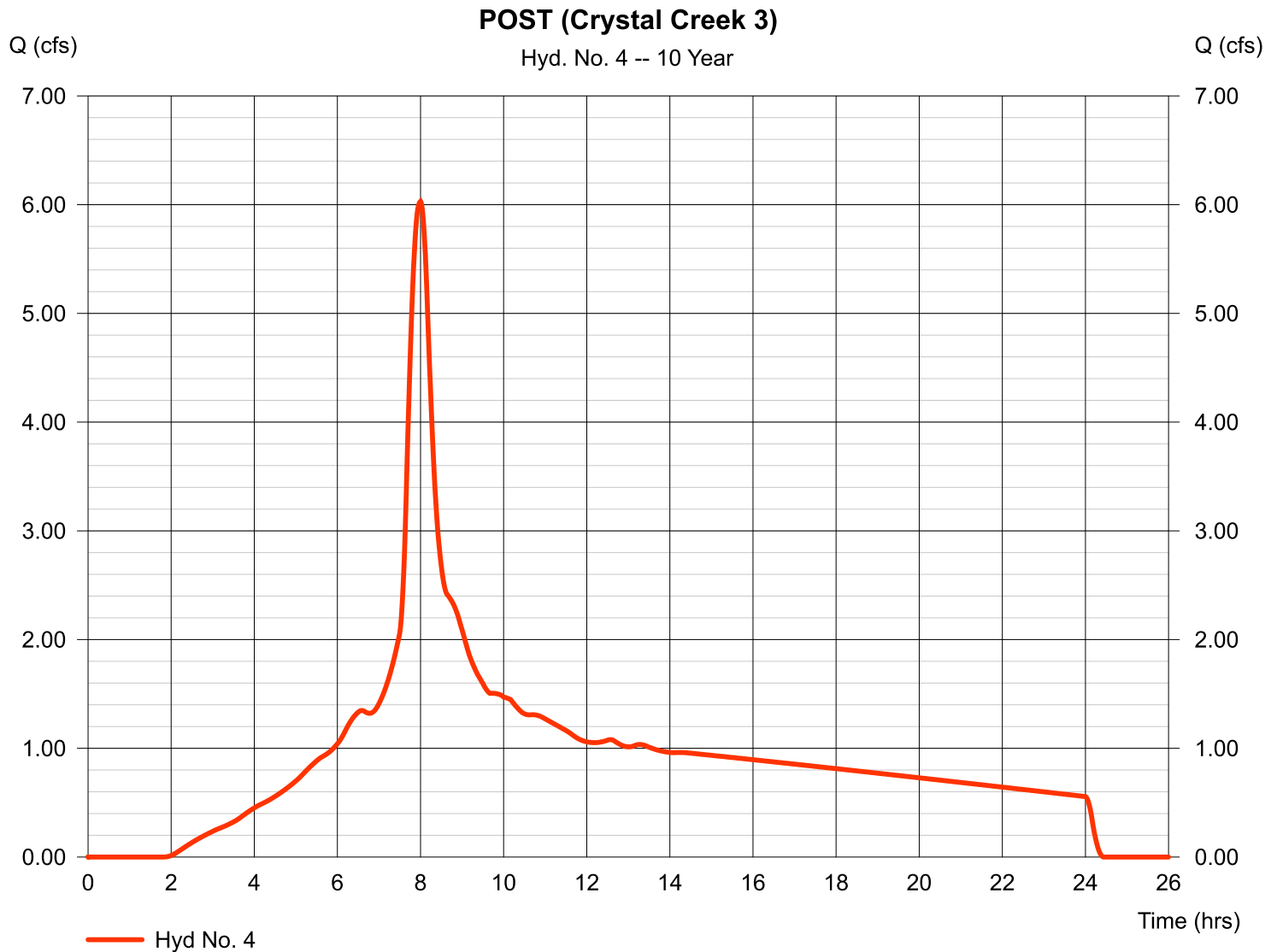
Hydrograph Report

Hyd. No. 4

POST (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 6.030 cfs
Storm frequency	= 10 yrs	Time to peak	= 8.00 hrs
Time interval	= 1 min	Hyd. volume	= 84,722 cuft
Drainage area	= 6.430 ac	Curve number	= 91*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.40 min
Total precip.	= 4.59 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(4.180 x 98) + (2.250 x 79)] / 6.430



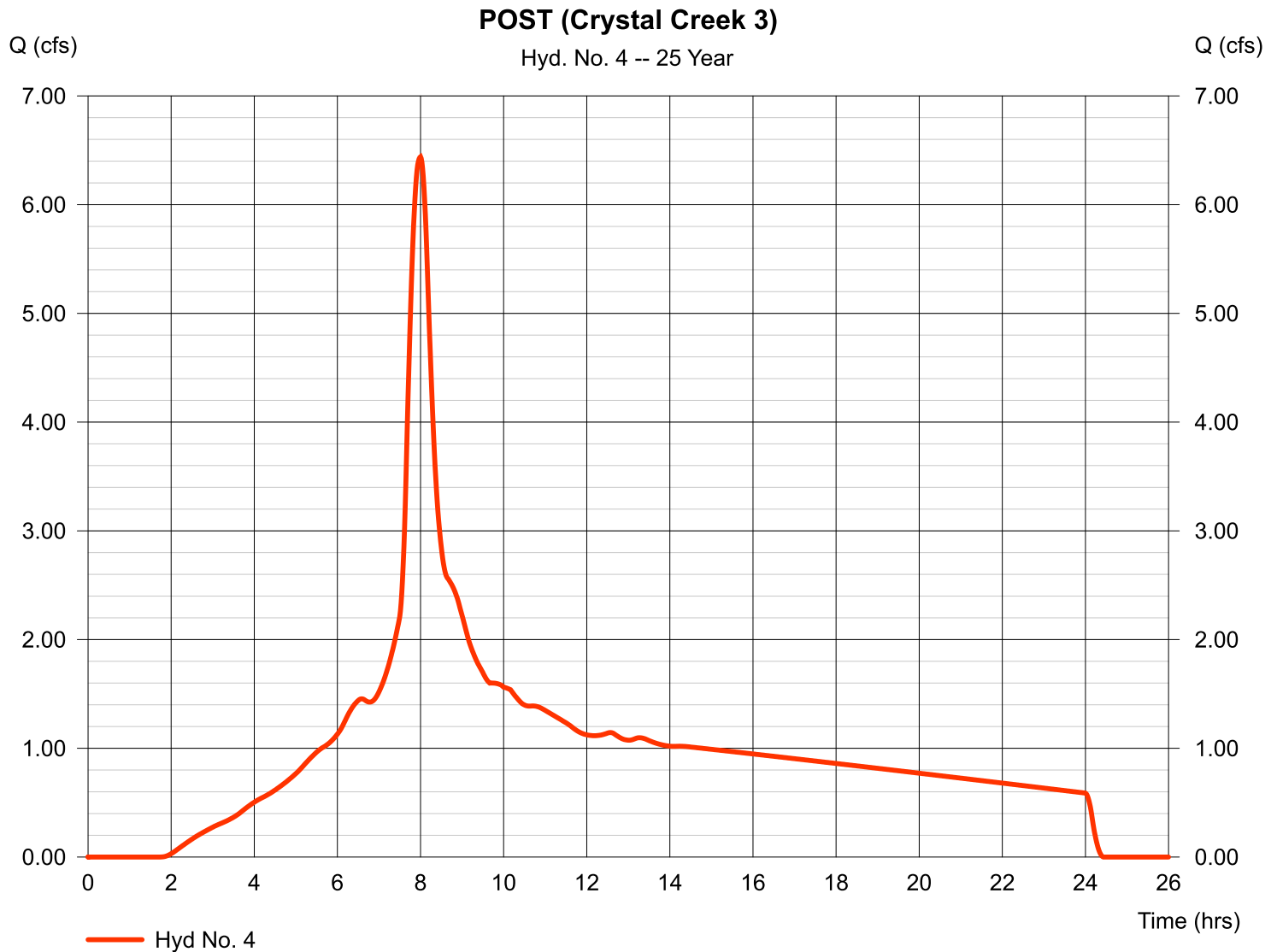
Hydrograph Report

Hyd. No. 4

POST (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 6.440 cfs
Storm frequency	= 25 yrs	Time to peak	= 8.00 hrs
Time interval	= 1 min	Hyd. volume	= 90,440 cuft
Drainage area	= 6.430 ac	Curve number	= 91*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.40 min
Total precip.	= 4.84 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(4.180 x 98) + (2.250 x 79)] / 6.430



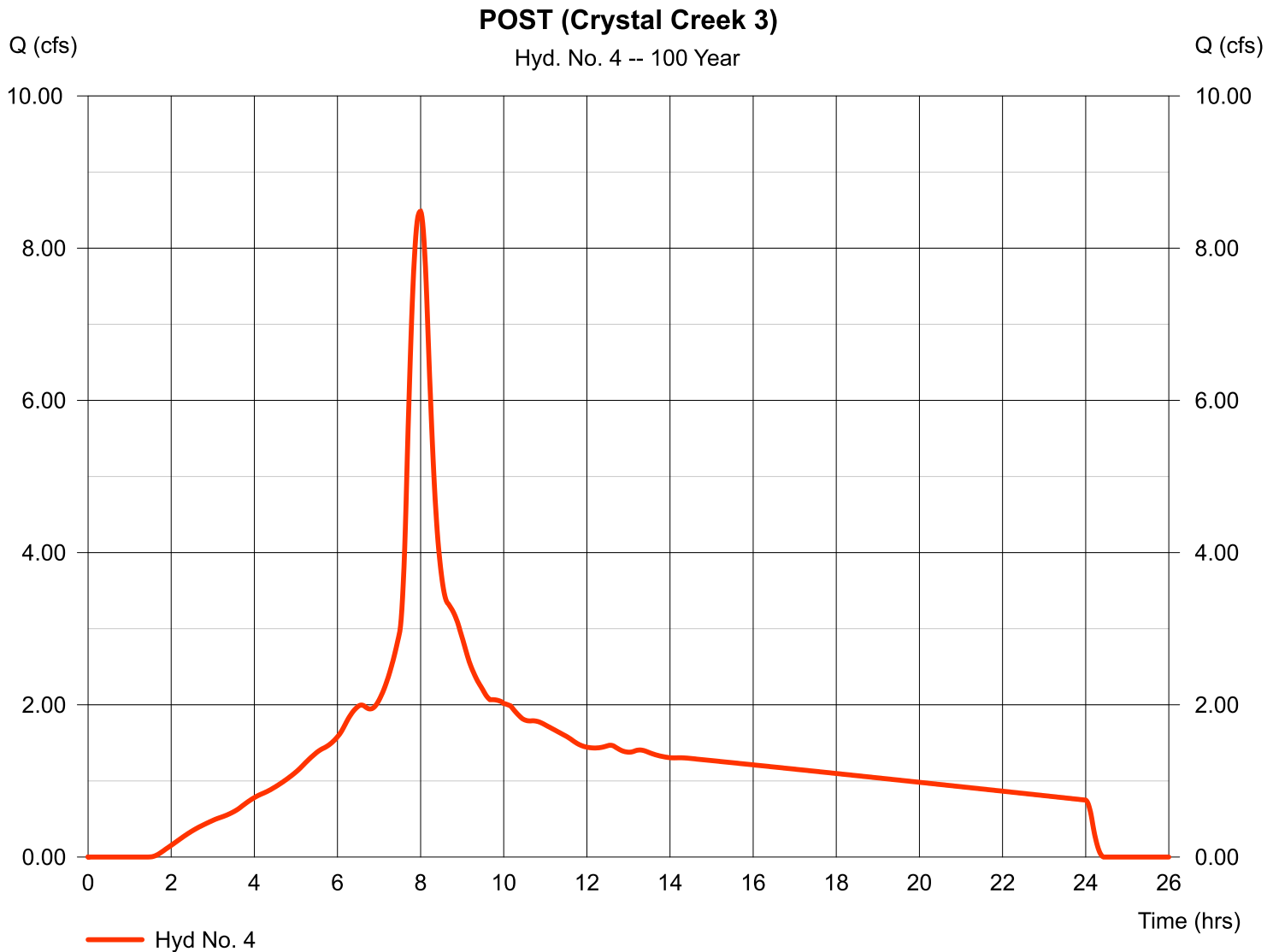
Hydrograph Report

Hyd. No. 4

POST (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 8.483 cfs
Storm frequency	= 100 yrs	Time to peak	= 8.00 hrs
Time interval	= 1 min	Hyd. volume	= 119,235 cuft
Drainage area	= 6.430 ac	Curve number	= 91*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.40 min
Total precip.	= 6.09 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(4.180 x 98) + (2.250 x 79)] / 6.430



Pond Report

Pond No. 1 - Vault C (3900)

Pond Data

Contours -User-defined contour areas. Average end area method used for volume calculation. Beginning Elevation = 100.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	100.00	3,900	0	0
1.00	101.00	3,900	3,900	3,900
2.00	102.00	3,900	3,900	7,800
3.00	103.00	3,900	3,900	11,700
4.00	104.00	3,900	3,900	15,600
5.00	105.00	3,900	3,900	19,500
6.00	106.00	3,900	3,900	23,400
7.00	107.00	3,900	3,900	27,300
8.00	108.00	3,900	3,900	31,200
9.00	109.00	3,900	3,900	35,100

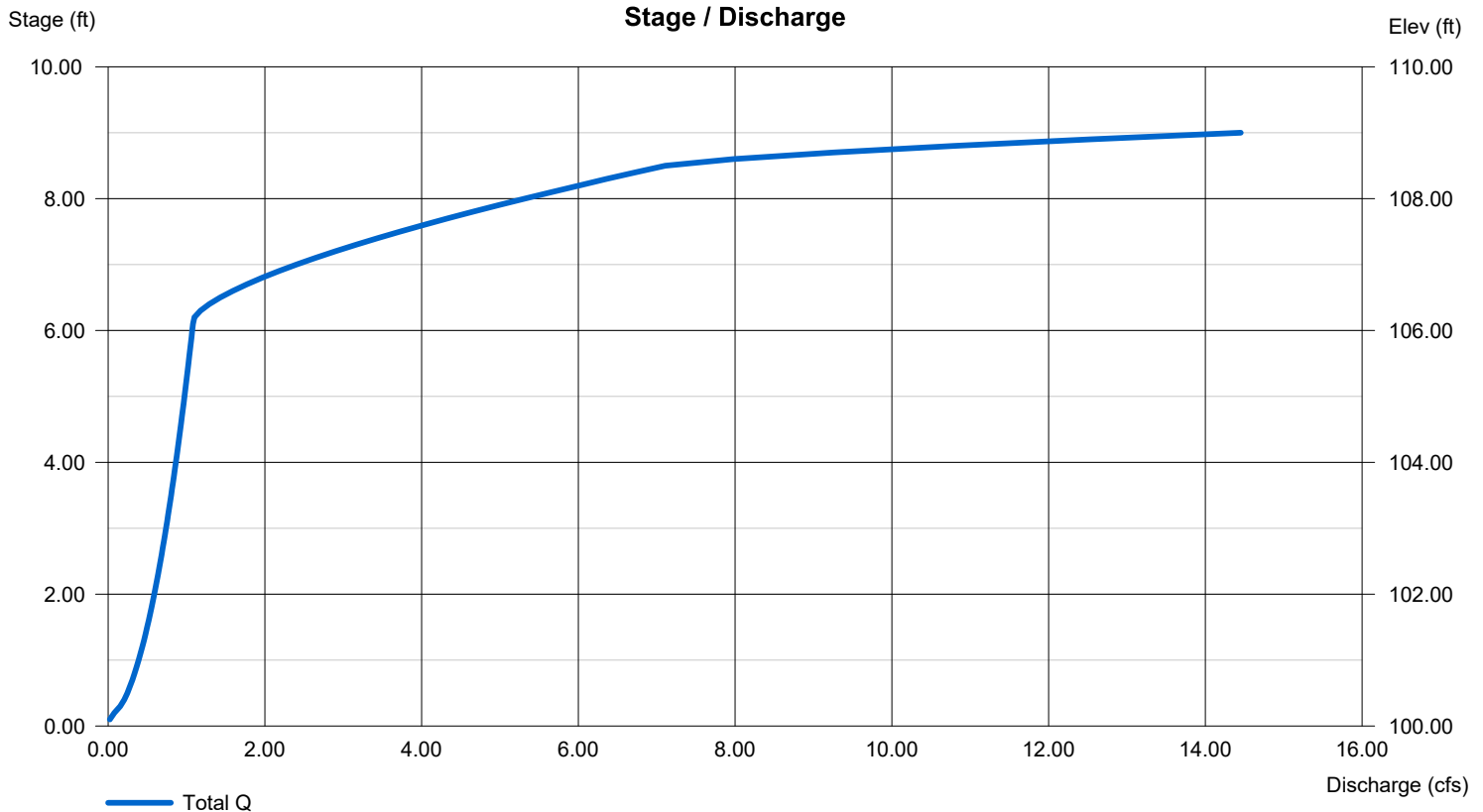
Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 18.00	4.17	Inactive	Inactive
Span (in)	= 18.00	4.17	0.00	0.00
No. Barrels	= 1	1	1	1
Invert El. (ft)	= 100.00	100.00	0.00	0.00
Length (ft)	= 104.00	0.00	0.00	0.00
Slope (%)	= 0.60	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	Yes	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 4.71	0.50	Inactive	0.00
Crest El. (ft)	= 108.50	106.17	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= 1	Rect	Rect	---
Multi-Stage	= Yes	Yes	No	No
Exfil.(in/hr)	= 0.000	(by Wet area)		
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Tuesday, 06 / 16 / 2020

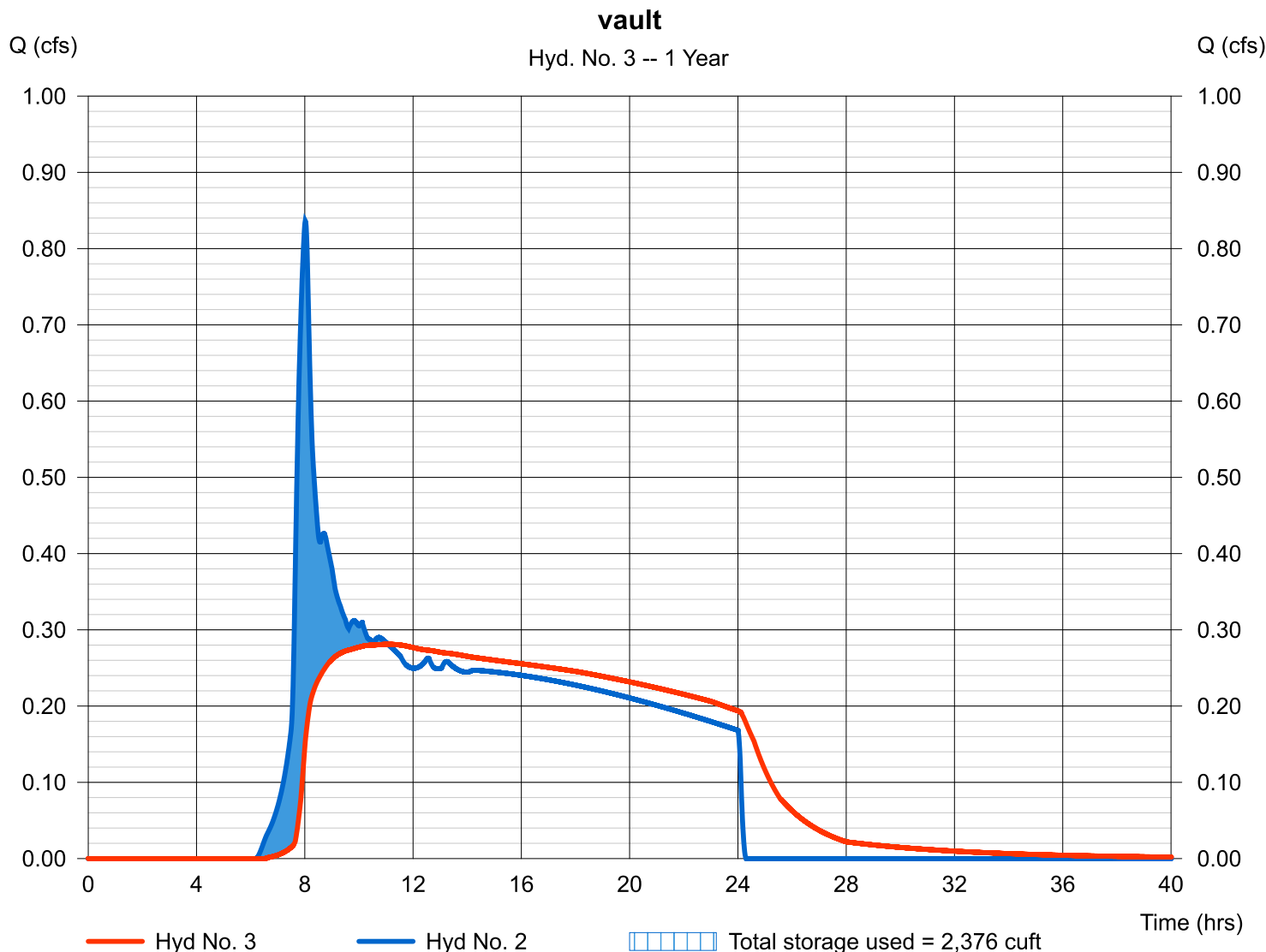
Hyd. No. 3

*1-yr is model for the 6 mo, 24 hr precip

vault

Hydrograph type	= Reservoir	Peak discharge	= 0.281 cfs
Storm frequency	= 1 yrs	Time to peak	= 11.07 hrs
Time interval	= 1 min	Hyd. volume	= 15,897 cuft
Inflow hyd. No.	= 2 - POST (Crystal Creek 5)	Max. Elevation	= 100.61 ft
Reservoir name	= Vault C (3900)	Max. Storage	= 2,376 cuft

Storage Indication method used.



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

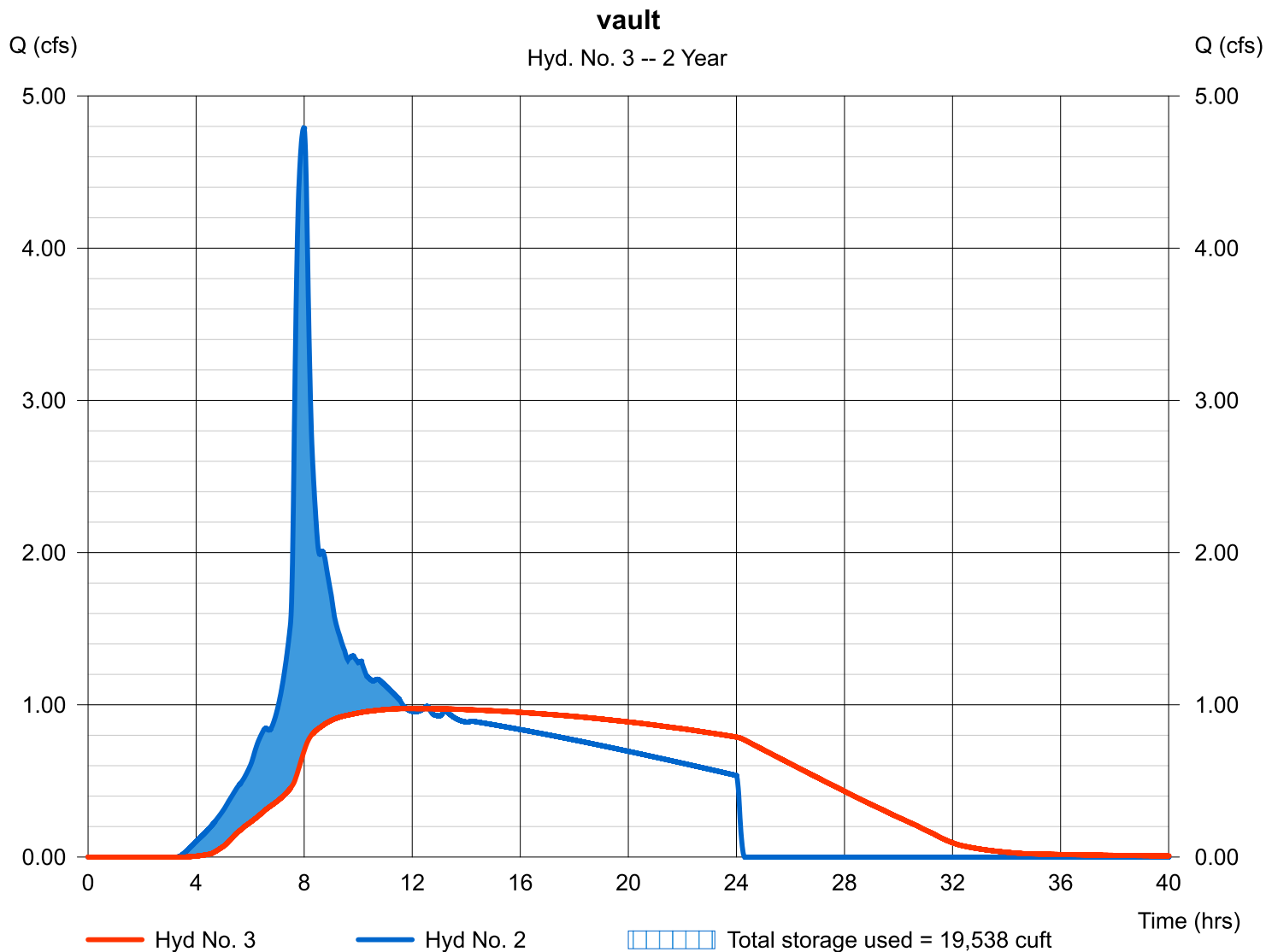
Tuesday, 06 / 16 / 2020

Hyd. No. 3

vault

Hydrograph type	= Reservoir	Peak discharge	= 0.975 cfs
Storm frequency	= 2 yrs	Time to peak	= 11.78 hrs
Time interval	= 1 min	Hyd. volume	= 69,442 cuft
Inflow hyd. No.	= 2 - POST (Crystal Creek 5)	Max. Elevation	= 105.01 ft
Reservoir name	= Vault C (3900)	Max. Storage	= 19,538 cuft

Storage Indication method used.



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

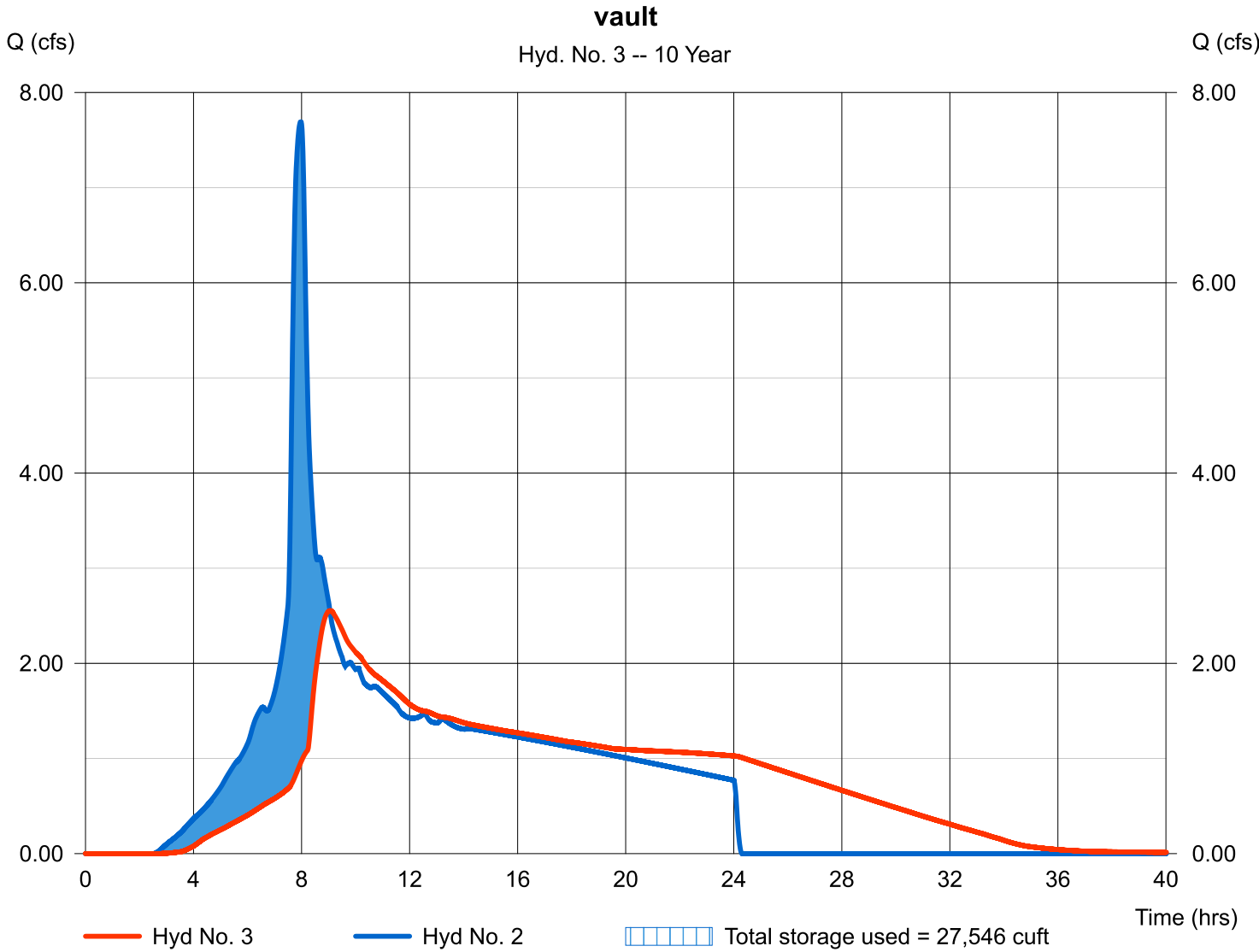
Tuesday, 06 / 16 / 2020

Hyd. No. 3

vault

Hydrograph type	= Reservoir	Peak discharge	= 2.553 cfs
Storm frequency	= 10 yrs	Time to peak	= 9.05 hrs
Time interval	= 1 min	Hyd. volume	= 108,383 cuft
Inflow hyd. No.	= 2 - POST (Crystal Creek 5)	Max. Elevation	= 107.06 ft
Reservoir name	= Vault C (3900)	Max. Storage	= 27,546 cuft

Storage Indication method used.



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

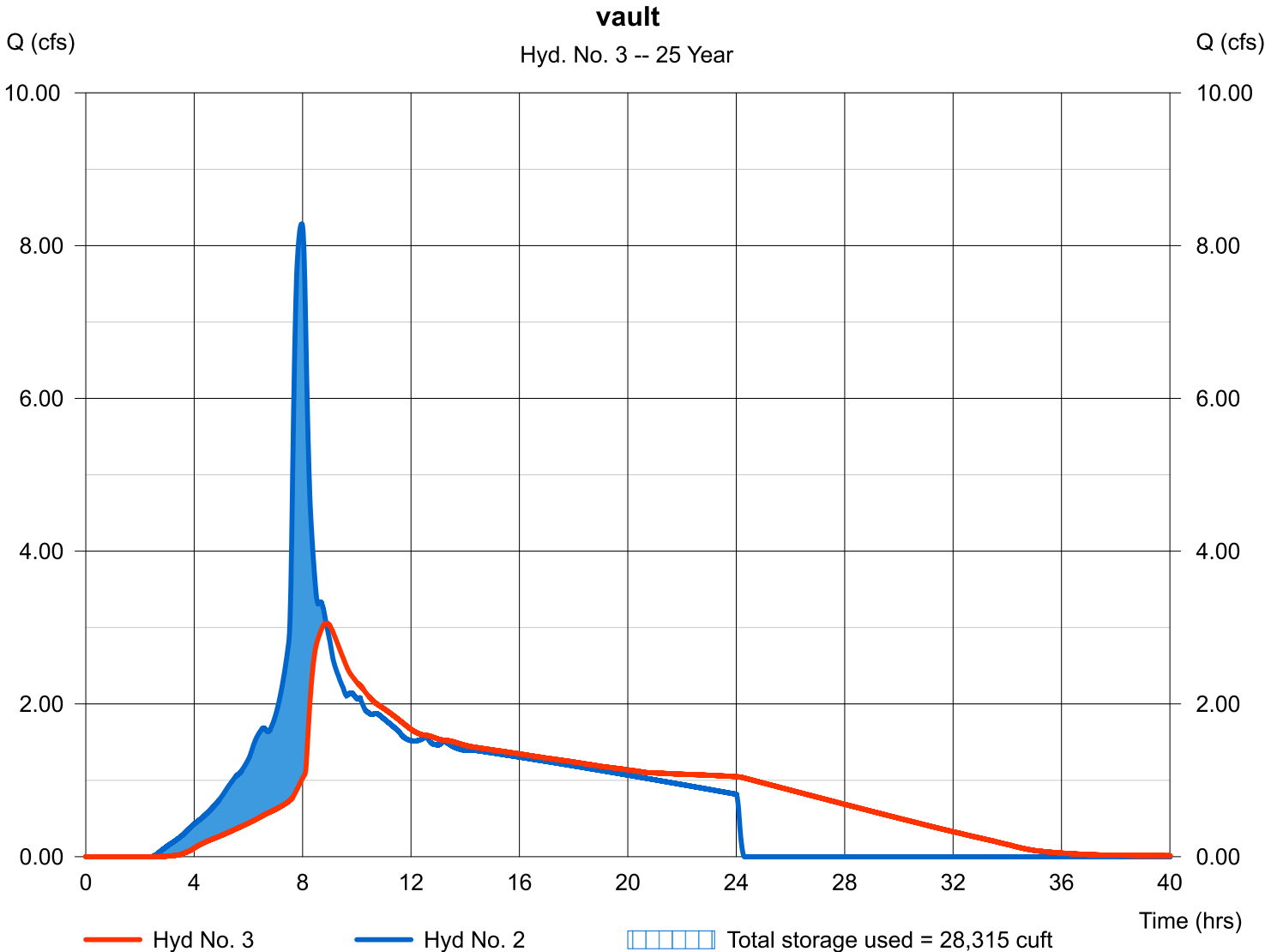
Tuesday, 06 / 16 / 2020

Hyd. No. 3

vault

Hydrograph type	= Reservoir	Peak discharge	= 3.054 cfs
Storm frequency	= 25 yrs	Time to peak	= 8.87 hrs
Time interval	= 1 min	Hyd. volume	= 116,353 cuft
Inflow hyd. No.	= 2 - POST (Crystal Creek 5)	Max. Elevation	= 107.26 ft
Reservoir name	= Vault C (3900)	Max. Storage	= 28,315 cuft

Storage Indication method used.



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

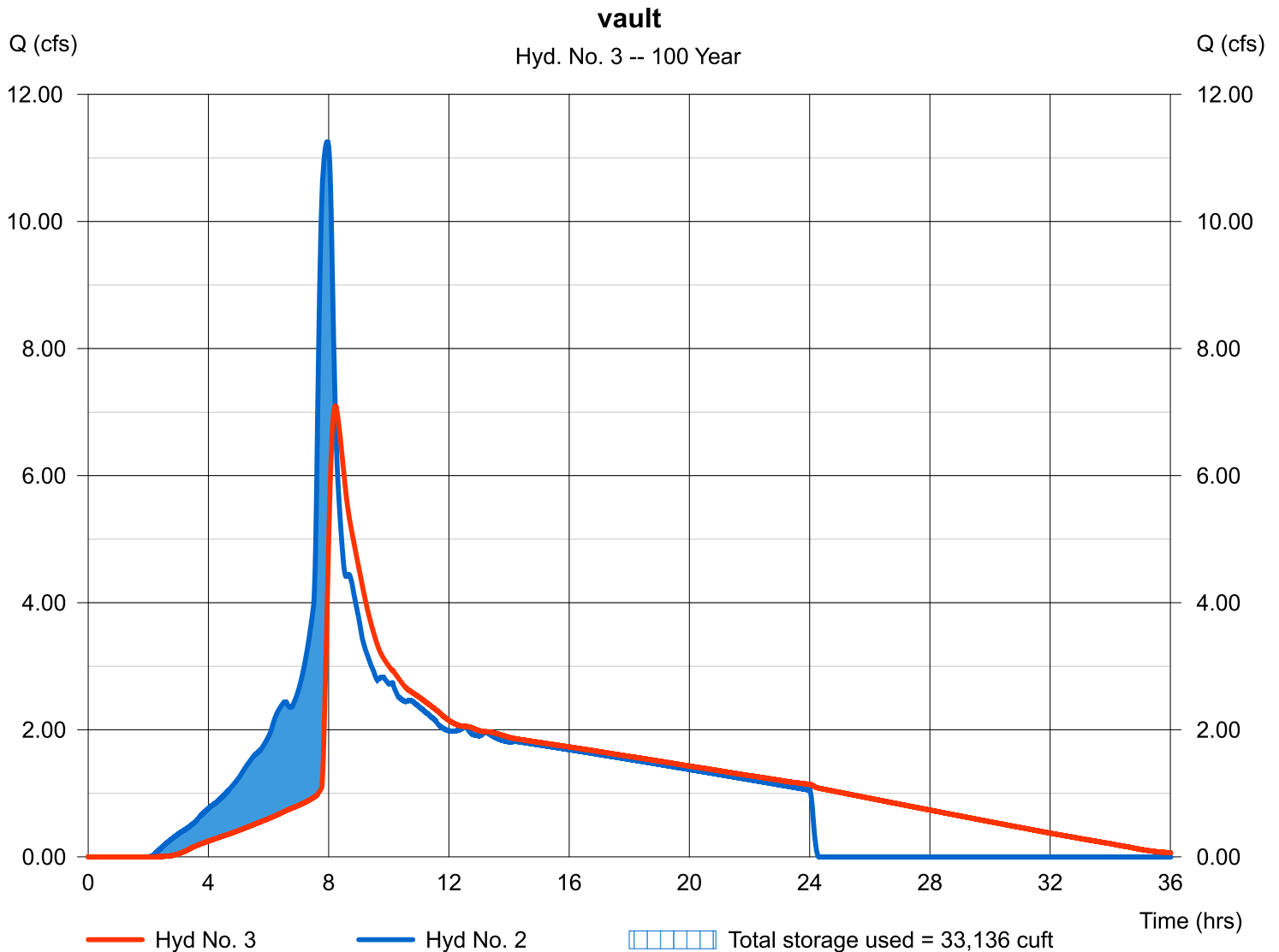
Tuesday, 06 / 16 / 2020

Hyd. No. 3

vault

Hydrograph type	= Reservoir	Peak discharge	= 7.095 cfs
Storm frequency	= 100 yrs	Time to peak	= 8.22 hrs
Time interval	= 1 min	Hyd. volume	= 156,768 cuft
Inflow hyd. No.	= 2 - POST (Crystal Creek 5)	Max. Elevation	= 108.50 ft
Reservoir name	= Vault C (3900)	Max. Storage	= 33,136 cuft

Storage Indication method used.

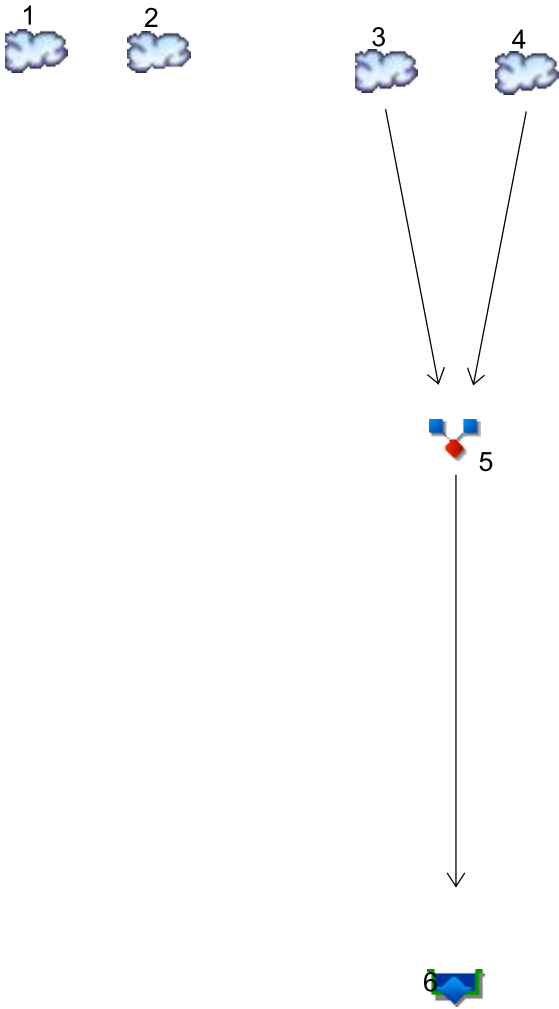


Crystal Creek 3 Detention Pond B7-A Output



Watershed Model Schematic

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Tuesday, 06 / 16 / 2020

Return Period (Yrs)	Intensity-Duration-Frequency Equation Coefficients (FHA)			
	B	D	E	(N/A)
1	0.0000	0.0000	0.0000	-----
2	0.0000	0.0000	0.0000	-----
3	0.0000	0.0000	0.0000	-----
5	0.0000	0.0000	0.0000	-----
10	0.0000	0.0000	0.0000	-----
25	0.0000	0.0000	0.0000	-----
50	0.0000	0.0000	0.0000	-----
100	0.0000	0.0000	0.0000	-----

File name: SampleFHA.idf

$$\text{Intensity} = B / (T_c + D)^E$$

Return Period (Yrs)	Intensity Values (in/hr)												
	5 min	10	15	20	25	30	35	40	45	50	55	60	
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
25	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

T_c = time in minutes. Values may exceed 60.

***1-yr column is the 6 mo, 24 hr precip**

Precip. file name: E:\Projects\19349\Engineering\Hydraflow\Phase 1\Pond 7B-A\precip.pcp

Storm Distribution	Rainfall Precipitation Table (in)							
	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
SCS 24-hour	1.40	3.34	0.00	3.30	4.59	4.84	6.80	6.09
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-1st	0.00	0.00	0.00	2.75	0.00	0.00	6.50	0.00
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Custom	0.00	0.00	0.00	2.80	0.00	0.00	6.00	0.00

TR55 Tc Worksheet

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No. 1

Upstream PRE (Crystal Creek 3)

<u>Description</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>Totals</u>
Sheet Flow				
Manning's n-value	= 0.350	0.011	0.011	
Flow length (ft)	= 209.0	0.0	0.0	
Two-year 24-hr precip. (in)	= 3.34	0.00	0.00	
Land slope (%)	= 12.00	0.00	0.00	
Travel Time (min)	= 16.64	+ 0.00	+ 0.00	= 16.64
Shallow Concentrated Flow				
Flow length (ft)	= 0.00	0.00	0.00	
Watercourse slope (%)	= 0.00	0.00	0.00	
Surface description	= Paved	Paved	Paved	
Average velocity (ft/s)	=0.00	0.00	0.00	
Travel Time (min)	= 0.00	+ 0.00	+ 0.00	= 0.00
Channel Flow				
X sectional flow area (sqft)	= 0.00	0.00	0.00	
Wetted perimeter (ft)	= 0.00	0.00	0.00	
Channel slope (%)	= 0.00	0.00	0.00	
Manning's n-value	= 0.015	0.015	0.015	
Velocity (ft/s)	=0.00	0.00	0.00	
Flow length (ft)	0.0	0.0	0.0	
Travel Time (min)	= 0.00	+ 0.00	+ 0.00	= 0.00
Total Travel Time, Tc				16.60 min

Hydrograph Report

Hyd. No. 1

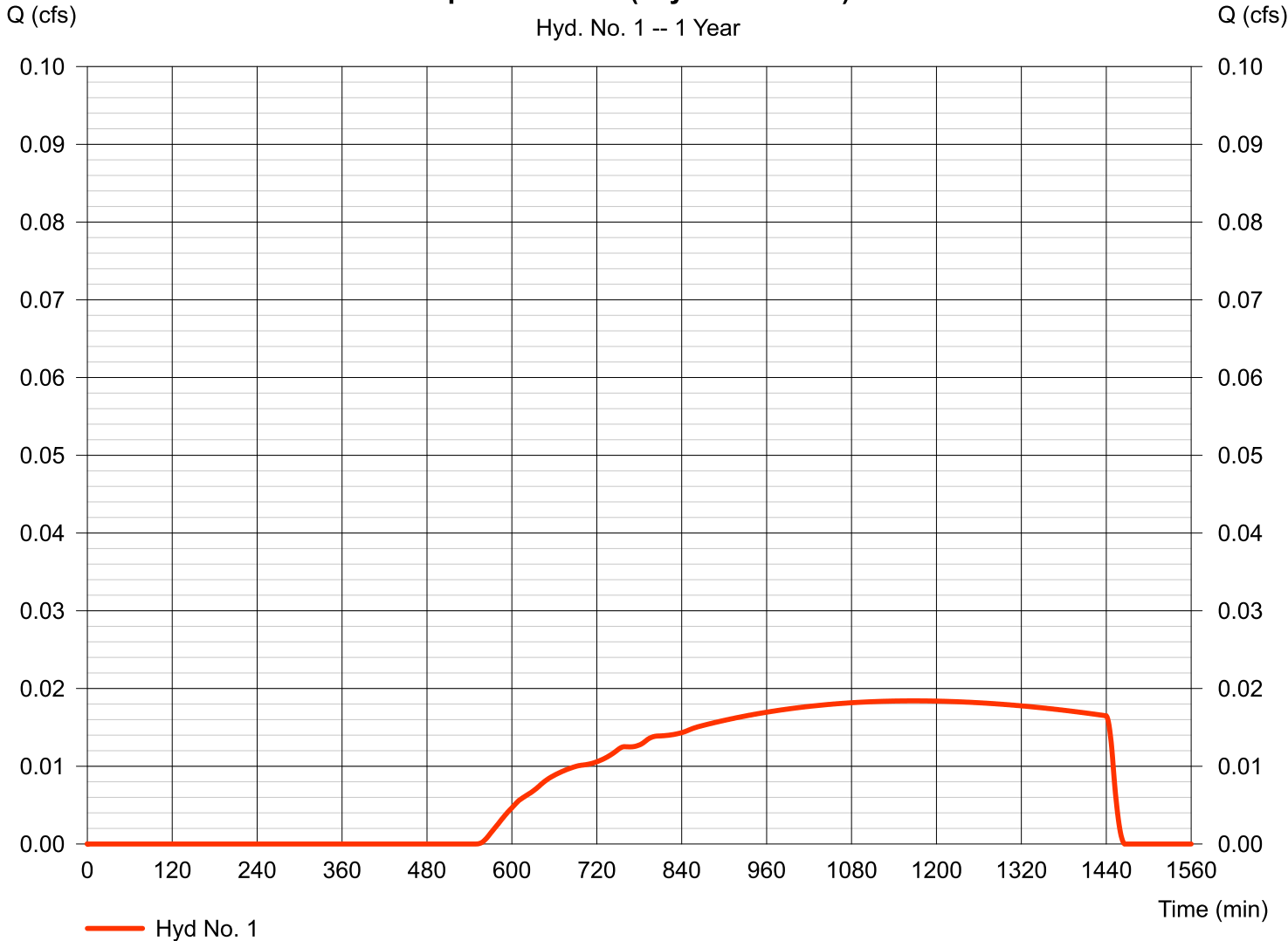
*1-yr is model for the 6 mo, 24 hr precip

Upstream PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.018 cfs
Storm frequency	= 1 yrs	Time to peak	= 1168 min
Time interval	= 1 min	Hyd. volume	= 798 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 1.40 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(2.170 x 73)] / 2.170

Upstream PRE (Crystal Creek 3)



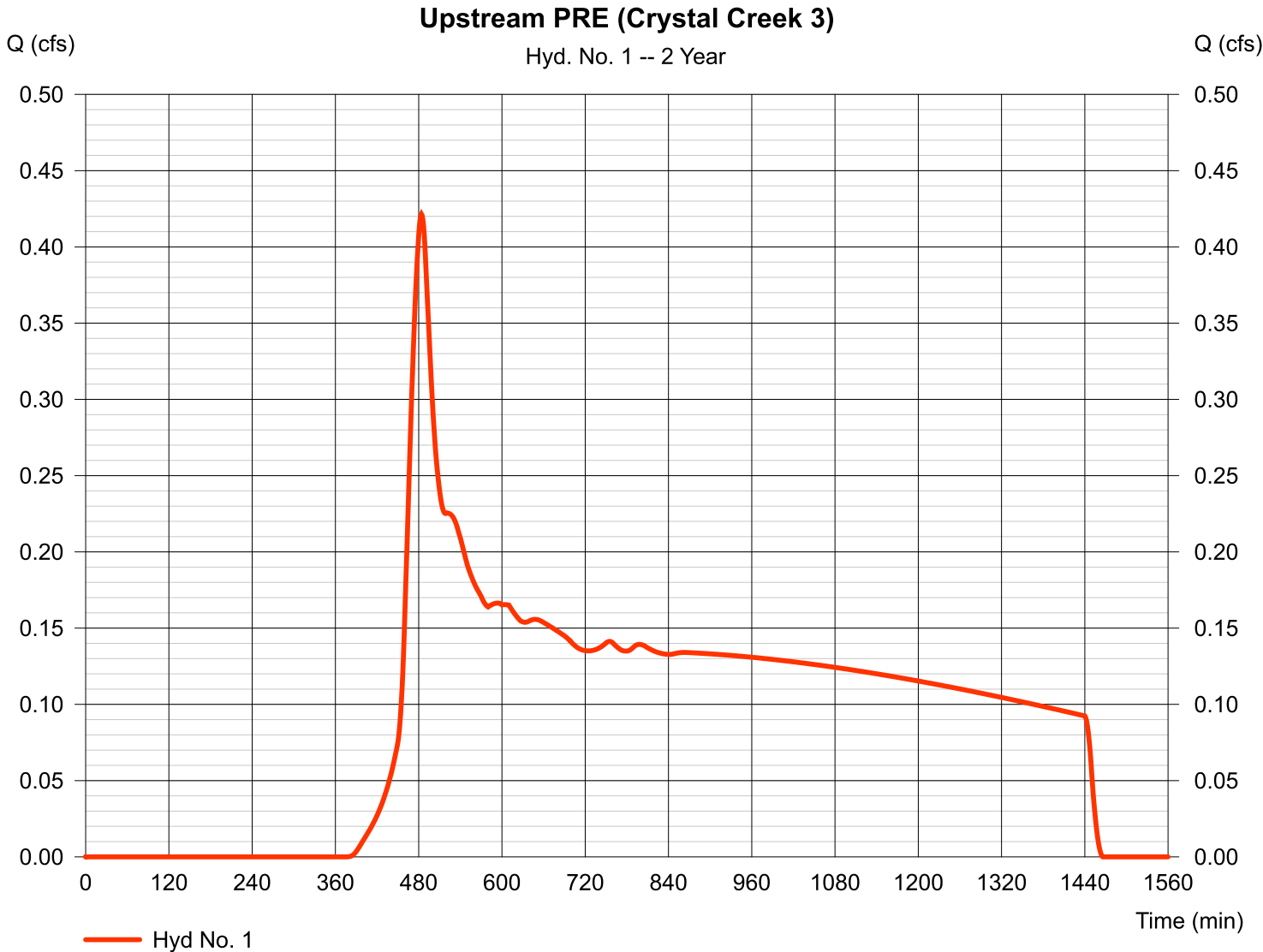
Hydrograph Report

Hyd. No. 1

Upstream PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.421 cfs
Storm frequency	= 2 yrs	Time to peak	= 484 min
Time interval	= 1 min	Hyd. volume	= 8,561 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 3.34 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(2.170 x 73)] / 2.170



Hydrograph Report

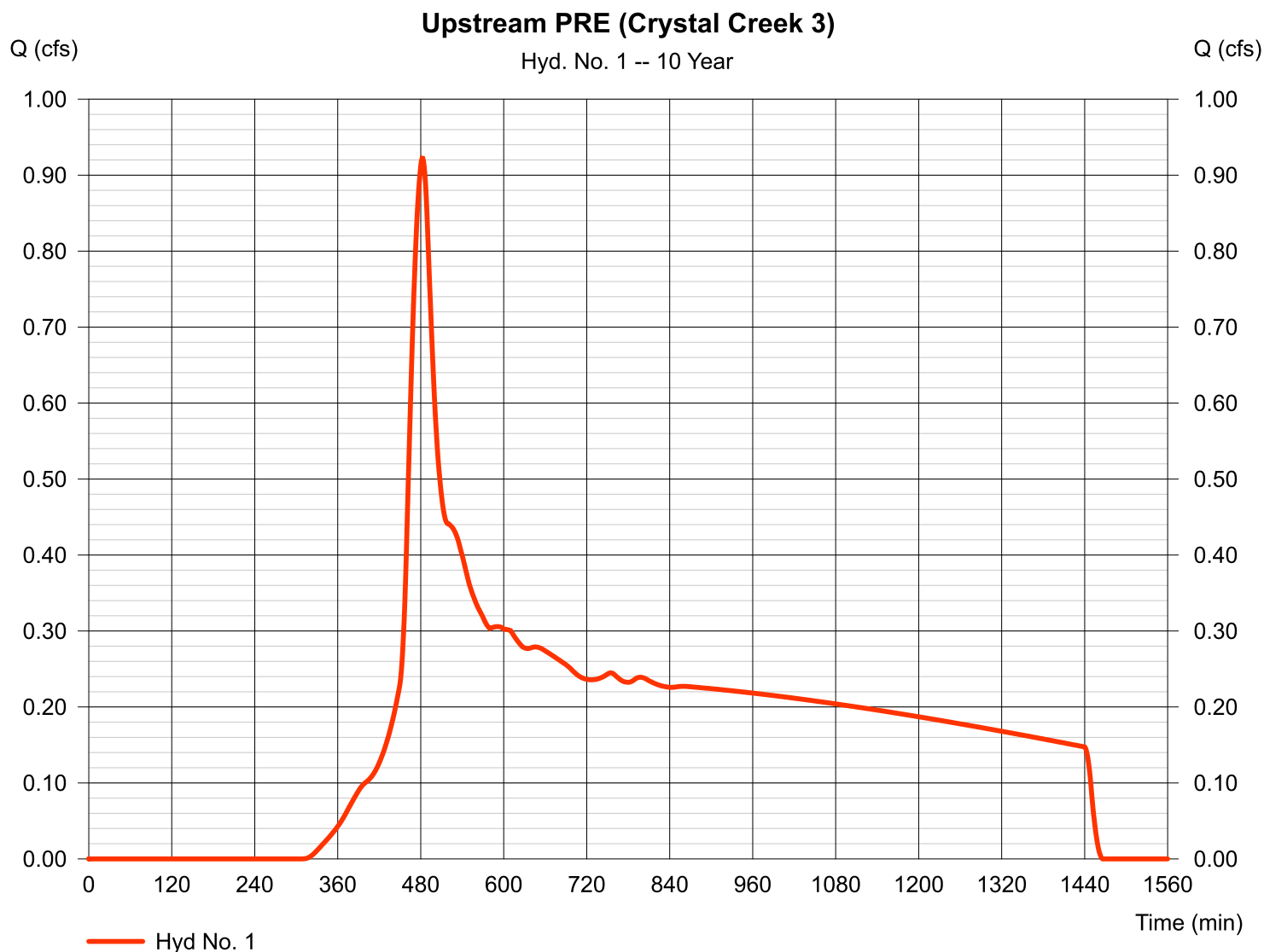
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Tuesday, 06 / 16 / 2020

Hyd. No. 1

Upstream PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.922 cfs
Storm frequency	= 10 yrs	Time to peak	= 482 min
Time interval	= 1 min	Hyd. volume	= 15,662 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 4.59 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(2.170 \times 73)] / 2.170$ 

Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Tuesday, 06 / 16 / 2020

Hyd. No. 1

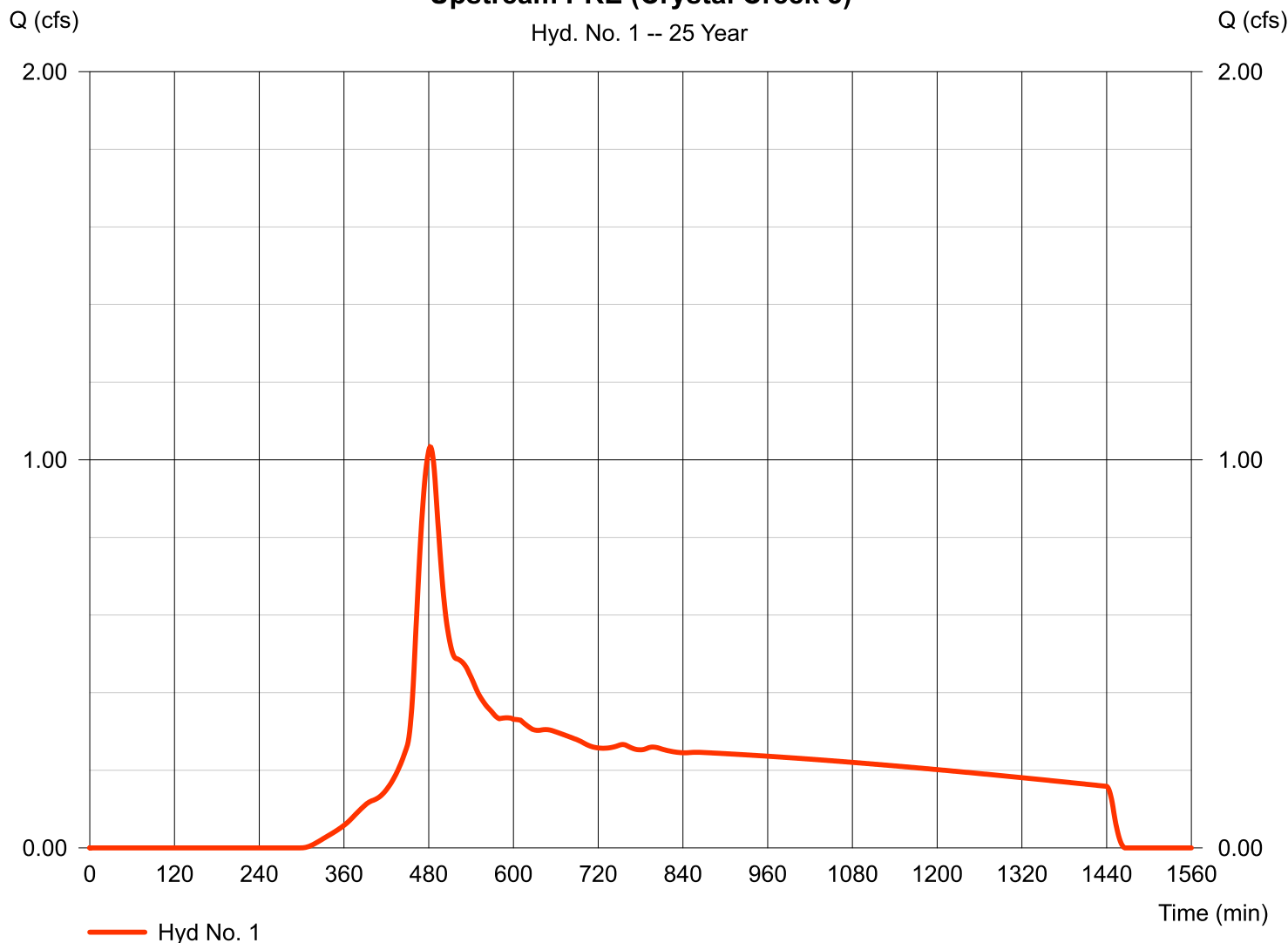
Upstream PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 1.033 cfs
Storm frequency	= 25 yrs	Time to peak	= 482 min
Time interval	= 1 min	Hyd. volume	= 17,193 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 4.84 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(2.170 x 73)] / 2.170

Upstream PRE (Crystal Creek 3)

Hyd. No. 1 -- 25 Year



Hydrograph Report

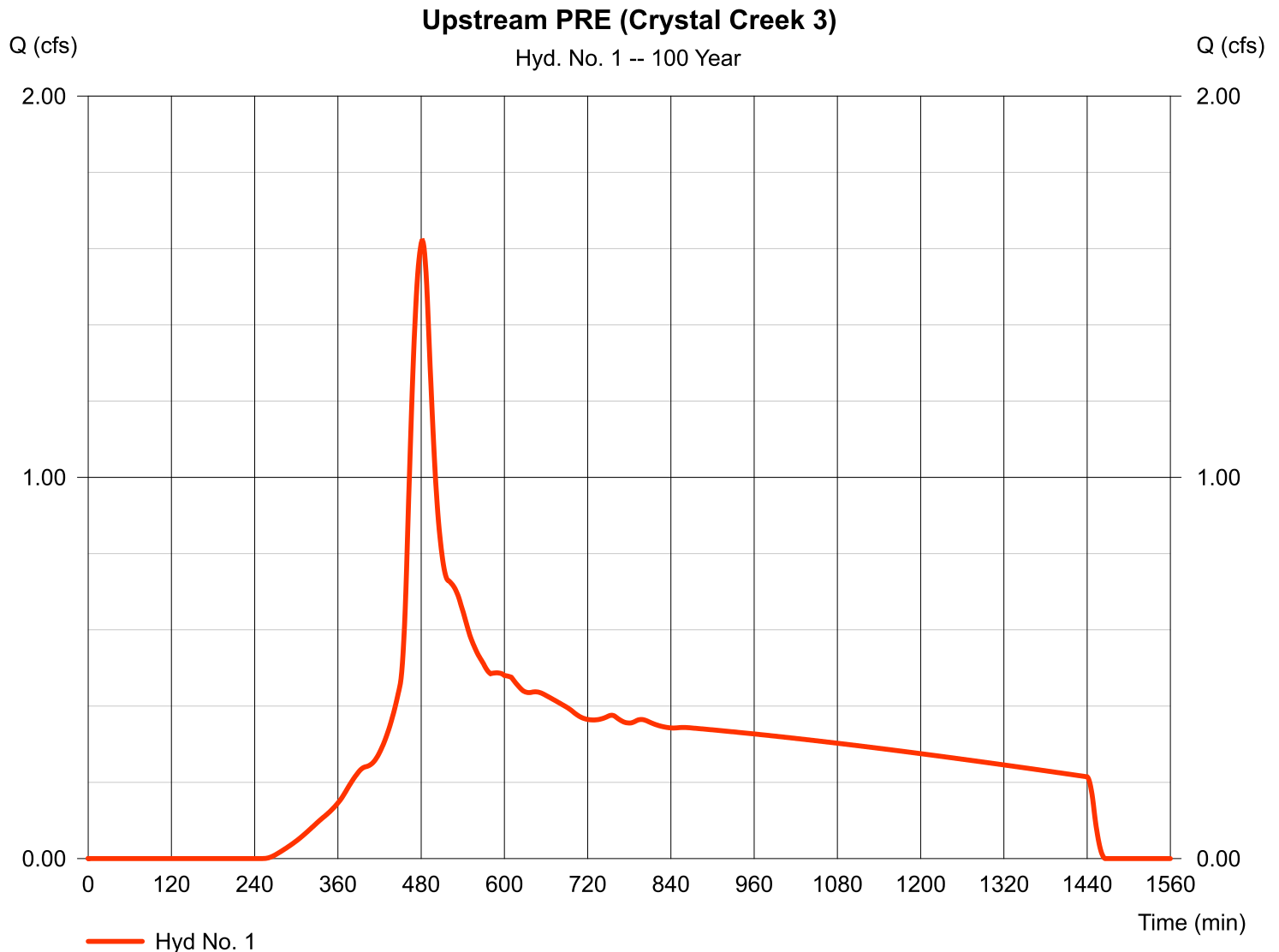
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Tuesday, 06 / 16 / 2020

Hyd. No. 1

Upstream PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 1.620 cfs
Storm frequency	= 100 yrs	Time to peak	= 482 min
Time interval	= 1 min	Hyd. volume	= 25,230 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 6.09 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(2.170 \times 73)] / 2.170$ 

TR55 Tc Worksheet

Hyd. No. 2

Onsite PRE (Crystal Creek 3)

<u>Description</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>Totals</u>
Sheet Flow				
Manning's n-value	= 0.350	0.011	0.011	
Flow length (ft)	= 200.0	0.0	0.0	
Two-year 24-hr precip. (in)	= 3.34	0.00	0.00	
Land slope (%)	= 18.00	0.00	0.00	
Travel Time (min)	= 13.66	+ 0.00	+ 0.00	= 13.66
Shallow Concentrated Flow				
Flow length (ft)	= 110.00	0.00	0.00	
Watercourse slope (%)	= 18.00	0.00	0.00	
Surface description	= Unpaved	Paved	Paved	
Average velocity (ft/s)	=6.85	0.00	0.00	
Travel Time (min)	= 0.27	+ 0.00	+ 0.00	= 0.27
Channel Flow				
X sectional flow area (sqft)	= 0.00	0.00	0.00	
Wetted perimeter (ft)	= 0.00	0.00	0.00	
Channel slope (%)	= 0.00	0.00	0.00	
Manning's n-value	= 0.015	0.015	0.015	
Velocity (ft/s)	=0.00	0.00	0.00	
Flow length (ft)	({0})0.0	0.0	0.0	
Travel Time (min)	= 0.00	+ 0.00	+ 0.00	= 0.00
Total Travel Time, Tc				13.90 min

Hydrograph Report

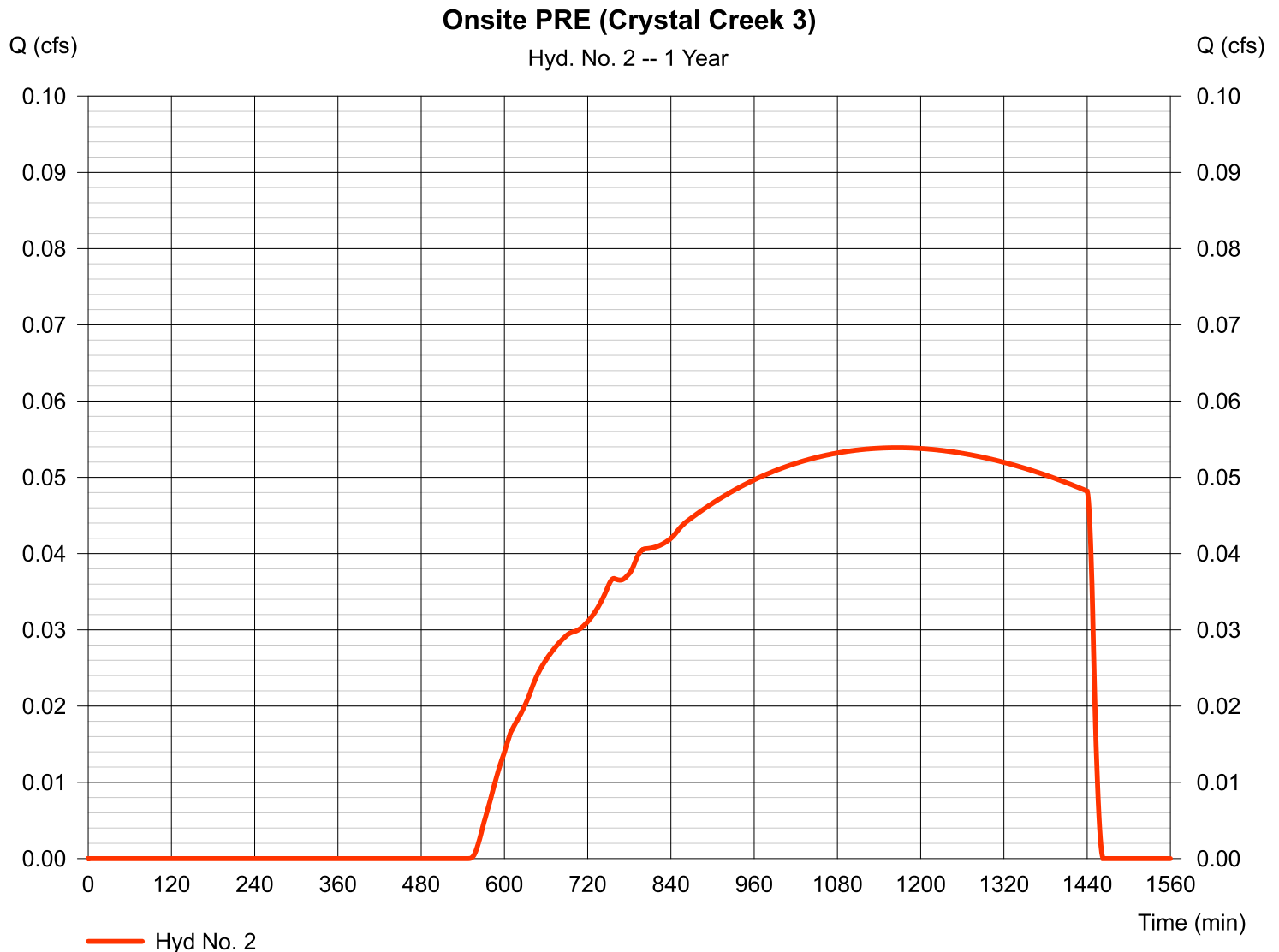
Hyd. No. 2

*1-yr is model for the 6 mo, 24 hr precip

Onsite PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.054 cfs
Storm frequency	= 1 yrs	Time to peak	= 1167 min
Time interval	= 1 min	Hyd. volume	= 2,334 cuft
Drainage area	= 6.430 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 13.90 min
Total precip.	= 1.40 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(6.430 \times 73)] / 6.430$



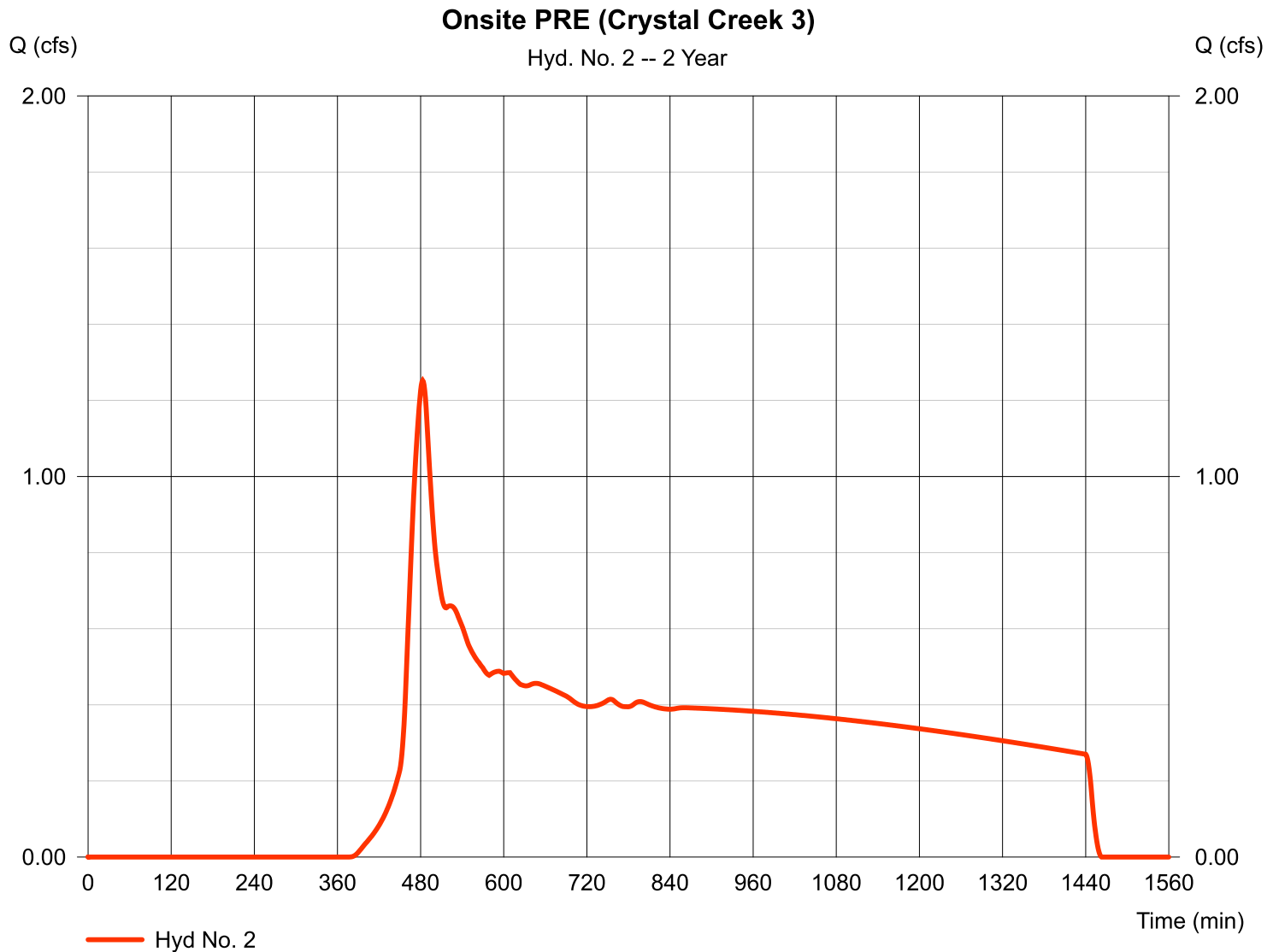
Hydrograph Report

Hyd. No. 2

Onsite PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 1.252 cfs
Storm frequency	= 2 yrs	Time to peak	= 483 min
Time interval	= 1 min	Hyd. volume	= 25,055 cuft
Drainage area	= 6.430 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 13.90 min
Total precip.	= 3.34 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(6.430 \times 73)] / 6.430$



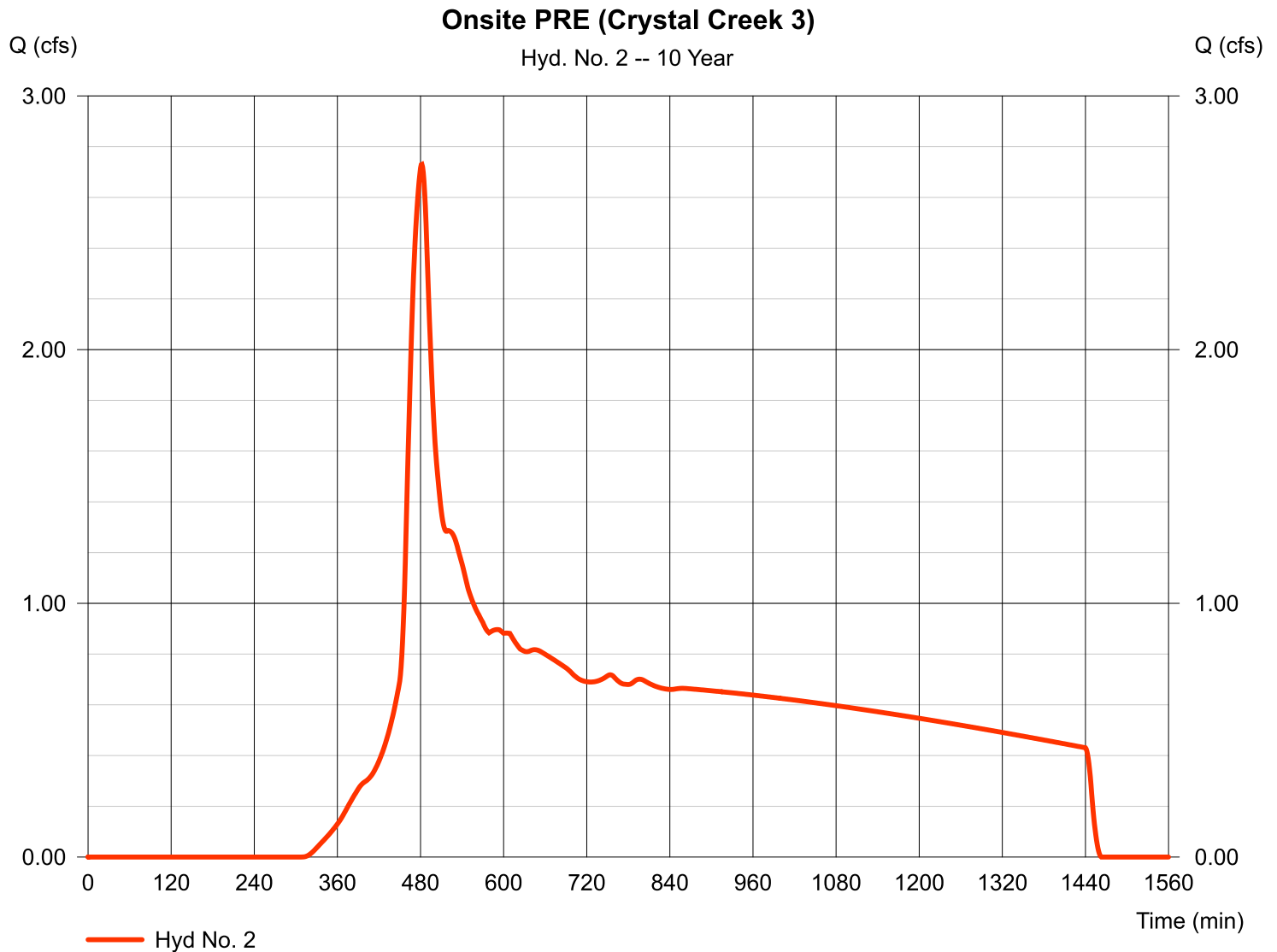
Hydrograph Report

Hyd. No. 2

Onsite PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 2.730 cfs
Storm frequency	= 10 yrs	Time to peak	= 482 min
Time interval	= 1 min	Hyd. volume	= 45,837 cuft
Drainage area	= 6.430 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 13.90 min
Total precip.	= 4.59 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(6.430 \times 73)] / 6.430$



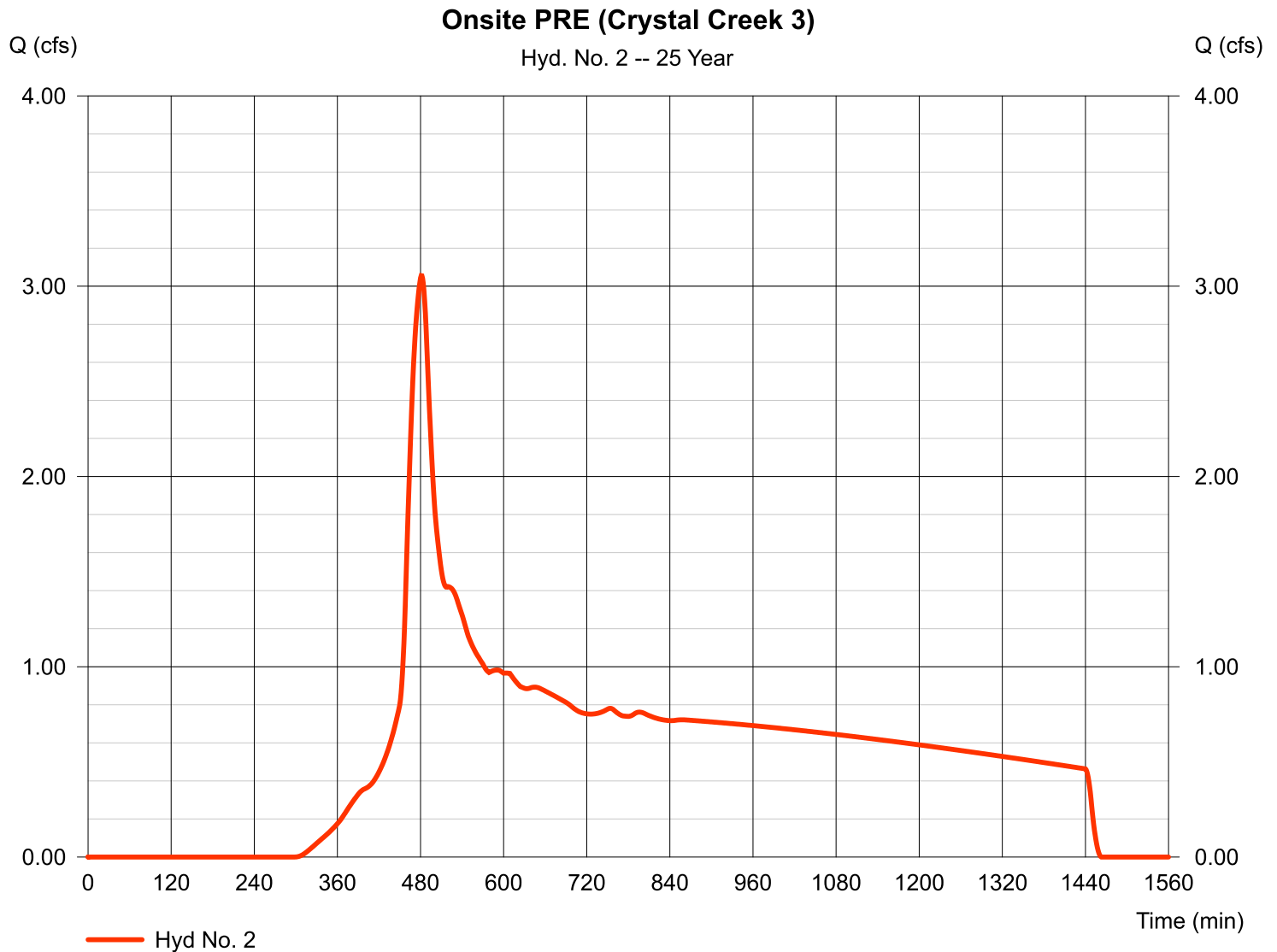
Hydrograph Report

Hyd. No. 2

Onsite PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 3.055 cfs
Storm frequency	= 25 yrs	Time to peak	= 481 min
Time interval	= 1 min	Hyd. volume	= 50,316 cuft
Drainage area	= 6.430 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 13.90 min
Total precip.	= 4.84 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(6.430 x 73)] / 6.430



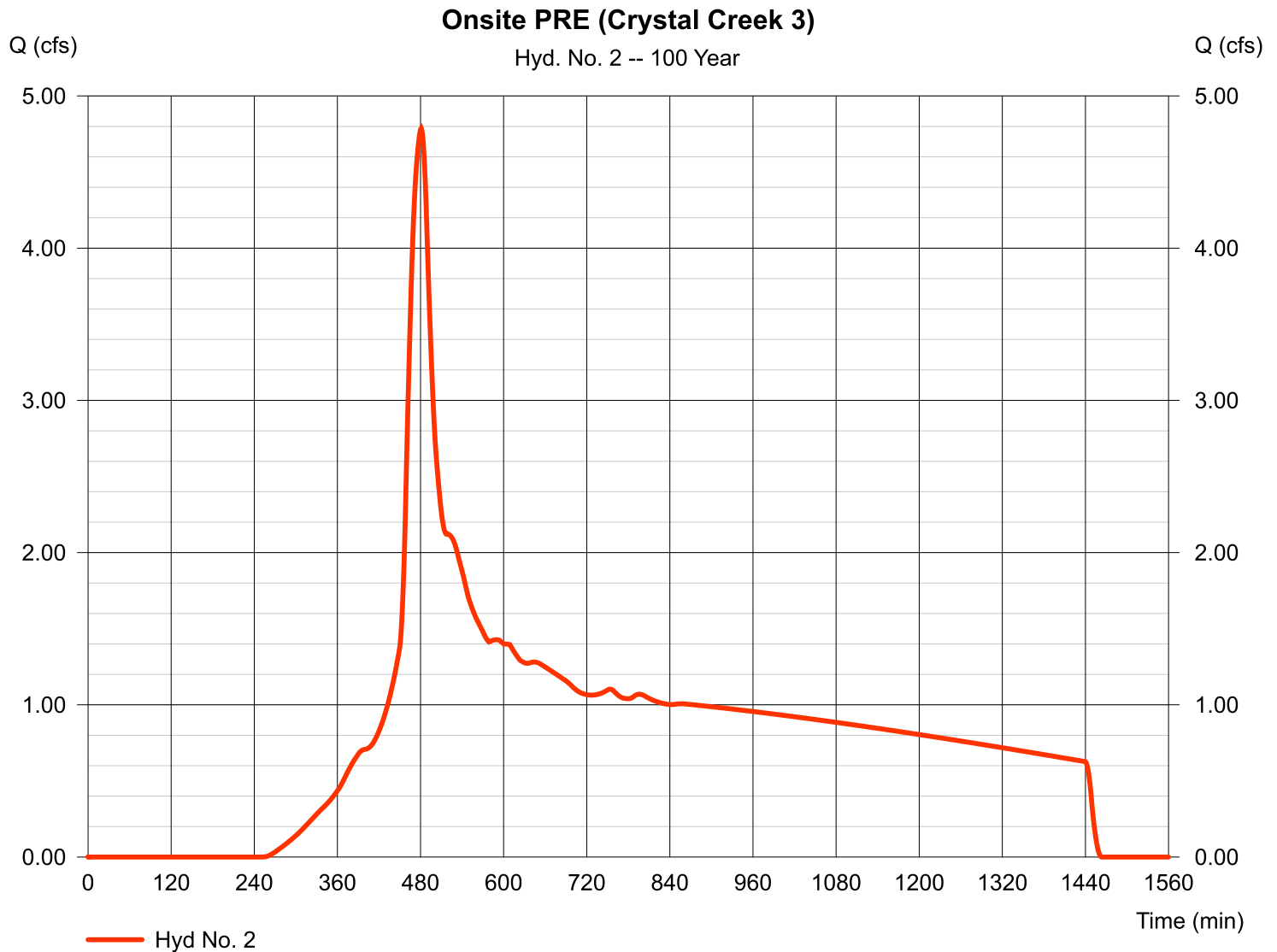
Hydrograph Report

Hyd. No. 2

Onsite PRE (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 4.787 cfs
Storm frequency	= 100 yrs	Time to peak	= 481 min
Time interval	= 1 min	Hyd. volume	= 73,837 cuft
Drainage area	= 6.430 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 13.90 min
Total precip.	= 6.09 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(6.430 x 73)] / 6.430



TR55 Tc Worksheet

Hyd. No. 3

Upstream Post (Crystal Creek 3)

<u>Description</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>Totals</u>
Sheet Flow				
Manning's n-value	= 0.350	0.011	0.011	
Flow length (ft)	= 209.0	0.0	0.0	
Two-year 24-hr precip. (in)	= 3.34	0.00	0.00	
Land slope (%)	= 12.00	0.00	0.00	
Travel Time (min)	= 16.64	+ 0.00	+ 0.00	= 16.64
Shallow Concentrated Flow				
Flow length (ft)	= 0.00	0.00	0.00	
Watercourse slope (%)	= 0.00	0.00	0.00	
Surface description	= Paved	Paved	Paved	
Average velocity (ft/s)	=0.00	0.00	0.00	
Travel Time (min)	= 0.00	+ 0.00	+ 0.00	= 0.00
Channel Flow				
X sectional flow area (sqft)	= 0.00	0.00	0.00	
Wetted perimeter (ft)	= 0.00	0.00	0.00	
Channel slope (%)	= 0.00	0.00	0.00	
Manning's n-value	= 0.015	0.015	0.015	
Velocity (ft/s)	=0.00	0.00	0.00	
Flow length (ft)	0.0	0.0	0.0	
Travel Time (min)	= 0.00	+ 0.00	+ 0.00	= 0.00
Total Travel Time, Tc				16.60 min

Hydrograph Report

Hyd. No. 3

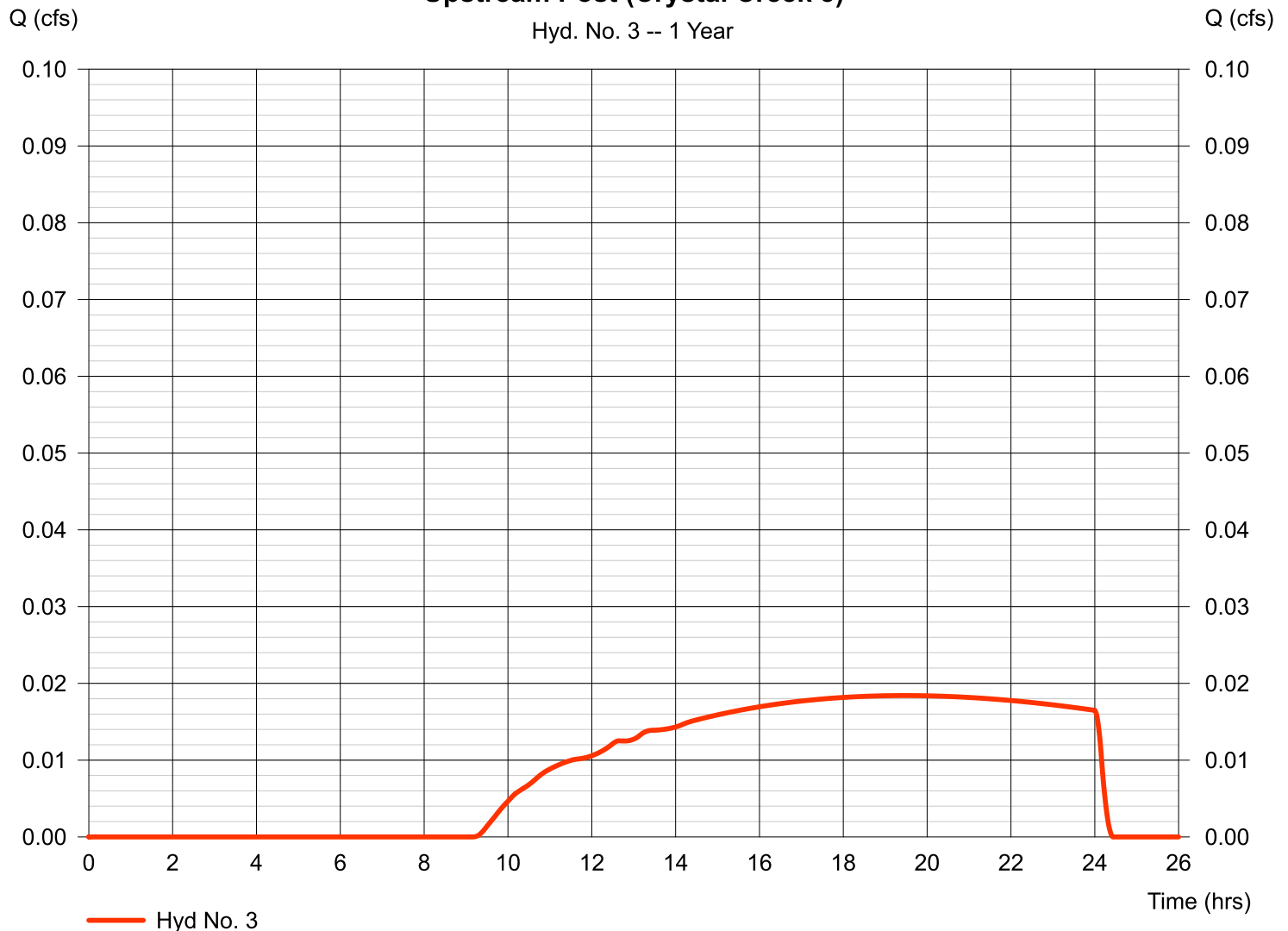
*1-yr is model for the 6 mo, 24 hr precip

Upstream Post (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.018 cfs
Storm frequency	= 1 yrs	Time to peak	= 19.47 hrs
Time interval	= 1 min	Hyd. volume	= 798 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 1.0 %	Hydraulic length	= 1 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 1.40 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(2.170 \times 73)] / 2.170$

Upstream Post (Crystal Creek 3)



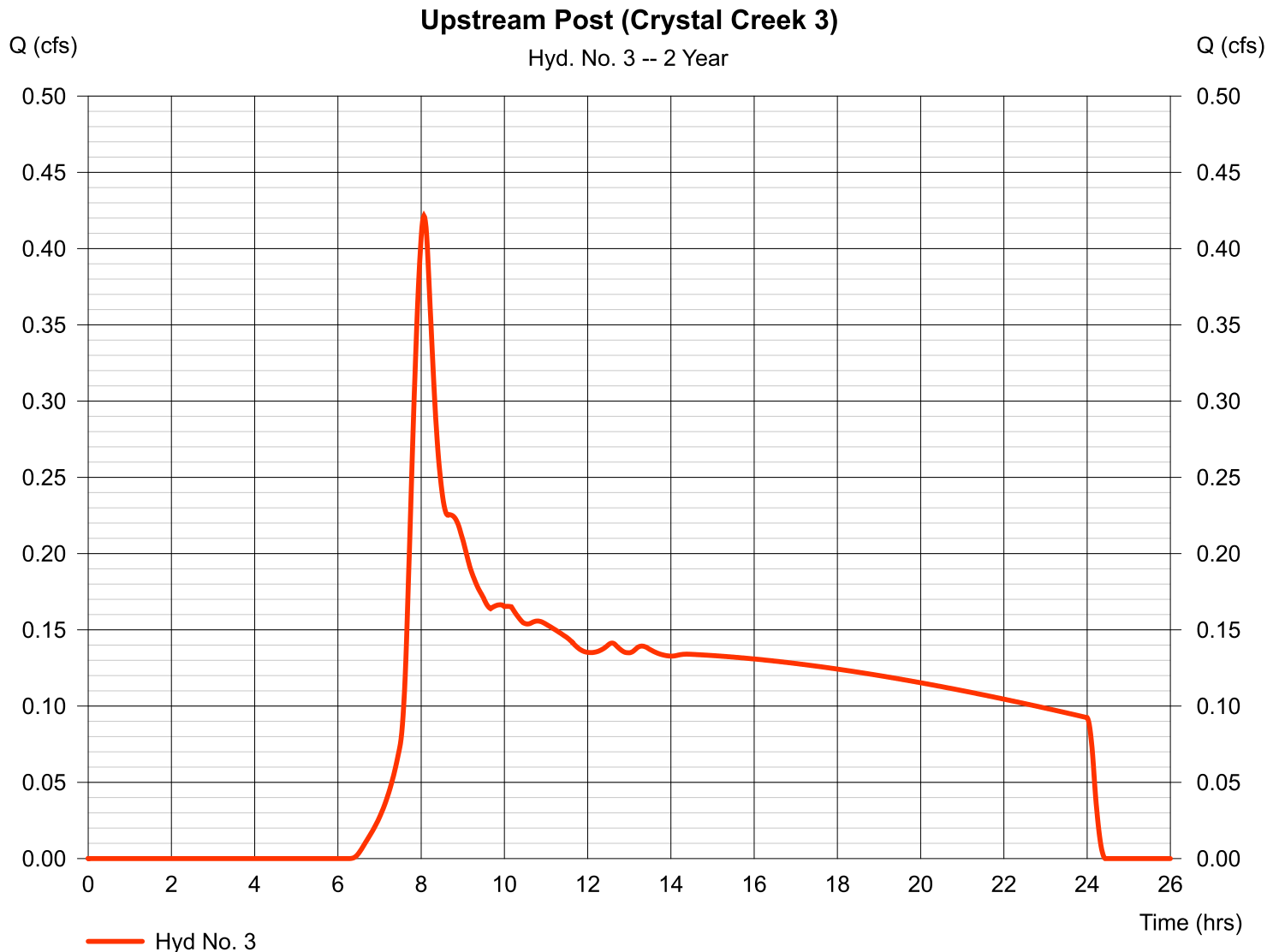
Hydrograph Report

Hyd. No. 3

Upstream Post (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.421 cfs
Storm frequency	= 2 yrs	Time to peak	= 8.07 hrs
Time interval	= 1 min	Hyd. volume	= 8,561 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 1.0 %	Hydraulic length	= 1 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 3.34 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(2.170 \times 73)] / 2.170$



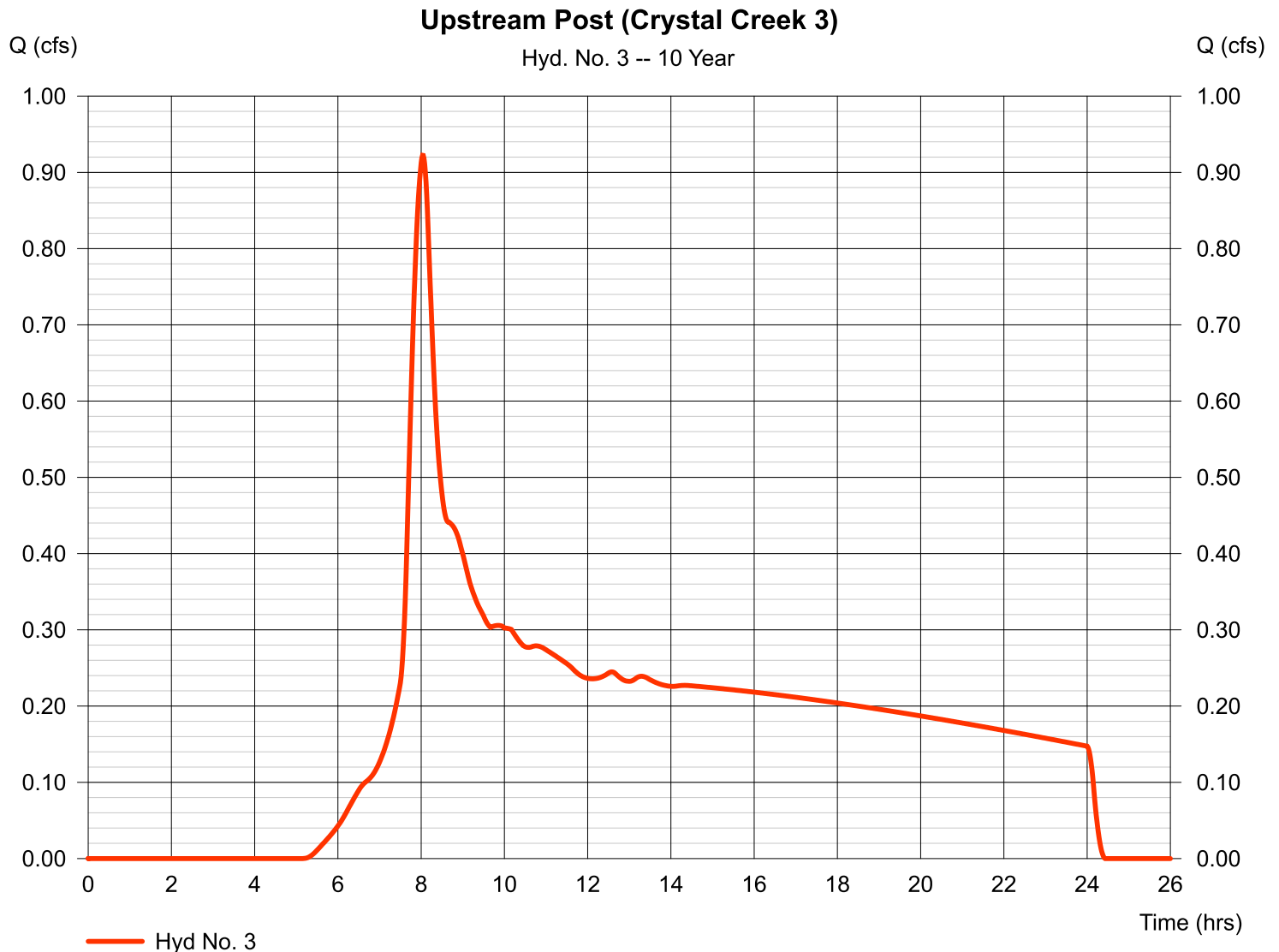
Hydrograph Report

Hyd. No. 3

Upstream Post (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.922 cfs
Storm frequency	= 10 yrs	Time to peak	= 8.03 hrs
Time interval	= 1 min	Hyd. volume	= 15,662 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 1.0 %	Hydraulic length	= 1 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 4.59 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(2.170 \times 73)] / 2.170$



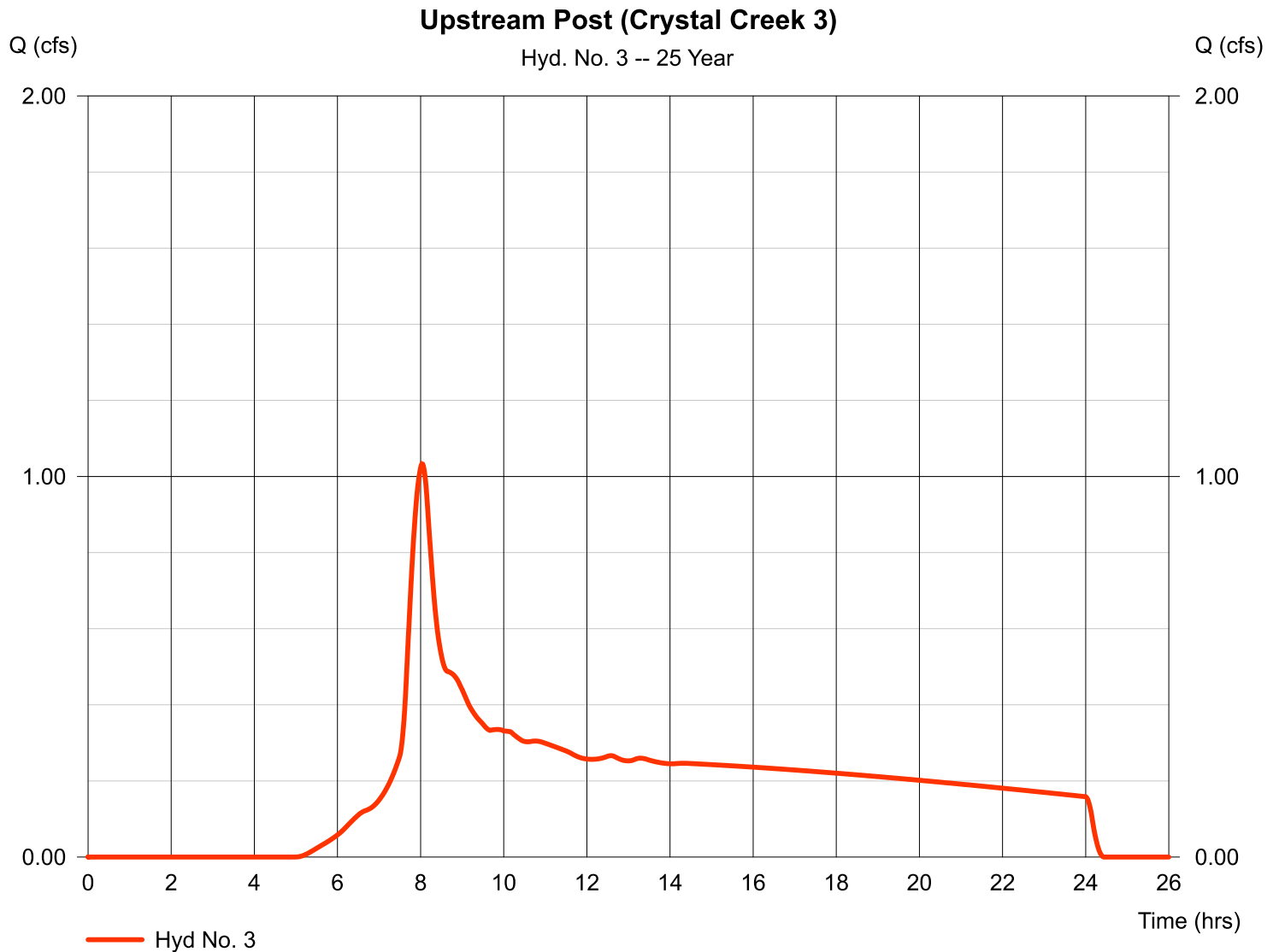
Hydrograph Report

Hyd. No. 3

Upstream Post (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 1.033 cfs
Storm frequency	= 25 yrs	Time to peak	= 8.03 hrs
Time interval	= 1 min	Hyd. volume	= 17,193 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 1.0 %	Hydraulic length	= 1 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 4.84 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(2.170 x 73)] / 2.170



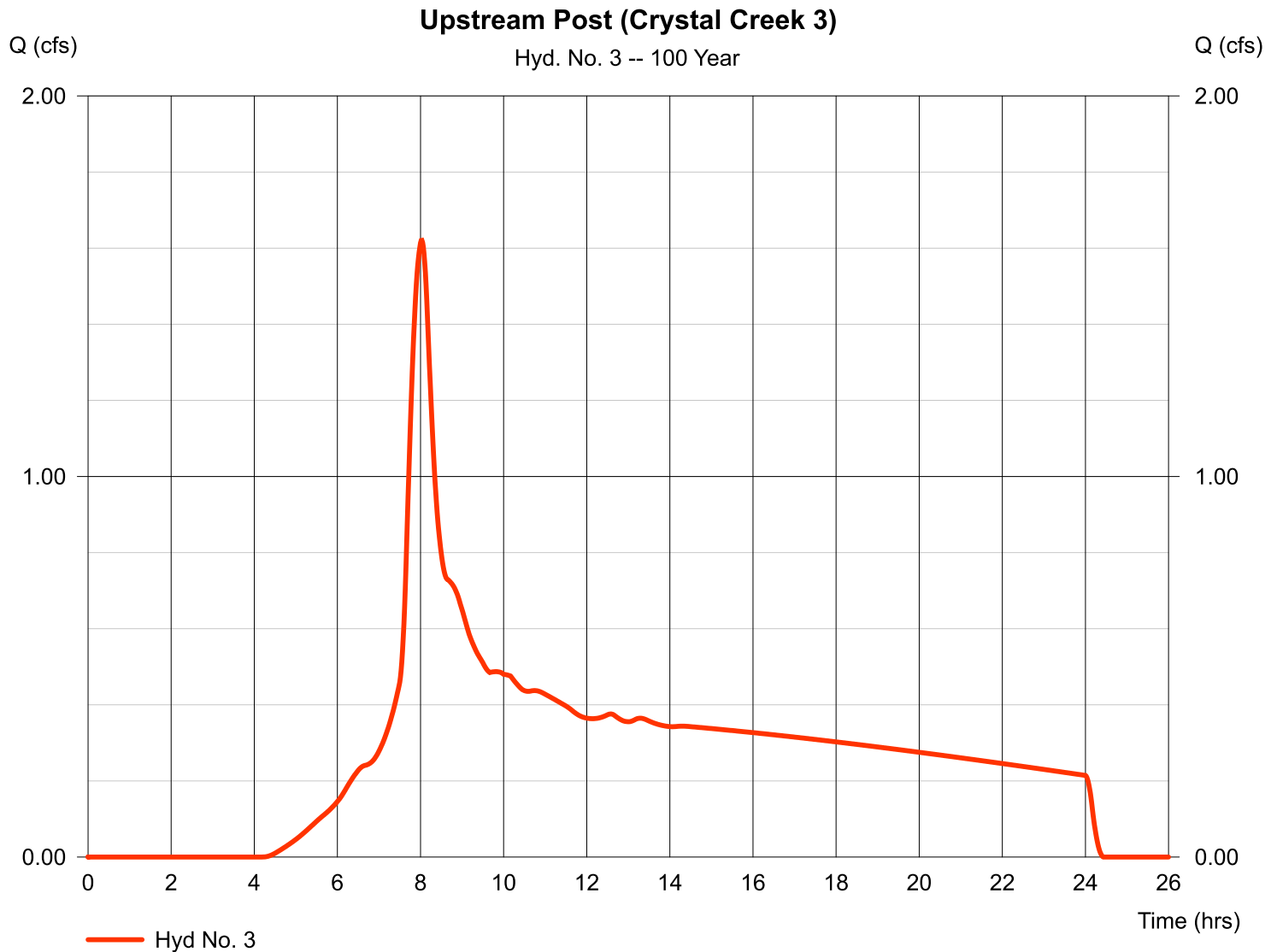
Hydrograph Report

Hyd. No. 3

Upstream Post (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 1.620 cfs
Storm frequency	= 100 yrs	Time to peak	= 8.03 hrs
Time interval	= 1 min	Hyd. volume	= 25,230 cuft
Drainage area	= 2.170 ac	Curve number	= 73*
Basin Slope	= 1.0 %	Hydraulic length	= 1 ft
Tc method	= TR55	Time of conc. (Tc)	= 16.60 min
Total precip.	= 6.09 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(2.170 \times 73)] / 2.170$



TR55 Tc Worksheet

Hyd. No. 4

POST (Crystal Creek 3)

<u>Description</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>Totals</u>
Sheet Flow				
Manning's n-value	= 0.350	0.011	0.011	
Flow length (ft)	= 95.0	0.0	0.0	
Two-year 24-hr precip. (in)	= 3.34	0.00	0.00	
Land slope (%)	= 19.00	0.00	0.00	
Travel Time (min)	= 7.37	+ 0.00	+ 0.00	= 7.37
Shallow Concentrated Flow				
Flow length (ft)	= 40.00	6.00	0.00	
Watercourse slope (%)	= 2.00	33.00	0.00	
Surface description	= Paved	Unpaved	Paved	
Average velocity (ft/s)	=2.87	9.27	0.00	
Travel Time (min)	= 0.23	+ 0.01	+ 0.00	= 0.24
Channel Flow				
X sectional flow area (sqft)	= 11.25	0.08	0.00	
Wetted perimeter (ft)	= 12.48	0.52	0.00	
Channel slope (%)	= 4.00	12.00	0.00	
Manning's n-value	= 0.350	0.012	0.015	
Velocity (ft/s)	=0.79	12.27	0.00	
Flow length (ft)	357.0	223.0	0.0	
Travel Time (min)	= 7.49	+ 0.30	+ 0.00	= 7.79
Total Travel Time, Tc				15.40 min

Hydrograph Report

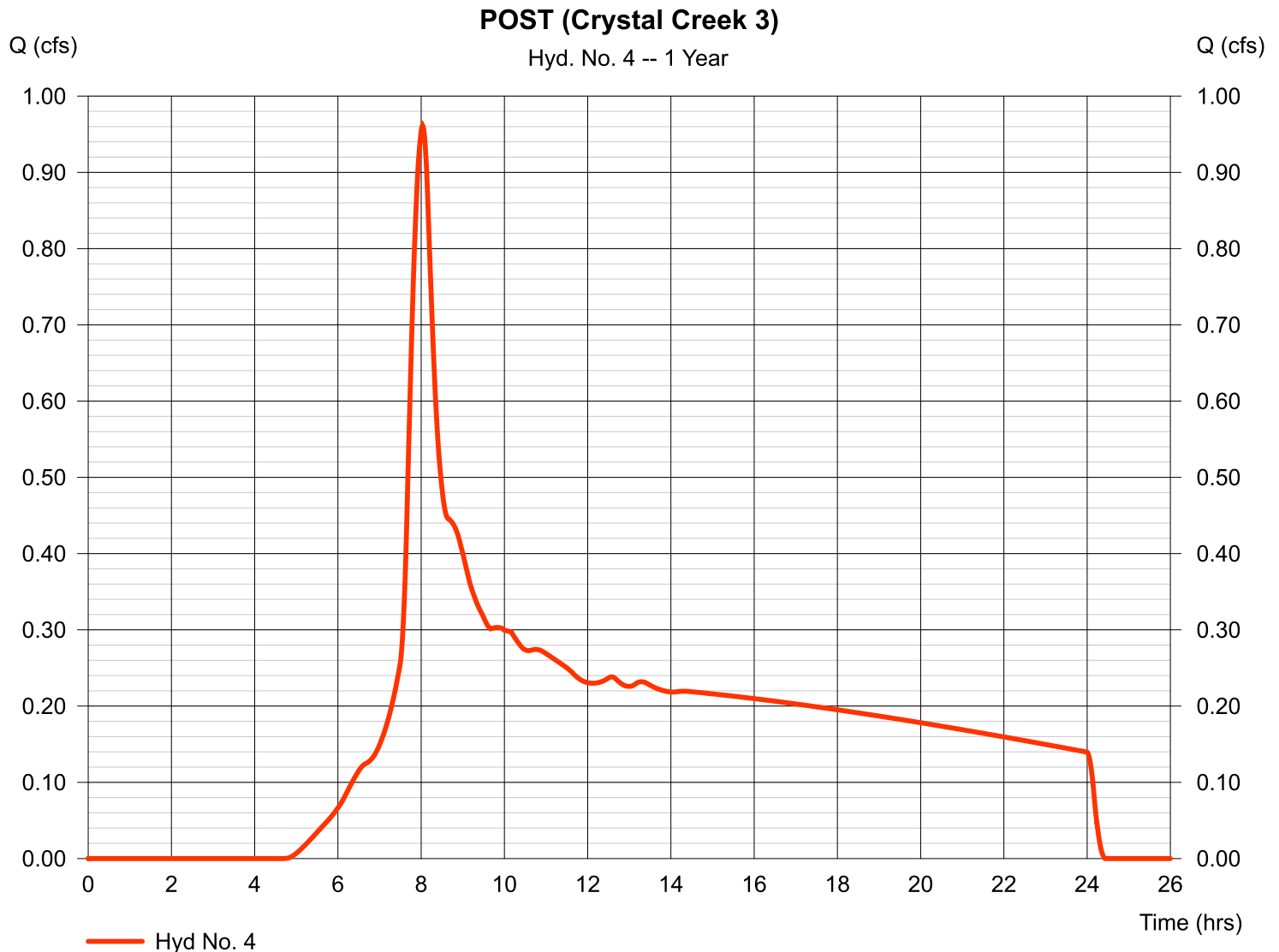
Hyd. No. 4

*1-yr is model for the 6 mo, 24 hr precip

POST (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 0.961 cfs
Storm frequency	= 1 yrs	Time to peak	= 8.03 hrs
Time interval	= 1 min	Hyd. volume	= 15,588 cuft
Drainage area	= 6.430 ac	Curve number	= 91*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.40 min
Total precip.	= 1.40 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(4.180 x 98) + (2.250 x 79)] / 6.430



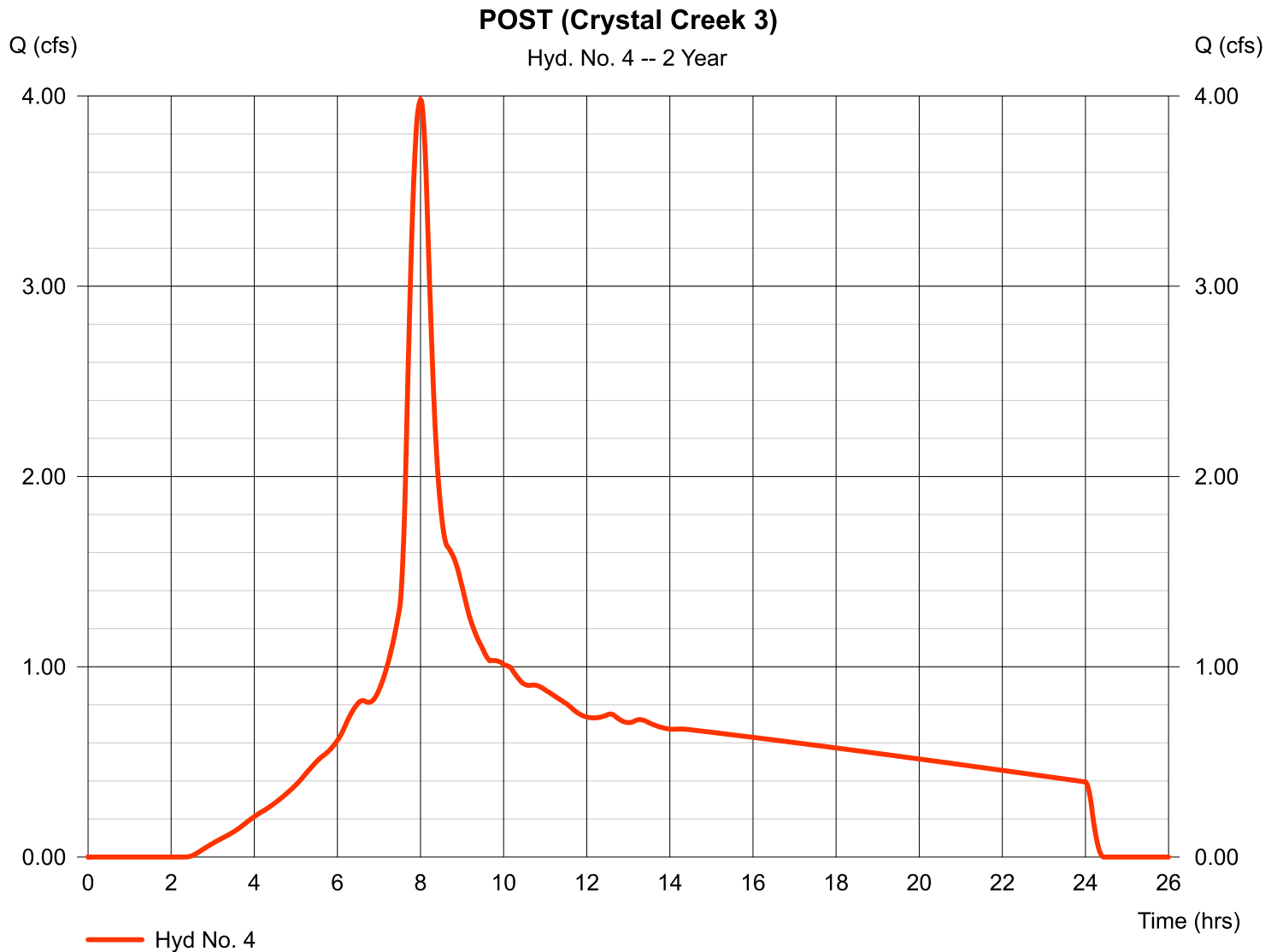
Hydrograph Report

Hyd. No. 4

POST (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 3.981 cfs
Storm frequency	= 2 yrs	Time to peak	= 8.00 hrs
Time interval	= 1 min	Hyd. volume	= 56,481 cuft
Drainage area	= 6.430 ac	Curve number	= 91*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.40 min
Total precip.	= 3.34 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(4.180 x 98) + (2.250 x 79)] / 6.430



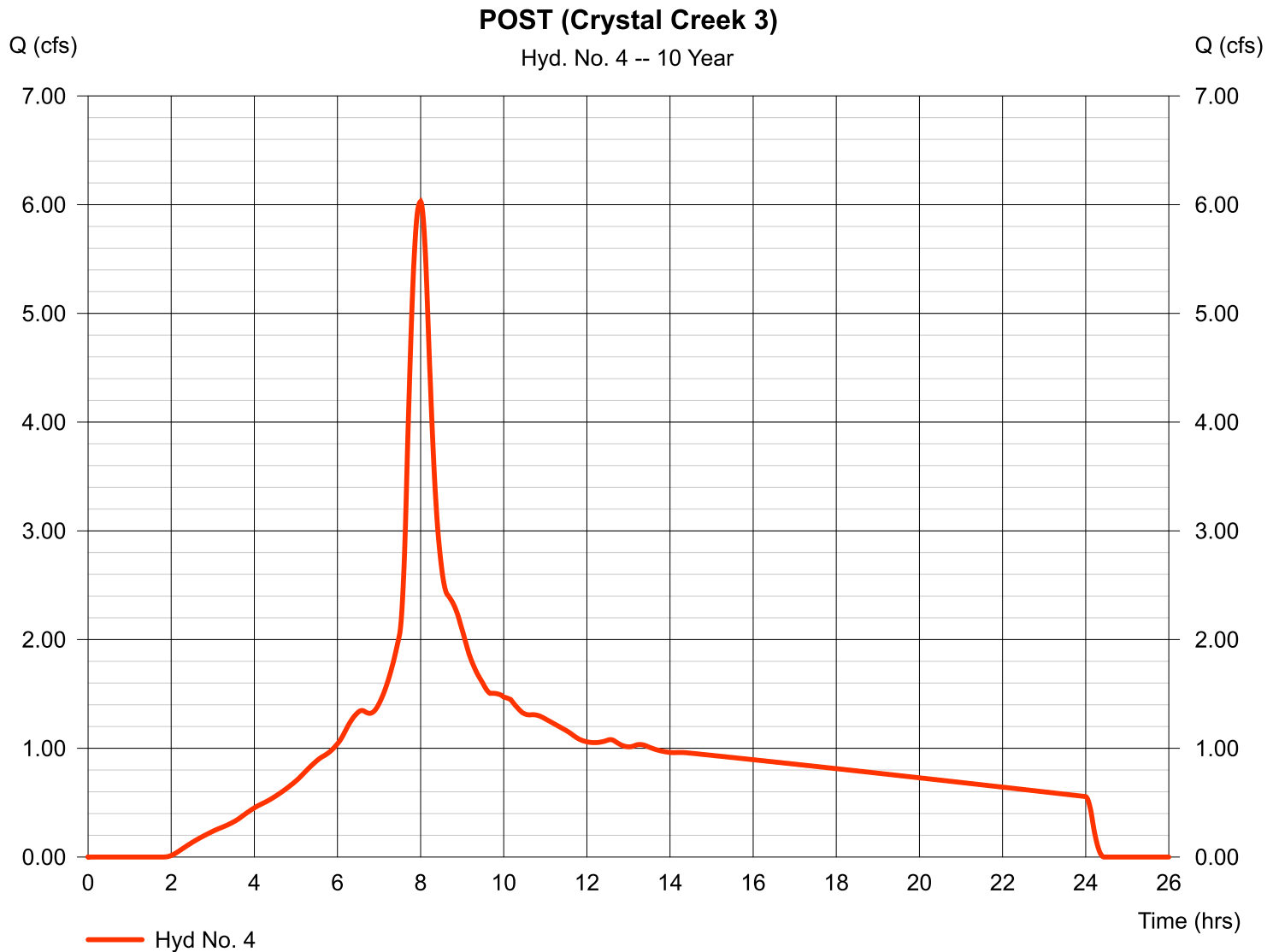
Hydrograph Report

Hyd. No. 4

POST (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 6.030 cfs
Storm frequency	= 10 yrs	Time to peak	= 8.00 hrs
Time interval	= 1 min	Hyd. volume	= 84,722 cuft
Drainage area	= 6.430 ac	Curve number	= 91*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.40 min
Total precip.	= 4.59 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(4.180 x 98) + (2.250 x 79)] / 6.430



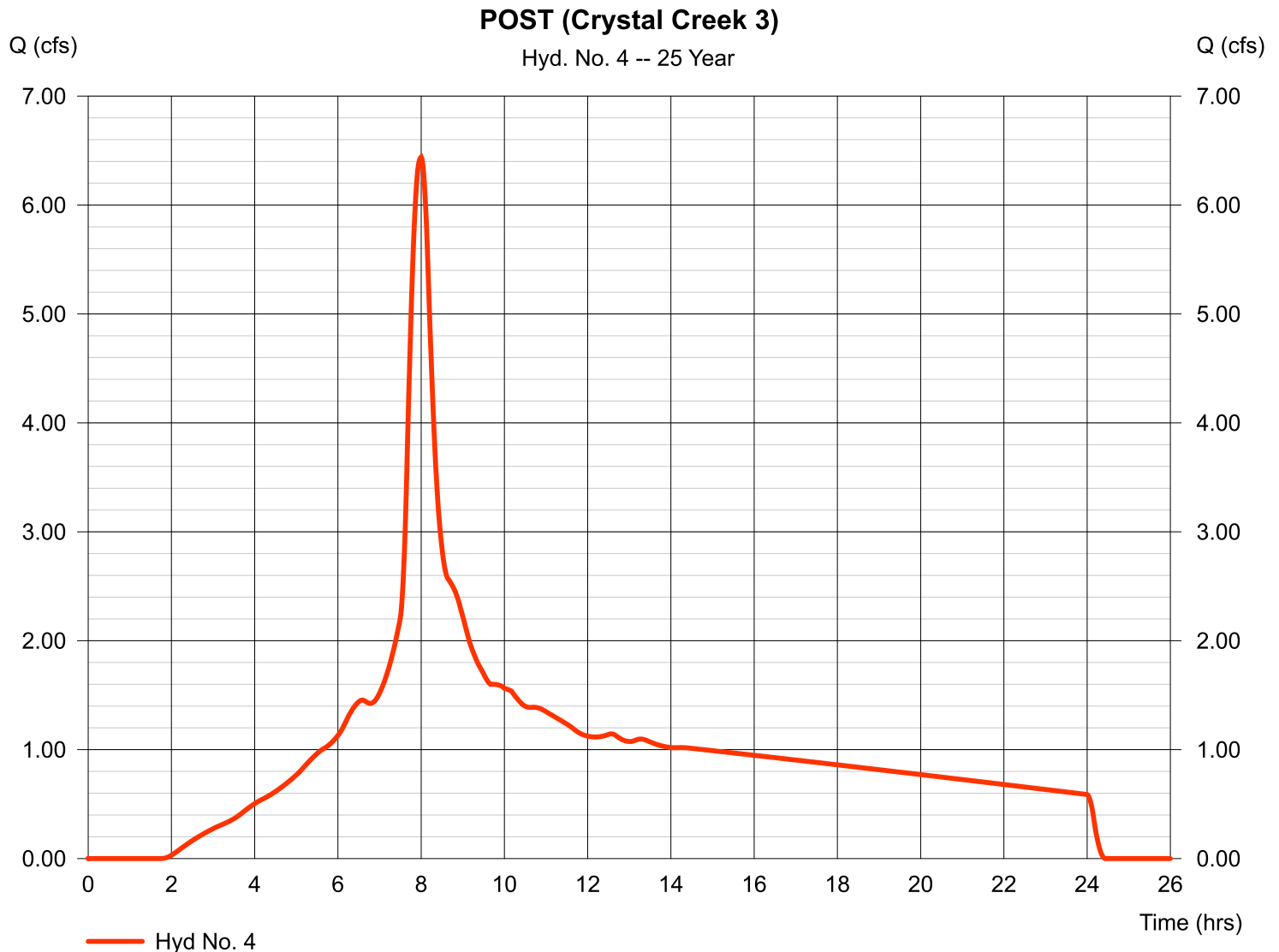
Hydrograph Report

Hyd. No. 4

POST (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 6.440 cfs
Storm frequency	= 25 yrs	Time to peak	= 8.00 hrs
Time interval	= 1 min	Hyd. volume	= 90,440 cuft
Drainage area	= 6.430 ac	Curve number	= 91*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.40 min
Total precip.	= 4.84 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = $[(4.180 \times 98) + (2.250 \times 79)] / 6.430$



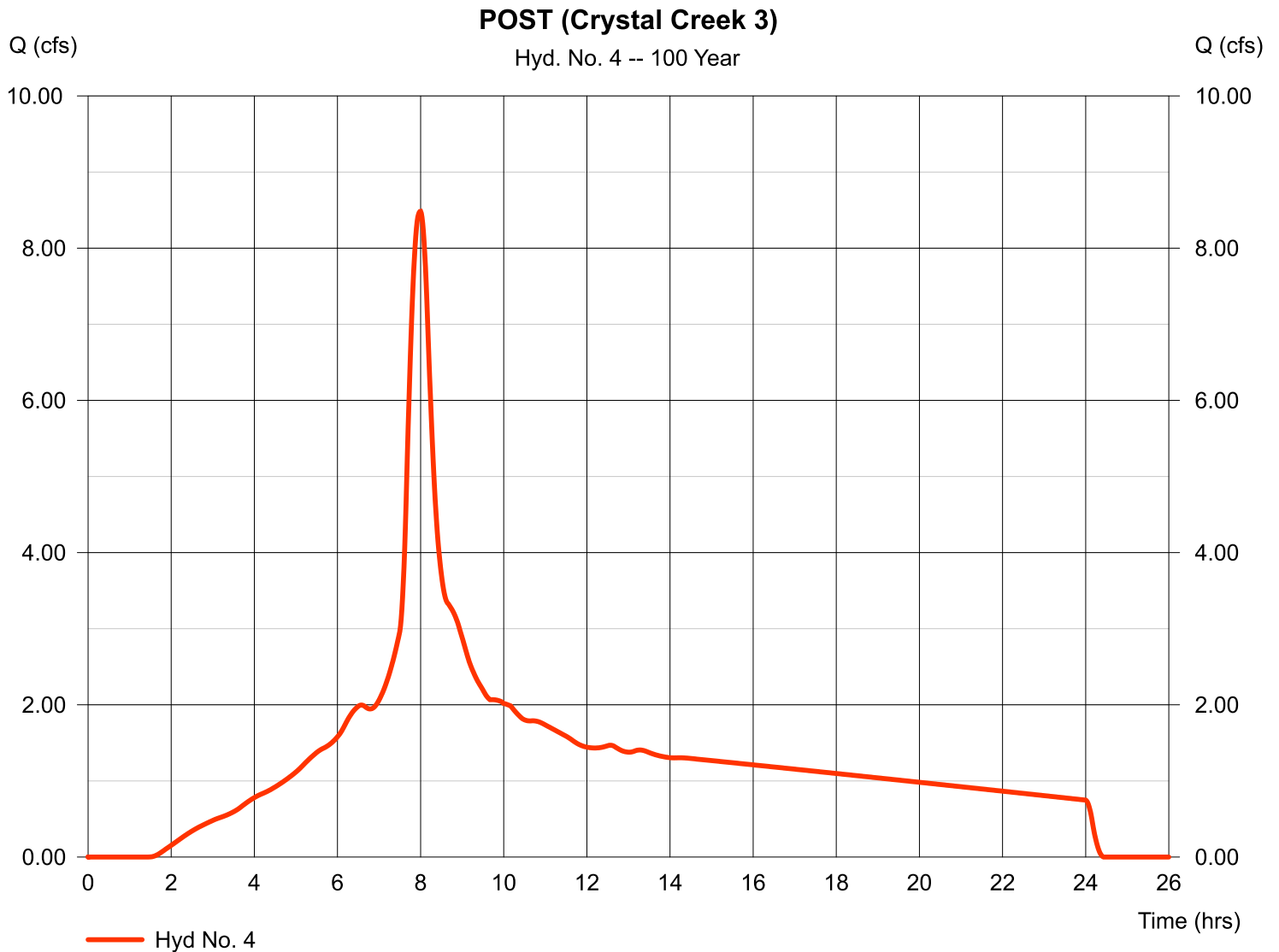
Hydrograph Report

Hyd. No. 4

POST (Crystal Creek 3)

Hydrograph type	= SCS Runoff	Peak discharge	= 8.483 cfs
Storm frequency	= 100 yrs	Time to peak	= 8.00 hrs
Time interval	= 1 min	Hyd. volume	= 119,235 cuft
Drainage area	= 6.430 ac	Curve number	= 91*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 15.40 min
Total precip.	= 6.09 in	Distribution	= Type IA
Storm duration	= 24 hrs	Shape factor	= 484

* Composite (Area/CN) = [(4.180 x 98) + (2.250 x 79)] / 6.430



Pond Report

Pond No. 3 - Pond B7-A

Pond Data

Contours -User-defined contour areas. Average end area method used for volume calculation. Beginning Elevation = 100.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	100.00	806	0	0
1.00	101.00	1,596	1,201	1,201
2.00	102.00	2,596	2,096	3,297
3.00	103.00	3,779	3,188	6,485
4.00	104.00	5,096	4,438	10,922
5.00	105.00	6,535	5,816	16,738
6.00	106.00	8,097	7,316	24,054
6.50	106.50	8,846	4,236	28,289
8.00	108.00	11,427	15,205	43,494

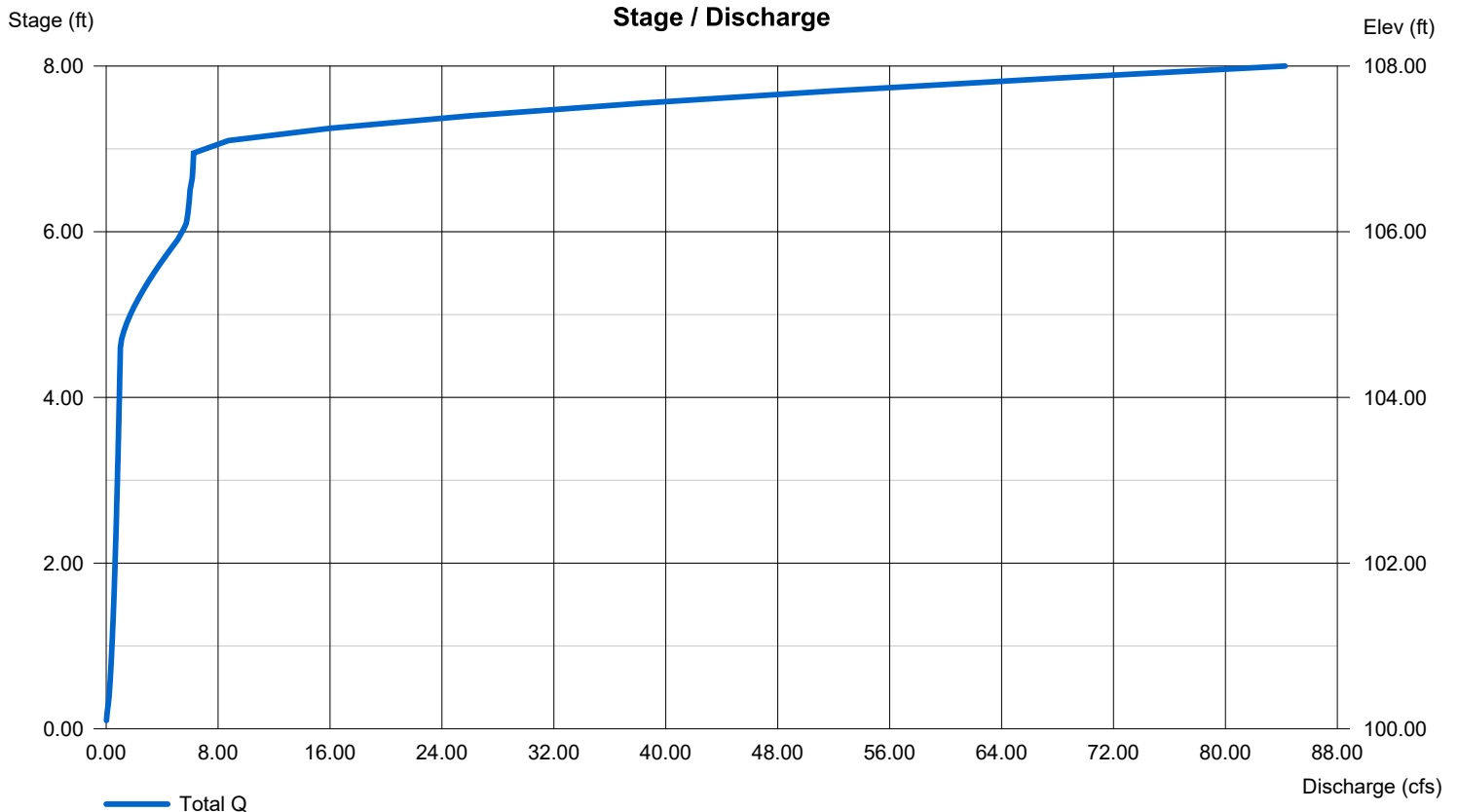
Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 12.00	4.38	Inactive	0.00
Span (in)	= 12.00	4.38	0.00	0.00
No. Barrels	= 1	1	1	0
Invert El. (ft)	= 100.00	100.00	0.00	0.00
Length (ft)	= 405.00	0.00	0.00	0.00
Slope (%)	= 1.95	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	Yes	Yes	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 12.57	0.85	30.00	Inactive
Crest El. (ft)	= 106.50	104.61	107.00	110.87
Weir Coeff.	= 3.33	3.33	2.60	3.33
Weir Type	= 1	Rect	Broad	Rect
Multi-Stage	= Yes	Yes	No	Yes
Exfil.(in/hr)	= 0.000 (by Contour)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydrograph Report

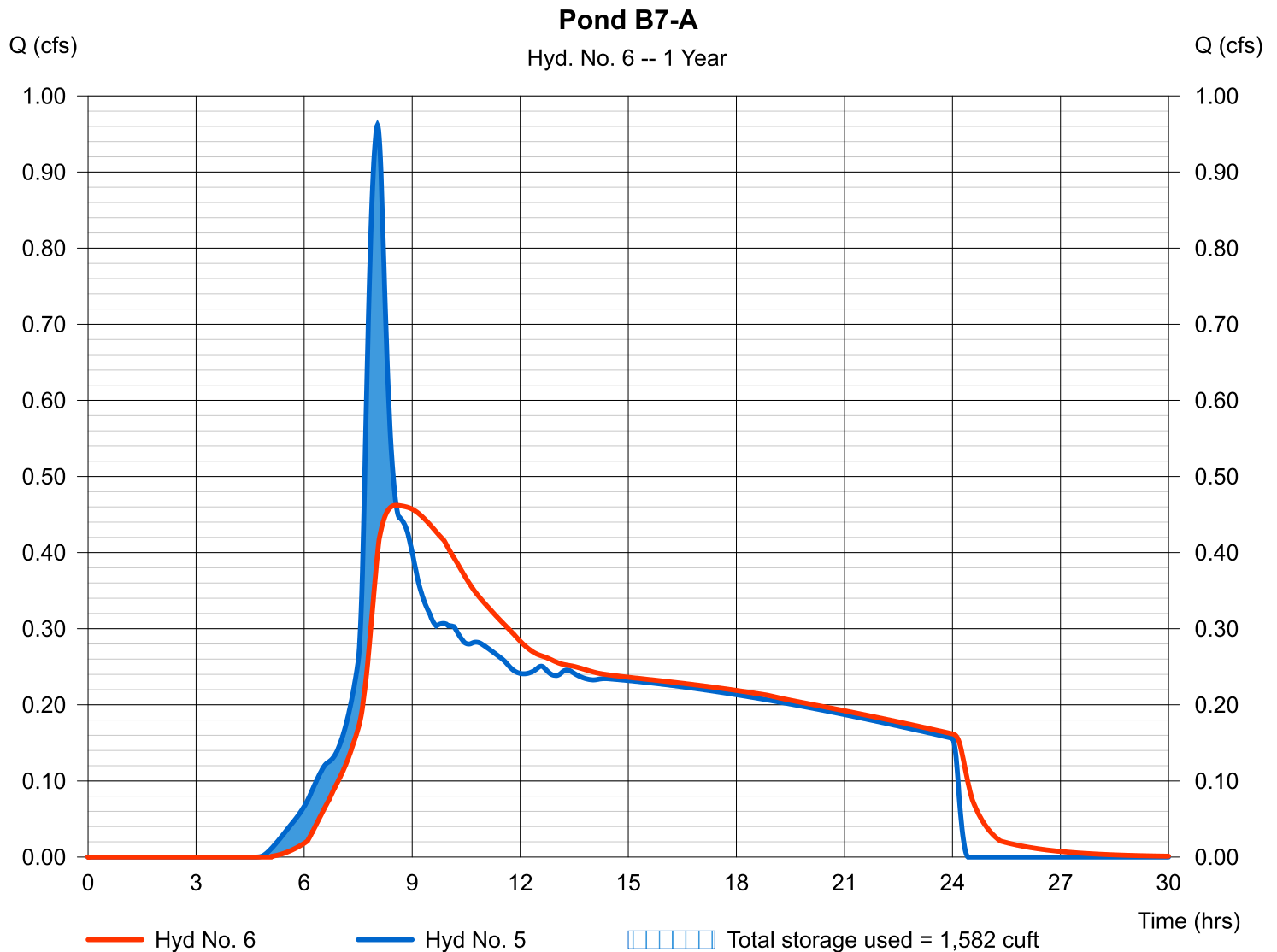
Hyd. No. 6

*1-yr is model for the 6 mo, 24 hr precip

Pond B7-A

Hydrograph type	= Reservoir	Peak discharge	= 0.462 cfs
Storm frequency	= 1 yrs	Time to peak	= 8.55 hrs
Time interval	= 1 min	Hyd. volume	= 16,380 cuft
Inflow hyd. No.	= 5 - Upst.+Onsite (CC3)	Max. Elevation	= 101.18 ft
Reservoir name	= Pond B7-A	Max. Storage	= 1,582 cuft

Storage Indication method used.



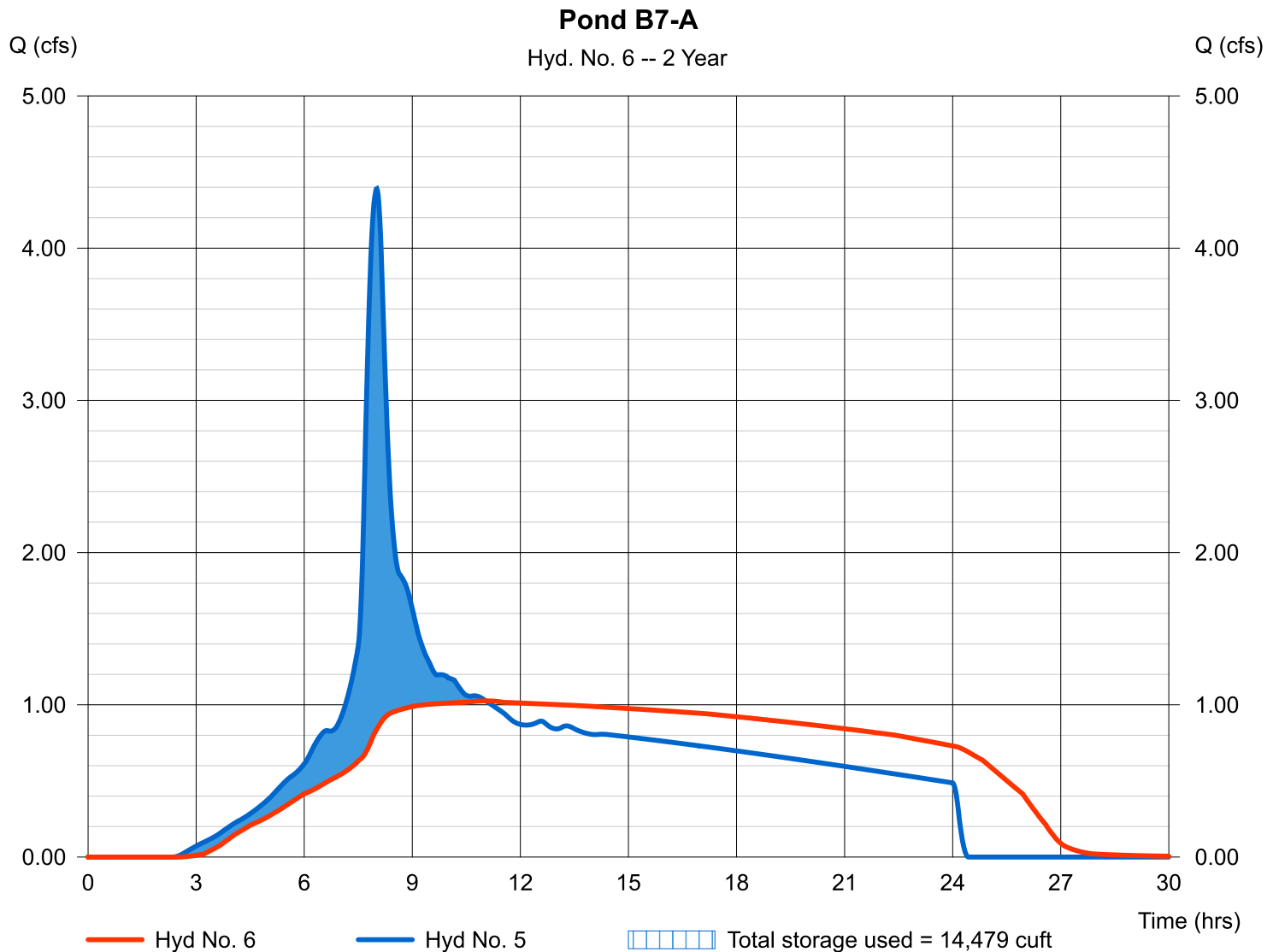
Hydrograph Report

Hyd. No. 6

Pond B7-A

Hydrograph type	= Reservoir	Peak discharge	= 1.026 cfs
Storm frequency	= 2 yrs	Time to peak	= 11.03 hrs
Time interval	= 1 min	Hyd. volume	= 65,036 cuft
Inflow hyd. No.	= 5 - Upst.+Onsite (CC3)	Max. Elevation	= 104.61 ft
Reservoir name	= Pond B7-A	Max. Storage	= 14,479 cuft

Storage Indication method used.



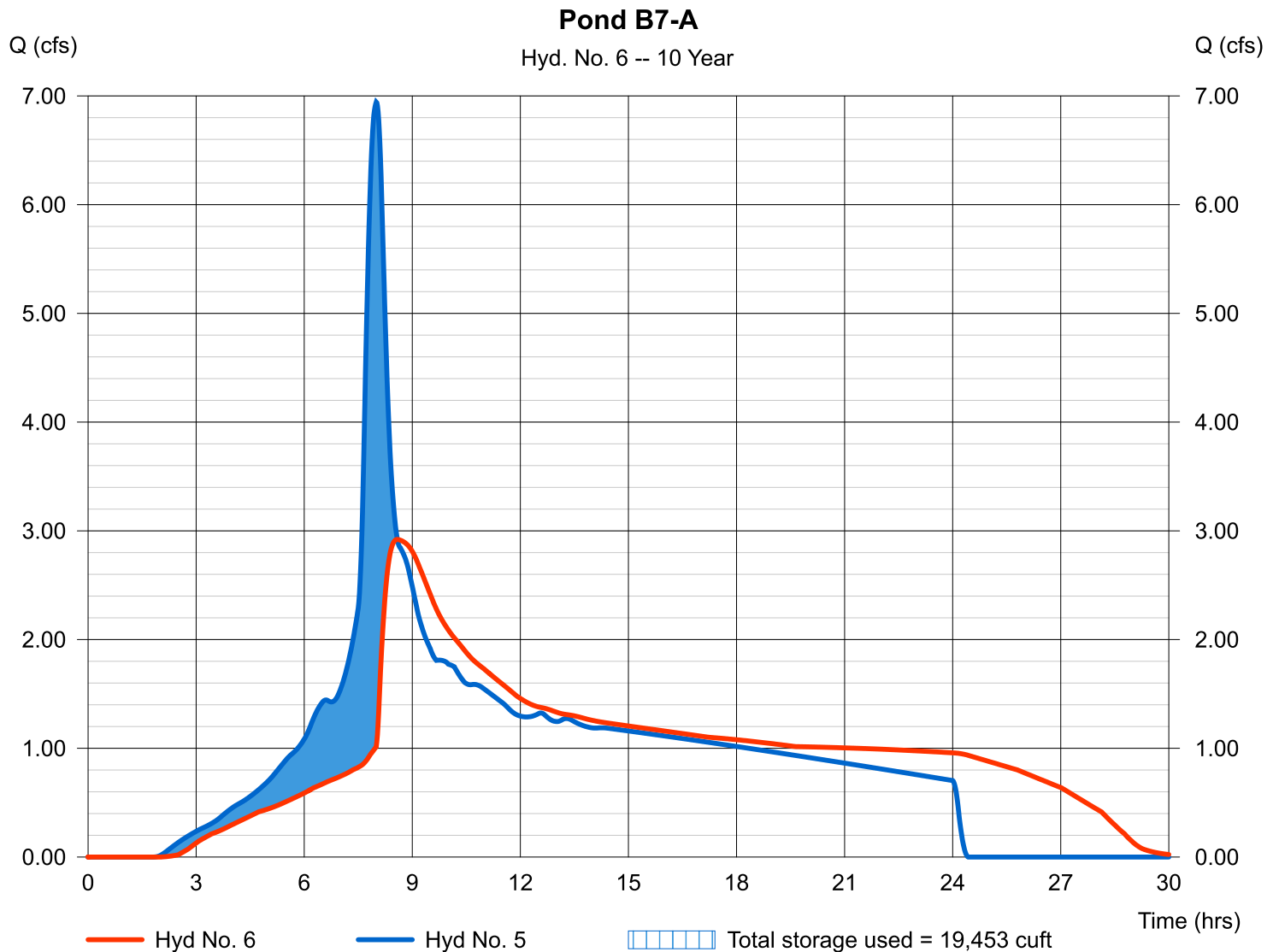
Hydrograph Report

Hyd. No. 6

Pond B7-A

Hydrograph type	= Reservoir	Peak discharge	= 2.921 cfs
Storm frequency	= 10 yrs	Time to peak	= 8.58 hrs
Time interval	= 1 min	Hyd. volume	= 100,379 cuft
Inflow hyd. No.	= 5 - Upst.+Onsite (CC3)	Max. Elevation	= 105.37 ft
Reservoir name	= Pond B7-A	Max. Storage	= 19,453 cuft

Storage Indication method used.



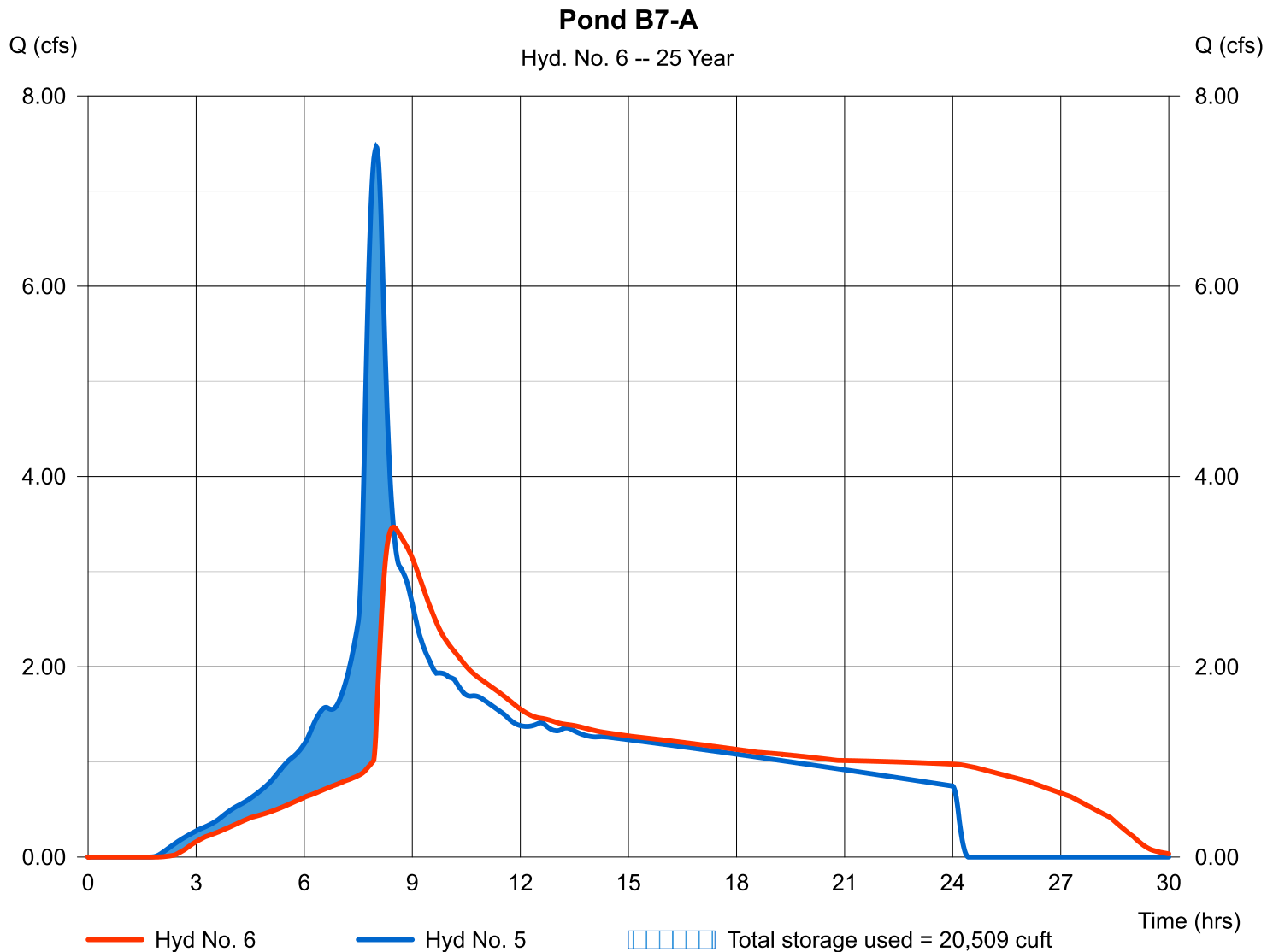
Hydrograph Report

Hyd. No. 6

Pond B7-A

Hydrograph type	= Reservoir	Peak discharge	= 3.467 cfs
Storm frequency	= 25 yrs	Time to peak	= 8.48 hrs
Time interval	= 1 min	Hyd. volume	= 107,627 cuft
Inflow hyd. No.	= 5 - Upst.+Onsite (CC3)	Max. Elevation	= 105.52 ft
Reservoir name	= Pond B7-A	Max. Storage	= 20,509 cuft

Storage Indication method used.



Hydrograph Report

Hyd. No. 6

Pond B7-A

Hydrograph type	= Reservoir	Peak discharge	= 5.836 cfs
Storm frequency	= 100 yrs	Time to peak	= 8.33 hrs
Time interval	= 1 min	Hyd. volume	= 144,459 cuft
Inflow hyd. No.	= 5 - Upst.+Onsite (CC3)	Max. Elevation	= 106.22 ft
Reservoir name	= Pond B7-A	Max. Storage	= 25,912 cuft

Storage Indication method used.

